(NASA-CR-161353) SPACE CONSTRUCTION BASE CONTROL SYSTEM Final Report (Bendix Corp.)
479 p. HC 421/MF 401 CSCL 22B

.N80515194

juclas 14 46605





FOREWORD

This Final Report is submitted in accordance with the Statement of Work, Exhibit "A" for Contract NAS8-32660. The study was directed from the Guidance Systems Division (GSD) of The Bendix The program manager Corporation. at this location was Mr. Raymond Kaczynski. Contributors from GSD were Mr. Raymond Kaczynski (Sections 1, 3, 5 and 9), Dr. Frederick Chichester (Sections 3 and 4) and the late Dr. Solomon Nachmias who initiated the study in Section 5. Other tasks were completed by personnel from the Bendix Research Laboratories Division (BRL) and the Bendix Energy, Environment and Technology Office (BEETO). The BRL effort, primarily Sections 2, 6 and 7, was coordinated by Mr. William Gelbach. Material in Sections 2 and 6 was generated by Dr. Mike Lodaya, with consultant Dr. Gary Leininger contributing to the basic approach in Section 6. Dr. Robert Gregory provided the material in Section 7. Mr. Don Lipski of BRL was responsible for the programming and some of the vehicle modeling in Sections 2, 4, Mr. Dan Johnson of BRL 6 and 8. was available for some of the mathematical modeling in the first half of the study. Mr. Calvin Rybak and Dr. Rao Karanam of BEETO were responsible for the material presented in Section 8. The guidance of Dr. Michael Borelli of MSFC throughout the study is again gratefully acknowledged.

ABSTRACT

Several approaches for an attitude control system are studied and developed for a large space construction base that is structurally flexible. Digital simulations were obtained using the following techniques: (a) the multivariable Nyquist array method combined with closed loop pole allocation, (b) the linear quadratic regulator method. Equations for the three-axis simulation using the multilevel control method were generated and are presented. Several alternate control approaches are also described. A technique is demonstrated for obtaining the dynamic structural properties of a vehicle which is constructed of two or more submodules of known dynamic characteristics.

THE BENDIX CORPORATION

GUIDANCE SYSTEMS DIVISION

TETERBORO, NEW JERSEY 07608

SPACE CONSTRUCTION BASE CONTROL SYSTEM

FINAL REPORT

SEPTEMBER 1, 1979

PREPARED FOR:

GEORGE C. MARSHALL SPACE FLIGHT CENTER HUNTSVILLE, ALABAMA

NASA CONTRACT NO. NAS8-32660

APPROVED BY:

DR. D. A. ZOMICK ENGINEERING MANAGER, SYSTEMS ENGINEER AND ANALYSIS

G. W. GARTNER DIRECTOR OF ENGINEERING PREPARED BY:

PROGRAM MANAGER

TABLE OF CONTENTS

SECTION NO.	TITLE	PAGE NO.
	ABSTRACT	i
1.0	INTRODUCTION	1-1
1.1	OBJECTIVES	11
1.2	SCOPE	1-1
1.3	GENERAL	1-3
1.4	REFERENCES	1-4
2.0	DYNAMIC MODELING OF THE VEHICLE	2-1
2.1	MATHEMATICAL MODEL	2-1
2,2	MODEL REDUCTION EIGENVALUE ANALYSIS	2-11
2.3	REFERENCES	2-16
3.0	CONTROL APPROACHES	3-1
3.1	MULTILEVEL CONTROL	3-1
3.1.1	GENERAL APPROACH	3-4
3.1.2	STATE VARIABLE MODEL	3-5
3.1.3	DECOMPOSED MODEL	3-5
3.1.4	PERFORMANCE INDEX	3-6
3.1.5	HAMILTONIAN	3-7
3.1.6	COSTATE EQUATIONS	3-8
3.1.7	COSTATE COORDINATION EQUATIONS	3-8
3.1.8	CONTROL EQUATIONS	3–8
3.1.9	SUBPROBLEM HIERARCHY	3-9
3.2	LINEAR QUADRATIC REGULATOR (LQR)	3-10
3.3	MULTIVARIABLE NYQUIST ARRAY (MNA)	3-12
3.3.1	MNA DESIGN PROCEDURE	3-12
3.3.2	RETALLACK POLE PLACEMENT METHOD	3-18
3.4	REFERENCES	3~21

SECTION NO.	TITLE		
4.0	SIMULATION OF MULTILEVEL CONTROL	4-1	
4.1	LINEARIZED THREE-DIMENSIONÁL DISCRETE MASS ROTATIONAL MODEL FOR CONFIGURATION 1	4-1	
4.1.1	DEFINITIONS	4-4	
4.1.2	ROTATIONAL EQUATIONS OF MOTION	4-5	
4.1.3	EULER ANGLE EQUATIONS	4-9	
4.1.4	SUSPENSION EQUATIONS	4-11	
4.1.5	ROTATIONAL STATE EQUATIONS	4-12	
4.2	APPLICATION OF MULTILEVEL CONTROL TECHNIQUES TO A LINEARIZED DISCRETE MASS MODEL	4-16	
4.2.1	DECOMPOSITION	4-16	
4.2.2	PERFORMANCE INDEX FOR THE LINEARIZED MODEL OF SCB CONFIG- URATION 1 WITH CONTROL TORQUE APPLIED ONLY TO BODY 1	4-18	
4.2.3	HAMILTONIAN FOR LINEARIZED MODEL OF SCB CONFIGURATION 1 WITH CONTROL APPLIED ONLY TO BODY 1	4-19	
4.2.4	COSTATE EQUATIONS FOR LINEARIZED MODEL OF SCB CONFIGURATION 1	4-20	
4.2.5	CONTROL EQUATIONS FOR LINEARIZED MODEL OF SCB CONFIGURATION 1	4-20	
4.2.6	ADDITIONAL NECESSARY CONDITIONS FOR LINEARIZED SYSTEM	4-21	
4.2.7	SUMMARY OF COORDINATION EQUATIONS FOR LINEARIZED MODEL	4-21	
4.2.8	VECTOR REPRESENTATION OF VARIABLES FOR LINEARIZED MODEL OF SCB CON- FIGURATION 1 WITH CONTROL APPLIED ONLY TO BODY 1	4-22	

SECTION NO.	TITLE	PAGE NO.	
4.3	APPLICATION OF MULTILEVEL CONTROL TECHNIQUES TO A HYBRID COORDINATE MODEL	4-23	
4.3.1	DISCRETE RIGID BODY MODEL OF A SPACECRAFT	4-23	
4.3.2	HYBRID COORDINATE MODEL	4-25	
4.3.3	DECOMPOSED HYBRID COORDINATE MODEL	4-27	
4.3.4	DECOMPOSED PERFORMANCE INDEX AND HAMILTONIAN	4-28	
4.3.5	COSTATE AND COSTATE COORDINATION . EQUATIONS	4-29	
4.3.6	THE CONTROL ALGORITHM	4-30	
4.3.7	CONSTRUCTION OF THE SUBPROBLEM HIERARCHY	4-30	
4.4	CONCLUSIONS AND RECOMMENDATIONS	4-30	
4.5	REFERENCES	4-34	
5.0	SIMULATION OF LQR CONTROL	5-1	
5.1	VEHICLE EQUATIONS	5-1	
5.2	OPTIMUM FEEDBACK GAIN	5-11	
5.3	SIMULATION	5-14	
5.4	DISCUSSION	5-21	
5.5	REFERENCES	5-24	
6.0	SIMULATION OF MNA CONTROL	6-1	
6.1	CONTROL DESIGN FOR THE Z-AXIS	6-2	
6.2	MNA DESIGN FOR ROM Z-AXIS	6-5	
6.3	RETALLACK POLE PLACEMENT FOR ROM Z-AXIS	6-12	
6.4	CONCLUSIONS AND RECOMMENDATIONS	6-35	
6.5	REFERENCES	6-37	

SECTION NO.	TITLE		
7.0	ALTERNATE CONTROL APPROACHES	7-1	
7.1	LINEAR, CONSTANT PARAMETER, MULTI- VARIABLE CONTROL APPROACH	7-2	
7.1.1	PLANT	7-2	
7.1.2	DESIGN OF STATE FEEDBACK CONTROLLER	7-4	
7.1.3	DESIGN OF STATE ESTIMATOR	7-9	
7.1.4	SYSTEM DESIGN PARAMETERS	7-12	
7.2	APPLICATION TO SPACE BASE	7-13	
7.2.1	WEIGHTING OF STATE VARIABLES	7-14	
7.2.2	AERODYNAMIC DISTURBANCE TORQUE	7-15	
7.2.3	WEIGHTING COEFFICIENTS FOR DISTURBANCE STATE VARIABLE ESTIMATION ERROR	7-16	
7.2.4	KNOWN INPUT AND PLANT DISTURBANCES	7–18	
8.0	STRUCTURAL ANĀLYSIS ŠTUDY	8-1	
8.1	SUMMARY OF APPROACH	8-1	
8.2	TECHNICAL DISCUSSION	8-2	
8.2.1	PRELIMINARIES	8-6	
8.2.2	CONSTRAINT FORCES AND CONSTRAINT TORQUES .	8–8	
8.2.3	TRANSLATIONAL EQUATIONS OF MOTION FOR THE FULL BEAM	8-15	
8.2.4	ROTATIONAL EQUATIONS OF MOTION FOR THE FULL BEAM	8–18	
8.2.5	MATRIX EQUATION OF MOTION FOR THE FULL BEAM	8-21	
8.2.6	SPLIT-BEAM INTERFACE FORCES AND TORQUES	8-25	
8.2.7	TRANSLATIONAL EQUATIONS FOR BODIES OF THE SPLIT-BEAM	8–30	
8.2.8	ROTATIONAL EQUATIONS FOR BODIES OF THE SPLIT-BEAM	8-33	

SECTION NO.	$\overline{ ext{TITLE}}$	PAGE NO.	
8.2.9	MATRIX EQUATION OF MOTION FOR THE SPLIT-BEAM	8-36	
8.2.10	DETERMINATION OF THE VIBRATION FREQUENCIES AND MODE SHAPES	8-39	
8.2.11	STIFFNESS MATRICES	8-40	
8.2.12	SIMULATION RESULTS	8-46	
8.3	CONCLUSIONS	8-53	
8.4	REFERENCES	8-54	
9.0	CONCLUSIONS AND RECOMMENDATIONS	9-1	
9.1	CONCLUSIONS	9-2	
9.2	RECOMMENDATIONS	9-4	

SECTION NO.	TITLE
APPENDICES	
A	NUMERICAL VALUES OF MATRICES USED IN ANALYSIS AND DESIGN
В	TRANSFER FUNCTIONS FOR SYMMETRIC Z-AXIS WITH STATE VECTOR
	$X^{T}(t) = \begin{bmatrix} \omega_{1}, & \omega_{21}, & \omega_{42}, & \psi_{21}, & \psi_{42}, \end{bmatrix}$
С	DERIVATION AND ANALYSIS OF MINIMUM
,	(TRACE $E_{\mathbf{c}}^{\mathbf{T}}E_{\mathbf{c}}^{\mathbf{T}}$) SOLUTION FOR STATE
	CONTROLLER MATRIX C .
D _.	ALGORITHM FOR GENERATING OPTIMUM STATE CONTROLLER OR ESTIMATOR GAIN MATRIX
E	DERIVATION AND ANALYSIS OF MINIMUM
	$(TRACE \ E_e^T E_e)^{\frac{1}{2}}$ SOLUTION FOR STATE
	ESTIMATION GAIN MATRIX H
F	EQUATIONS FOR THE FULL BEAM AND SPLIT-BEAM
G	MODE SHAPES OF THE NATURAL FREQUENCIES FOR THE ORIGINAL BEAM
H	MODE SHAPES OF THE NATURAL FREQUENCIES FOR THE SPLIT-BEAM

LIST OF ILLUSTRATIONS

FIGURE NO.	TITLE			
2-1	CONFIGURATION 1 OF SPACE CONSTRUCTION BASE	2-2		
2-2	TOPOLOGICAL DIAGRAM OF SCB CONFIGURATION 1	2-3		
3-1	TWO LEVEL SUBPROBLEM HIERARCHY FOR MULTILEVEL CONTROL	3-3		
3-2	MULTIVARIABLE SYSTEM CONFIGURATION	3-13		
3-3	CLOSED LOOP SPACECRAFT CONTROL DESIGN	3-17		
4-1	TOPOLOGICAL DIAGRAM OF SCB CONFIGURATION 1	4-3		
4-2	SUBPROBLEM HIERARCHY FOR LINEARIZED SPACE CONSTRUCTION BASE ROTATIONAL MODEL WITH MULTILEVEL CONTROL	4-24		
4-3	TORSIONAL MODEL OF THE VEHICLE	4-26		
4-4	SUBPROBLEM HIERARCHY FOR MULTILEVEL CONTROL	4-31		
5-1	SPACE CONSTRUCTION BASE CONFIGURATION 1	5-2		
5-2	INERTIA MODEL FOR CONFIGURATION 1	5-3		
5-3	TORSIONAL MODEL OF THE VEHICLE	5-6		
5-4	MATRIX PARAMETERS FOR DISCRETE INERTIA, SPRING AND DAMPING CONSTANTS	5–10		
5-5	THE INVERSE OF INERTIA MATRIX, \mathbf{A}_{K} , \mathbf{A}_{D} AND \mathbf{B}^{T}	5-10		
5-6	BLOCK DIAGRAM OF LQR-CONTROLLED SYSTEM	5-13		
5-7	SYSTEM MATRICES A AND B, WEIGHTING FACTORS Q AND R, AND INITIAL CONDITIONS FOR SOLUTION OF THE MATRIX RICCATI EQUATION	5–15		
5-8	"FINAL" CONDITIONS OF MATRIX RICCATI EQUATION SOLUTION AT TIME = 200 SECONDS	5–15		

LIST OF ILLUSTRATIONS (Cont'd)

FIGURE NO.	TITLE				
5-9	FULL STATE LQR FEEDBACK, CENTRAL BODY ATTITUDE AND CONTROL TORQUE, INITIAL CONDITION: $9_1(O) = 1$ DEGREE	5-17			
5-10	FULL STATE LQR FEEDBACK, RELATIVE MOTION OF INBOARD AND OUTBOARD APPENDAGES	5–18			
5-11	PARTIAL STATE "LQR" FEEDBACK, CENTRAL BODY ATTITUDE AND CONTROL TORQUE INITIAL CONDITION: $\Theta_{7}(O) = 1$ DEGREE	5-19 ·			
5-12	PARTIAL STATE "LQR" FEEDBACK, RELATIVE MOTION OF INBOARD AND OUTBOARD APPENDAGES	5-20			
5-13	SINGLE AXIS N-DIMENSIONAL REPRESEN- TATION OF A LARGE FLEXIBLE VEHICLE	5-23			
6-1	A TYPICAL BODE DIAGRAM FOR THE Z-AXIS	6-4			
6-2	CLOSED LOOP SPACECRAFT CONTROL DIAGRAM	·66			
6-3	BODE DIAGRAM LOOP 1 FOR ROM Z-AXIS .	6-7			
6-4	BODE DIAGRAM LOOP 2 FOR ROM Z-AXIS	. 6-7-			
6-5	CLOSED LOOP TIME RESPONSE FOR Ψ_{21} ,	6-9			
•	WITH NO DYNAMIC COMPENSATION				
6-6	BODE DIAGRAM LOOP 2 WITH BRIDGED-T COMPENSATOR INSERTED	6-10			
6-7	CLOSED LOOP Y 21 TIME RESPONSE FOR COMPENSATED SYSTEM	6-11			
6-8	BODE PLOT FOR LOOP 2 WITH SIMULTANEOUS FREQUENCY AND DAMPING RATIO SHIFT OF POLE AT $\omega=1.0$	6–13			
6-9	CLOSED LOOP TIME RESPONSE FOR ψ_{21}	6-14			
6-10	ANGULAR POSITION BODY 1	6-20			
6-11	RELATIVE ANGULAR POSITION BODY 2	6-20			
6-12	RELATIVE ANGILAR POSITION BODY 4	6-21			

LIST OF ILLUSTRATION (Cont'd)

FIGURE NO.	TITLE	NO.
6-13	CONTROL TORQUE BODY 1	6-21
6-14	CONTROL TORQUE BODY 2	6-22
6-15	ANGULAR POSITION BODY 1	6-23
6-16	RELATIVE ANGULAR POSITION BODY 2	6-23
6-17	RELATIVE ANGULAR POSITION BODY 4	6-24
6-18	CONTROL TORQUE BODY 1.	6-24
6-19	CONTROL TORQUE BODY 2	6-25
6-20	ANGULAR POSITION BODY 1	6-26
6-21	RELATIVE ANGULAR POSITION BODY 2	6-26
6-22	RELATIVE ANGULAR POSITION BODY 4	6-27
6-23	CONTROL TORQUE BODY 1	6-27
6-24	CONTROL TORQUE BODY 2	6-28
6-25	MAXIMUM TORQUE T _{1Z} VS POLE	6-30
	LOCATION FOR RIGID BODY	
6-26	ANGULAR POSITION BODY 1	6-32
6-27	RELATIVE ANGULAR POSITION BODY 2	6-32
6 - 28	RELATIVE ANGULAR POSITION BODY 4	6-33
6-29	CONTROL TORQUE BODY 1	6-33
6-30	CONTROL TORQUE BODY 2	6-34
· 7-1	BLOCK DIAGRAM OF COMPLETE SYSTEM	7–11
8-1	IDEALIZED MODEL OF THE BEAM	8-3
8-2	ILLUSTRATION OF SOME NOMENCLATURE (8-3
8-3	CONNECTION OF BODIES i AND i+2	8-9
8-4	CONNECTION OF BODIES i AND I+1	8-9
8-5	CONNECTION OF THE HALF-BEAMS	8-25
8-6	ILLUSTRATION OF THE COORDINATE SYSTEM	8-4]
8-7	RELATIONSHIP BETWEEN BODIES	8-4]

LIST OF TABLES

TABLE NO.	TITLE	PAGE NO.
5-1	INERTIA CHARACTERISTICS OF BODY 1	5-5
5-2	SUMMARY OF PHYSICAL CONSTANTS	5-9
6-1	CLOSED LOOP RESPONSE	6-19
6-2	GAIN MATRIX FOR $ au_{2Z}$	6-31
8-1	NOMENCLATURE	8-4
8-2	COMPARISON OF THE FREQUENCIES OF VIBRATION FOR THE ORIGINAL BEAM AND THE SPLIT-BEAM	8–48

SECTION 1

1.0 INTRODUCTION

This report is submitted in compliance with the statement of Work under contract NASS-32660. The period of performance covered by the report is the calendar year of August 26, 1978 to August 26, 1979. The submission and approval of this report constitute the successful completion of the Exhibit "A" and Exhibit "B" portions of the contract.

This report is the second of a series under the same contract number. The previous report (Reference 1-1) was submitted in October 1978 and covered the period from July 27, 1977 to July 27, 1978 in compliance with Exhibit "A" of contract NASS-32660.

1.1 OBJECTIVES

The sections that follow summarize the effort expended on the Space Construction Base (SCB) Control System Study contract. The primary objective of the study was to develop a control system and flexible control techniques that will stabilize a large and growing space station of the future. The study emphasized control methods, but additional topics include dynamic modeling of the vehicle and a technique for combining the dynamics of two or more submodules into one overall model.

1.2 SCOPE

Study effort was concentrated in two major areas:

a. Application of different methods for control of large flexible spacecraft.

- b. Generation of flexible vehicle dynamic models. Control equations were developed for three distinct approaches:
 - a. Multilevel control
 - b. Linear quadratic regulator (LQR)
 - c. Multivariable Nyquist array (MNA) method and Pole Placement Techniques.

Single axis simulations were generated for control of the SCB Configuration 1 using the LQR and MNA techniques. Control equations were generated for three-axis control of the same vehicle using the Multilevel control method. A heavy programming load resulting from one of the vehicle modeling tasks pre-empted the completion of this three-axis multilevel control simulation.

Equations were generated for this three-axis vehicle model and are presented along with control equations for the multilevel approach. Single axis vehicle models also were derived for application with the other control approach simulations. One additional vehicle modeling task was a structural analysis study in which the dynamic models of two submodules were combined to form a single structural model. Vibration modes for the individual submodules and those for the composite structure were obtained using computerized matrix techniques for finite elements of the bodies. Analytical techniques also were applied to verify the results.

Some assumptions used throughout the report are that sensor and actuator dynamics are negligible in the control analysis because of their relatively broad bandwidths, computer quantization and other non-linearities were assumed to be negligible for the time being.

A number of other items related to SCB control are not discussed here since they were completed in the previous study (Reference 1-1):

- a. Mission requirements
- b. Pointing and orientation requirements
- c. Actuator sizing requirements
- d. Momentum desaturation requirements.

1.3 GENERAL

This report is comprised of nine sections. Section 2 contains an SCB vehicle model (Configuration 1), which is used in Section 4 in equation form and in Section 6 as numerical data. Sections 3 through 7 treat control techniques for attitude stabilization of flexible vehicles. Section 3 contains a preliminary description of each of the control techniques utilized in Sections 4, 5 and 6. Section 4 describes equations for three axis simulation of the multilevel control method. Section 5 presents a single axis simulation of control using the linear quadratic regulator (LQR) method. Section 6 describes a simulation of one axis of the SCB using the multivariable Nyquist array (MNA) method of control, and also applies a technique for closed loop pole placement. Section 7 discusses several alternate control approaches

which may be considered in future efforts. Section 8 treats a potentially important tool for flexible vehicle modeling: a structural analysis study for combining the dynamics of two or more distributed parameter submodules into a single model when the submodules are securely fastened together. Section 9 is a discussion of conclusions and recommendations. A number of Appendices are placed at the end of the report. References are cited liberally and are listed at the end of each section.

The original RFQ requested that the International System of units (designated as SI) be used in the program and in any reporting. Torques, moments, angular momentum, moments of inertia and distances, however, are stated in English units since this was the system of units used in presenting all of the vehicle inertia data in the RFQ.

A liberal approach was also followed in the numbering of SCB configurations. The original RFQ initially used Roman numerals, but the text here used Arabic numerals in most cases -- except where material is reprinted from the RFQ.

1.4 REFERENCES

1-1 Guidance Systems Division, The Bendix Corporation, Space Construction Base Control System, Final Report, Contract NASS-32660 for Geroge C. Marshall Space Flight Center, Oct. 27, 1979.

SECTION 2

SECTION 2

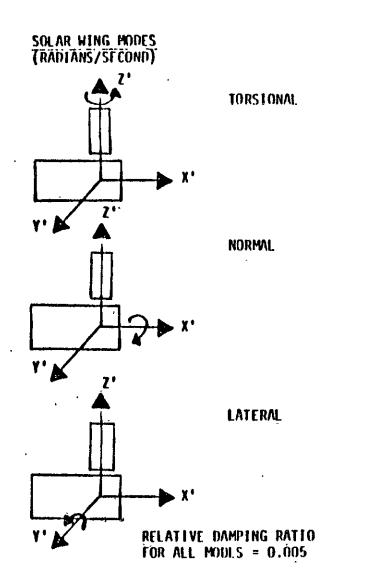
2.0 DYNAMIC MODELING OF THE VEHICLE

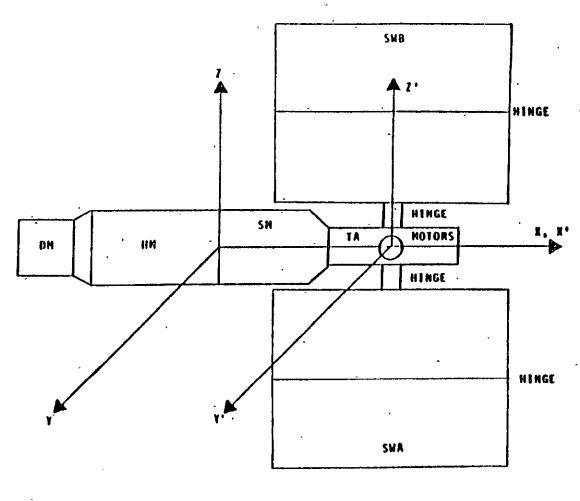
Configuration 1 of the SCB consists of two solar wings connected to four contiguous modules which are considered to be rigid relative to the solar wings. Each solar wing is converted to two rigid bodies as shown in Figure 2-1. The five individual bodies are designated as in the diagram of Figure 2-2. They are connected to each other via the three degree of freedom hinge suspensions, designated as 2 through 5 as shown.

2.1 MATHEMATICAL MODEL

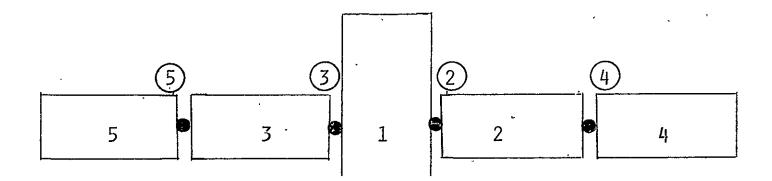
The mathematical model for the SCB Configuration

1 spacecraft was obtained using the discrete coordinate method described in Reference 2-1. The system model consists of five rigid bodies connected by joints or hinges and subjected to arbitrary external forces and torques. The modeling procedure assumes that the bodies are connected in the form of a topological tree and hence contains no "closed loops". The relative motion about each joint is assumed to be rotational, and a three axis model which includes all cross-coupled axis interactions was developed.





CONFIGURATION 1 OF SPACE CONSTRUCTION BASE FIGURE 2-1



(The individual bodies are connected to each other via three degree of freedom spring hinge suspensions. Hinge numbers are circled.)

TOPOLOGICAL DIAGRAM OF SCB CONFIGURATION 1 FIGURE 2-2 The linearized model, derived based on small relative assumptions using the discrete coordinate approach (References 2-2 and 2-3), is expressible in the form.

$$\dot{P\omega} = Q \tag{2-1}$$

where: P is 15 x 15 nonsingular matrix, function of the model parameters (inertias, masses, etc.)

ω is 15 x 1 angular velocity vector, defined as $ω = \begin{bmatrix} ω_{1X}, ω_{1Y}, ω_{1Z}, ω_{2X}, ω_{2Y}, ω_{2Z}, ω_{3X}, ω_{3Y}, ω_{3Z}, ω_{4X}, ω_{4Y}, ω_{4Z}, ω_{5X}, ω_{5Y}, ω_{5Z} \end{bmatrix}^{T}$ Q is 15 x 1 torque vector,

defined as:

$$Q = \begin{bmatrix} Q_1, Q_2, Q_3, Q_4, Q_5 \end{bmatrix}^T$$
 and $Q_i = \begin{pmatrix} Q_{ix}, Q_{iy}, Q_{iz} \end{pmatrix}^T$ for $i=1,\ldots,5$

The vector components of the Matrix Q are given as follows:

$$Q_{1} = T_{e_{1}} + T_{a_{1}} - T_{S_{12}} - T_{S_{13}}$$

$$Q_{2} = T_{e_{2}} + T_{a_{2}} + T_{S_{12}} - T_{S_{24}}$$

$$Q_{3} = T_{e_{3}} + T_{a_{3}} + T_{S_{13}} - T_{S_{35}}$$

$$Q_{4} = T_{e_{4}} + T_{a_{4}} + T_{S_{24}}$$

$$Q_{5} = T_{e_{5}} + T_{a_{5}} + T_{S_{35}}$$

$$(2-2)$$

where $T_{e_{i}}$ is an external torque vector on body i given by $T_{e_{i}} = (T_{e_{iX}}, T_{e_{iY}}, T_{e_{iZ}})^{T}$

T is an actuator, torque vector on body i ai given as $T_{a_i} = (T_{a_iX}, T_{a_iY}, T_{a_iZ})T$

 T_{S} is a suspension torque vector between ij bodies i and j given as

$$T_{S_{ij}} = (T_{S_{ijX}}, T_{S_{ijY}}, T_{S_{ijZ}})^{T}$$

Define thirty state variables as follows:

$$X_{1} = \omega_{1X}$$
 $X_{16} = \phi_{1}$ $X_{2} = \omega_{1Y}$ $X_{3} = \omega_{1Z}$ $X_{18} = \psi_{1}$ $X_{18} = \psi_{1}$

$$X_{4} = \omega_{2X} - \omega_{1X}$$
 $X_{19} = \phi_{2} - \phi_{1}$ $X_{5} = \omega_{2Y} - \omega_{1Y}$ $(2-4)$ $X_{20} = \theta_{2} - \theta_{1}$ $(2-9)$ $X_{6} = \omega_{2Z} - \omega_{1Z}$ $X_{21} = \psi_{2} - \psi_{1}$

$$X_7 = \omega_{3X} - \omega_{1X}$$
 $X_{22} = \phi_3 - \phi_1$ $X_8 = \omega_{3Y} - \omega_{1Y}$ (2-5) $X_{23} = \theta_3 - \theta_1$ (2-10) $X_9 = \omega_{3Z} - \omega_{1Z}$ $X_{24} = \psi_3 - \psi_1$

$$X_{13} = \omega_{5X} - \omega_{3X}$$
 $X_{28} = \phi_5 - \phi_3$ $X_{14} = \omega_{5Y} - \omega_{3Y}$ (2-7) $X_{29} = \theta_5 - \theta_3$ (2-12) $X_{15} = \omega_{5Z} - \omega_{3Z}$ $X_{30} = \psi_5 - \psi_3$

Where $\phi_{\bf i},~\theta_{\bf i},~\psi_{\bf i}$ are the Euler angles about X, Y and Z axis, respectively, for body i.

 $\phi_{\mbox{ij}}=\phi_{\mbox{i}}-\phi_{\mbox{j}}$ represents a relative angle of body i with respect to body j in the X direction.

Similarly,
$$\theta_{ij} = \theta_{i} - \theta_{j}$$
, $\psi_{ij} = \psi_{i} - \psi_{j}$, $\omega_{ijx} = \omega_{ix} - \omega_{jx}$, $\omega_{ijy} = \omega_{iy} - \omega_{jy}$ and $\omega_{ijz} = \omega_{iz} - \omega_{jz}$.

Also define:

$$\mathbf{X}_{\mathrm{H1}} = (\mathbf{X}_{1}, \ \mathbf{X}_{2}, \ \mathbf{X}_{3}, \ \mathbf{X}_{4}, \ \mathbf{X}_{5}, \ \mathbf{X}_{6}, \ \mathbf{X}_{7}, \ \mathbf{X}_{8}, \ \mathbf{X}_{9}, \ \mathbf{X}_{10}, \\ \mathbf{X}_{11}, \ \mathbf{X}_{12}, \ \mathbf{X}_{13}, \ \mathbf{X}_{14}, \ \mathbf{X}_{15})^{\mathrm{T}}$$
 (2-13)

$$\mathbf{X}_{\mathrm{H2}} = (\mathbf{X}_{16}, \ \mathbf{X}_{17}, \ \mathbf{X}_{18}, \ \mathbf{X}_{19}, \ \mathbf{X}_{20}, \ \mathbf{X}_{21}, \ \mathbf{X}_{22}, \ \mathbf{X}_{23}, \\ \mathbf{X}_{24}, \ \mathbf{X}_{25}, \ \mathbf{X}_{26}, \ \mathbf{X}_{27}, \ \mathbf{X}_{28}, \ \mathbf{X}_{29}, \ \mathbf{X}_{30})^{\mathrm{T}}$$

$$(2-14)$$

$$\begin{split} \mathbf{X} &= \begin{bmatrix} \mathbf{X}_{\text{H1}} \\ \mathbf{X}_{\text{H2}} \end{bmatrix} = (\mathbf{X}_{1}, \ \mathbf{X}_{2}, \ \mathbf{X}_{3}, \ \mathbf{X}_{4}, \ \mathbf{X}_{5}, \ \mathbf{X}_{6}, \ \mathbf{X}_{7}, \ \mathbf{X}_{8}, \\ & \mathbf{X}_{9}, \ \mathbf{X}_{10}, \ \mathbf{X}_{11}, \ \mathbf{X}_{12}, \ \mathbf{X}_{13}, \ \mathbf{X}_{14}, \ \mathbf{X}_{15}, \\ & \mathbf{X}_{16}, \ \mathbf{X}_{17}, \ \mathbf{X}_{18}, \ \mathbf{X}_{19}, \ \mathbf{X}_{20}, \ \mathbf{X}_{21}, \ \mathbf{X}_{22}, \\ & \mathbf{X}_{23}, \ \mathbf{X}_{24}, \ \mathbf{X}_{25}, \ \mathbf{X}_{26}, \ \mathbf{X}_{27}, \ \mathbf{X}_{28}, \ \mathbf{X}_{29}, \\ & \mathbf{X}_{30})^{\mathrm{T}} \end{split}$$

From the definition of the state variables:

$$X_{H2} = X_{H1}$$
 (2-16)

i.e.,
$$X_{16} = X_1$$
, $X_{17} = X_2$, etc.

Equations (2-3) through (2-7) can easily be rearranged so that ω can be expressed in terms of $X_{\rm H1}$ by the following relationship:

$$\omega = N X_{H1}$$
 (2-17)

Where N is 15 x 15 constant, nonsingular matrix.

Differentiating (2-17) with respect to time yields;

$$\dot{\hat{\mathbf{w}}} = \mathbf{N} \dot{\mathbf{X}}_{\mathbf{H1}} \tag{2-18}$$

Multiplying both sides of equation (2-1) by P^{-1} and substituting for angular acceleration vector $\hat{\omega}$ from equation (2-18) yields;

$$N \dot{X}_{H1} = P^{-1} Q (2-19)$$

Multiplying both sides of equation (2-19) by N^{-1} gives;

$$\dot{X}_{H1} = N^{-1} P^{-1} Q$$
 (2-20)

Assuming no external torques, equation set (2-2) can be written as;

$$Q = T_2 + T_S \tag{2-21}$$

where T_a is 15 x 1 actuating torque vector.

 $T_{\rm S}$ is 15 x 1 suspension torque vector, given by:

$$T_{S} = (-T_{S_{12}} - T_{S_{13}}, T_{S_{12}} - T_{S_{24}}, T_{S_{24}}, T_{S_{35}})^{T}$$

$$(2-22)$$

$$(-T_{S_{12}} - T_{S_{13}})$$
, etc., are 3 x 1 vectors.

The scalar suspension torques can be expressed in terms of rate and displacement constants and inertial rate difference and relative displacements, for example:

$$T_{S_{12X}} = -K_{S_{12X}} \qquad \phi_{21} - C_{S_{12X}} \qquad (\omega_{2X} - \omega_{1X})$$

$$T_{S_{12Y}} = -K_{S_{12Y}} \qquad \theta_{21} - C_{S_{12Y}} \qquad (\omega_{2Y} - \omega_{1Y}) \qquad (2-23)$$

$$T_{S_{35Z}} = -K_{S_{35Z}} \qquad \psi_{53} - C_{S_{35Z}} \qquad (\omega_{5Z} - \omega_{3Z})$$

Substituting equation set (2-23) for all scalar suspension torques in (2-22), using definitions of the state variables (2-3 through 2-12) and re-arranging the terms, equation (2-22) can be expressed as

$$T_{S} = KD X_{H1} + KS X_{H2}$$
 (2-24)

where KD is 15 x 15 matrix of damping constants and KS is 15×15 stiffness matrix.

Substituting (2-24), into (2-21) gives

$$Q = T_a + KD X_{H1} + KS X_{H2}$$
 (2-25)

substituting Q given by (2-25) into (2-20) and multiplying by N^{-1} yields;

$$\dot{x}_{h1} = N^{-1} p^{-1} [T_a + KD X_{H1} + KS X_{H2}]$$
 (2-26)

Rewriting (2-16) in the following form:

$$x_{H2} = 1 x_{H1} + 0 x_{H2}$$
 (2-27)

where I is 15x15 identity matrix and 0 is 15x15 null matrix.

Combining (2-26) and (2-27) Yields

$$\begin{bmatrix} \dot{\mathbf{x}}_{\mathrm{H1}} \\ \dot{\mathbf{x}}_{\mathrm{H2}} \end{bmatrix} = \begin{bmatrix} \mathbf{n}^{-1}\mathbf{p}^{-1}\mathbf{K}\mathbf{D} & \mathbf{n}^{-1}\mathbf{p}^{-1}\mathbf{K}\mathbf{S} \\ \mathbf{I} & \mathbf{0} \end{bmatrix} \begin{bmatrix} \mathbf{x}_{\mathrm{H1}} \\ \mathbf{x}_{\mathrm{H2}} \end{bmatrix}$$

$$+ \begin{bmatrix} N^{-1}p^{-1} \\ 0 \end{bmatrix}^{T} a$$
 (2-28)

This can be further expressed as:

$$\dot{X}(t) = AX(t) + B\tau(t)$$
where $X = \begin{bmatrix} X_1, ---X_{30} \end{bmatrix}^T$

$$\tau(t) = T_a = [T_{alx}, T_{aly}, T_{alz}, \dots, T_{a5z}]_{15xl}^T$$

$$A = \begin{bmatrix} N^{-1}P^{-1}KD & N^{-1}P^{-1}KS \\ I & 0 \end{bmatrix}$$
30x30

$$B = \begin{bmatrix} N^{-1}P^{-1} \\ 0 \\ 30x15 \end{bmatrix}$$

Assuming no torque applied to body 4 and 5, τ can be written as

$$\tau = \left[\tau_{1x}, \dots, \tau_{3Z}\right]_{9 \times 1}^{T}$$
(2-30)

and B can be reduced to 30x9 matrix.

Numerical values of matrices P, N, KD, KS, A and B used for analysis and design purposes are shown in Appendix A.

2.2 Model Reduction Eigenvalue Analysis

The eigenvalues for the five-body three-axis models were obtained as follows: (Set A)

```
(1)
     -.0149042
                      j 1.61213
(2) -.0268672
                      j 1.20486
(3) -.0153772
                      j 0.642112
(4) -.00228948
                      j 0.312132
(5) -.43191
                      j20.9923.
                  +
(6) -.462163
                      j20.4238
(7) -.0653141
                      j 7.13316
(8) -.0356952
                      j 5.55713
(9) -.00502089
                  +
                      j 1.00192
(10) -.00500057
                     j 1.00005
                      j 0.322123
(11) -.00172613
(12) -.00160014
                      j 0.32009
```

There are also six eigenvalues at the origin.

Setting all cross-axis coupling terms to zero, three five-body single-axis models can be developed. Under this condition the eigenvalues were computed as follows (Set B):

<u>X-axis</u> 0.0 0.0			· <u>Y-ax</u>	<u>is</u>		
				0.0		
				0.	0	
014904	<u>+</u>	j	1.61213	431645	<u>+</u>	j20.989
0266921	<u>+</u>	j	1.18467	462423	+	j20.427
0153771	<u>+</u>	j	0.642111	0654125	<u>+</u>	j 7.13772
00222516	+	j	0.30449	0356052	+	j 5.55064

Z-axis

0.0

0.0

-.00502089 + j 1.00192

 $-.00500057 \pm j 1.00005$

-.90172613 + j 0.322132

-.00160014 + j 0.32009

A comparison of the single axis eigenvalues with the three axis eigenvalues leads to the conclusion that, from an eigenvalue assignment viewpoint, the three axis vehicle control system can be subdivided into three single axis control systems. Further comparison suggests that cross-axis coupling from an eigenvalue perspective is minimal, and thus an increase in the damping and/or stiffness factors of the system by active control can be accomplished by single axis measures.

To examine the eigenstructure further, consider the single axis representations of Figure 2-2. The eigenvalues at the origin represent the rigid body dynamics of the main unit while the flexible modes are attributed to the solar wings. If the main unit were

sufficiently larger than the solar wing, the dynamics would not interact. The eigenvalues would then appear in double complex pairs. As the mass of the main unit decreases the eigenvalues of the open loop single axis system will shift in a predetermined way. These eigenvalues will then appear as single complex pairs.

Assume the state model for a single axis to be represented by the form

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\mathbf{\tau} \tag{2-31}$$

with the state vector as

$$x(t) = \left[\omega_{21} \omega_{42} \psi_{21} \psi_{42} \omega_{31} \omega_{53} \psi_{31} \psi_{53} \omega_{1} \psi_{1} \right]^{T}$$
 (2-32)

or in partitioned form

$$x(t) = [x_1(t)]x_2(t)x_3(t)]^T$$
 (2-33)

Substituting (2-33) into (2-31) yields

$$\begin{bmatrix} x_1 \\ x_2 \\ \overline{x}_3 \end{bmatrix} = \begin{bmatrix} A_{11} & A_{12} & A_{13} \\ A_{21} & A_{22} & A_{23} \\ A_{31} & A_{32} & A_{33} \end{bmatrix} \begin{bmatrix} x_1 \\ -1 \\ x_2 \\ \overline{x}_3 \end{bmatrix} + \begin{bmatrix} B_1 \\ -1 \\ B_2 \\ \overline{B}_3 \end{bmatrix}_{\tau}$$
(2-34)

with $A_{11}=A_{22}$ a 4x4 matrix representing individual solar wing dynamics, $A_{12}=A_{21}$ a 4x4 matrix representing the dynamic interaction of solar wing A on solar wing B, $A_{13}=0$, $A_{23}=0$, A_{31} and A_{32} are 2x4 matrices reflecting

the interaction of the solar wings on the rigid body and

$$A_{33} = \begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix}$$

contains the rigid body dynamics. Thus (2-34) becomes

$$\dot{\mathbf{x}} = \begin{bmatrix} \mathbf{A}_{11} & \mathbf{A}_{12} & 0 \\ \mathbf{A}_{12} & \mathbf{A}_{11} & 0 \\ \mathbf{A}_{31} & \mathbf{A}_{32} & \mathbf{A}_{33} \end{bmatrix} \mathbf{x} + \mathbf{B}\tau \tag{2-35}$$

The open loop eigenvalues of (2-35) consist of the eigenvalues of A_{33} (designated as $\lambda(A_{33})$) plus the eigenvalues of the partitioned block

$$\begin{bmatrix} A_{11} & A_{12} \\ A_{12} & A_{11} \end{bmatrix}$$
 (2-36)

With ${\rm A}_{11}$ and ${\rm A}_{12}$ square and of the same dimension (i.e., 4x4), row and column manipulations on (2-36) yield

$$\begin{bmatrix} A_{11} - A_{12} & 0 \\ A_{12} & A_{11} + A_{12} \end{bmatrix}$$
 (2-37)

Since eigenvalues of (2-36) are unaffected by row and column manipulations, the eigenvalues in (2-36) equal the eigenvalues of (2-37). But (2-37) is in block diagonal form, thus the eigenvalues of A in (2-34) equal the eigenvalues of A_{33} , plus the eigenvalues of A_{11} - A_{12} , plus the eigenvalues of A_{11} + A_{12} ; i.e.,

$$\lambda(A) = \lambda(A_{33}), \quad \lambda(A_{11} + A_{12}), \quad \lambda(A_{11} - A_{12})$$
 (2-38)

If $A_{12} = 0$, then the eigenvalues will appear in double complex pairs. Hence any departure of A_{12} from the zero matrix will cause an eigenvalue shift in the manner described by (2-38).

Re-ordering the state vector for each of the single axis models as in (2-32), the single axis eigenvalues previously computed were similarly obtained using (2-38). Thus the significant eigenvalue shifts in both the X and Y axes result from the cross-coupled interactions of the solar wings in the respective axis and not by any cross-axis coupling.

To obtain a qualitative measure of the interactive eigenshifts, assume $\psi_{21} = \psi_{31}$ and $\psi_{42} = \psi_{53}$ in both magnitude and phase for all time. This is equivalent to a symmetry assumption about the main unit. The eigenvalues for each axis are subsequently computed as (Set C):

<u>X-axis</u>				<u>Y-axis</u>		
0.0				0.0		
	0.0			0.0		
0153606	<u>+</u>	j	0.641803	0697786	+	j 7.13515
0149224	<u>+</u>	j	1.61229	482064	<u>+</u>	j20.9874
0153606	<u>+</u>	j	0.641803	0697786	<u>+</u>	j 7.13515
0149224	+	j	1.61229	482064	+	j20.9874

Z-axis

0.0

0.0

ļ

-.00500564 + j 1.00112

-.00160836 + j 0.320495

-.00500564 + j 1.00112

-.00160836 + j 0.320495

Comparing eigenvalue Set C with eigenvalue Set B we conclude that the symmetry assumption for the z axis (and possible the y axis) is worthy of further investigation. The eigenvalue shift in the x-axis as caused by the solar panel interations suggests that this axis model should be treated in its entirety.

2.3 REFERENCES

- 2-1 Hooker, W. W. and Margulies, G., "The Dynamical Attitude Equations for an N-body Satellite", Journal of the Astronautical Sciences, Vol. XII, No. 4, PP. 123-128, 1965.
- 2-2 Lipski, D. B., "Discrete Coordinate Approach to Analytical Modeling of Flexible Bodies 11, to Distribution, Bendix Research Lab, 22 February, 1979.
- 2-3 Lipski, D. B., "Linearized Five Body Space Base Simulation Model", to Distribution, Bendix Research Lab, 23 April, 1979.

SECTION 3

3.0 CONTROL APPROACHES

Three diverse techniques are, in the succeeding subsections, described which are applicable to the control of large, flexible vehicles. The first technique (multilevel control) solves a complex control problem by reducing the solution to a large number of simpler problems. The second approach (LQR) utilizes some of the basic concepts of modern control theory for determining the optimal control loop feedback. The third scheme (MNA) reduces the effective cross-coupling of a complex "plant" to an extent that the closed loop design reduces to a set of independent single loop design problems; techniques for obtaining closed loop pole placement are also utilized in this approach.

The theoretical background and references for each control approach are presented in this section. The actual equations and some simulation results as applied to Configuration 1 of the Space Construction Base are offered in Sections 4, 5 and 6 for the multilevel, LQR and MNA control approaches respectively.

3.1 MULTILEVEL CONTROL

The control of large-scale multivariable systems is a class of control problems that arises in many areas of practical application. Direct application of control to a large-scale system often severely taxes or exceeds available computer capacity due to the high dimensions involved in the overall control problem to be solved. Application of multilevel systems analysis techniques to the large overall control problem decomposes it into

a multilevel hierarchy of subproblems of smaller dimension. An example of a two level subproblem hierarchy is depicted in Figure 3-1.

In general a subproblem hierarchy resulting from the application of multilevel control techniques may contain several levels of subproblems. The roles of the subproblems are correlated with the levels that they occupy in the hierarchy. Each of the subproblems on the lowest (first) level of the hierarchy pertains to a portion of the original system to be controlled. Each of the subproblems on a level above the lowest one pertain to coordination of the solutions of the subproblems on the next lower level. The number of subproblems per level decreases as the level becomes higher in the hierarchy until the top or supremal level is occupied by a single overall coordination subproblem.

Each subproblem comprising the hierarchy transmits its solution(s) to other subproblems in the hierarchy in the course of the solution of the overall control problem. Such a solution proceeds iteratively. For example, the subproblems of the two level hierarchy may be solved in the following sequence. The second level coordination subproblem provides coordination variables, \underline{C} , $\underline{\rho}$, which are held fixed while the optimal solutions for \underline{x} , $\underline{\lambda}$ and \underline{u} are determined for all of the first level subproblems independently. After the optimal solution is obtained for each first level subproblem, numerical responses are sent to the coordination subproblem on the second level. The coordination subproblem

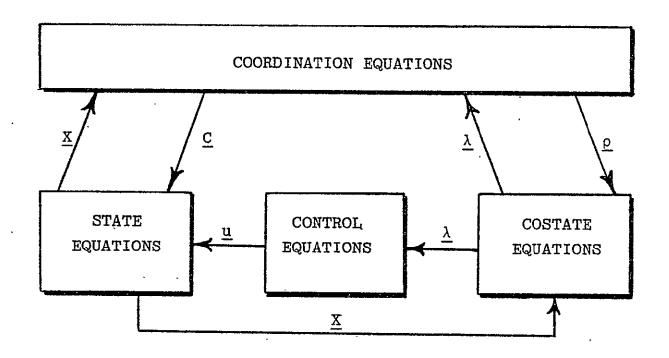


FIGURE 3-1 Two Level Subproblem Hierarchy
For Multilevel Control

now adjusts the coordination variables and sends their adjusted values to the subproblems on the first level. The first level subproblems are again solved independently with the adjusted values of the coordination variables. This procedure continues iteratively until the overall coordination problem at the top of the hierarchy is satisfied. The result sought is an optimized collection of subsystems, with interconnections restored, which is equivalent to the original controlled system optimized. This procedure may be readily extended to subproblem hierarchies with more than two levels.

3.1.1 General Approach

The overall procedure to be utilized in applying multilevel control techniques to a mathematical model of a system to be controlled is outlined as follows:

- 1. Express mathematical model in state variable form.
- 2. Decompose mathematical model into set of decoupled equations.
- 3. Construct decomposed performance index.
- 4. Form decomposed Hamiltonian.
- 5. Develop costate equations with associated coordination equations.
- 6. Develop control algorithm.

- 7. Construct subproblem hierarchy.
- 8. Simulate subproblem hierarchy on digital computer.

3.1.2 State Variable Model

$$\dot{x} = Ax + Bu \tag{3-1}$$

where:

$$x = (x_1, x_2, ---x_n)^{T} \text{ (state vector)}$$
 (3-2)

$$u = (u_1, x_2, ---u_m)^T \text{ (control vector)}$$
 (3-3)

$$A = nxn matrix (3-4)$$

$$B = nxm matrix; m < n (3-5)$$

Equation (3-1) is the canonical state variable form of the mathematical model of the system to be controlled. It represents a set of n simultaneous scalar ordinary linear differential equations which; in general, are coupled.

Typical scalar state equation:

$$\dot{x}_{i} = f_{i}(x,u) = \sum_{j=1}^{n} a_{ij}x_{j} + \sum_{j=1}^{m} b_{ij}u_{j}, i = 1, 2, ---, n \quad (3-6)$$

where
$$f = (f_1, f_2, ---, f_n)^T$$
 (3-7)

3.1.3 Decomposed Model

Define state coordination variables with following coordination equations.

$$C_{i} = g_{i} = \sum_{j=1}^{n} a_{ij}x_{j} + \sum_{j=1}^{m} b_{ij}u_{j}$$

$$j \neq i \qquad j \neq i$$
(3-8)

Then the scalar state equations may be written in decomposed (decoupled) form as follows:

$$\dot{x}_{i} = f_{i} = a_{ii}x_{i} + b_{ii}u_{i} + C_{i}$$
(3-9)

with the initial condition,

$$x_{i}(0) = x_{i0}$$
 (3-10)

3.1.4 Performance Index

Original performance index to be minimized:

$$P = \int_{t_0}^{t_f} (x^T Q x + u^T R u) dt$$
 (3-11)

where

Q = nxn weighting matrix

R = mxm weighting matrix

 t_0 = initial time in interval considered

 t_f = final time in interval considered

If the matrices Q and R are diagonal, the performance index is said to be saparable and it may be written in decomposed (decoupled) form as follows:

$$P = \Sigma P_i$$
 $i = 1, 2, ---, n$ $(3-12)$

where:
$$P_i = \int_{t_0}^{t_f} p_i dt$$
 (3-13)

$$p_i = q_i x_i^2 + r_i u_i^2$$
 for $i = 1, 2, ---m$ (3-14)

$$p_i = q_i x_i^2$$
 for $i = m+1, ---, n$ (3-15)

3.1.5 Hamiltonian

The Hamiltonian is proportional to the energy of the system and may be written in decomposed form as follows:

where:

$$H_{i} = p_{i} + \lambda_{i} f_{i} + \rho_{i} (g_{i} - C_{i})$$
 (3-17)

 λ_i = ith scalar costate variable.

 ρ_i = ith Lagrange multiplier associated with the ith state coordination equation.

According to Pontryagin's minimum principle minimization of the Hamiltonian corresponds to optimization of the controlled system with respect to the performance index given in (3-11). Application of the necessary conditions for minimization of the Hamiltonian of the controlled system generates the costate, control and costate coordination equations for the system to be optimized.

3.1.6 Costate Equations

$$\dot{\lambda}_{i} = -\frac{\partial H}{\partial x_{i}}$$

$$= -a_{ii}\lambda_{i} - 2q_{i}x_{i} - \sum_{\substack{j=1\\ j \neq i}}^{n} a_{ji}\rho_{j}, i = 1, 2, ---, n$$
 (3-18)

with the final condition,

$$\lambda_{i} (t_{f}) = 0 (3-19)$$

3.1.7 Costate Coordination Equations

$$\frac{\partial H}{\partial C_{i}} = 0 \rightarrow \rho_{i} = \lambda_{i}; \quad i = 1, 2, ---, n$$
 (3-20)

3.1.8 Control Equations

For a system that is operating suboptimally with respect to its performance index, some of the necessary optimality conditions applied to its Hamiltonian will not be satisfied at the outset. The selection of the specific set of necessary conditions to be temporarily violated at the beginning of operation of the system determines the nature of the decomposition of the system. In this case it is assumed that the system decomposition is such that all of the necessary conditions listed so far, (3-18), (3-20), and the necessary conditions leading to the state and state coordination equations are satisfied throughout the time interval of interest, (t_o,t_f). Given these conditions, for suboptimal operation at the outset, the necessary condition associated

with the control variables cannot be satisfied at the outset. It is therefore approached during the operation of the system by means of the following gradient formulation.

$$(u_i)_{\ell+1} = (u_i)_{\ell} - s_i (\frac{\partial H}{\partial u_i})_{\ell}, i = 1, 2, ---, m$$
 (3-21)

where:

l = the iteration subscript

s_i = constants to be chosen on the basis of the rate of approach of the controlled system to optimal operation.

From (3-8), (3-9), (3-14) and (3-17) an expression may be written for the gradient of the Hamiltonian with respect to each scalar control variable as follows.

$$\frac{\partial H}{\partial u_{i}} = 2r_{i}u_{i} + \sum_{j=1}^{n} b_{ji}\lambda_{j}$$
 (3-22)

3.1.9 Subproblem Hierarchy

Equations (3-8) and (3-20) may be assembled into an overall coordination subproblem for the generation of the optimal control contours. Equations (3-9) with their associated initial conditions, equations (3-10), constitute the first level state subproblems to be solved. Since these equations are temporarily decoupled from each other, they may be regarded as n subproblems each of which can be solved independently. Similarly, (3-18) with the final conditions of (3-19) may be associated into a first

level costate subproblem and (3-21) and (3-22) may be assembled into an overall control subproblem. These four subproblems may then be assembled into a hierarchy with the coordination subproblem at its apex as shown in Figure 3-1.

3.2 LINEAR QUADRATIC REGULATOR (LQR)

With a linear system described in the state variable form

$$\dot{x} = Ax + Bu \tag{3-23}$$

where x = the system state variable vector

u = the control vector

A,B =the system matrices,

an optimum feedback control u = Fx can be determined by utilizing Pontryagin's minimum principle.

An expression for the optimum feedback F can be derived (References 3-4 and 3-5) through application of either Hamilton-Jacobi equations or utilizing the second method of Liapunov with a "quadratic cost" system performance index.

$$p_{F} = \int_{0}^{T} (x^{T}Q_{X} + u^{T}Ru) dt \qquad (3-24)$$

where T = upper limit in time (could also be infinite in. some derivations)

Q,R = weighting factors, where Q must be at least a positive semidefinite matrix and R must be positive definite

For an initial state x(0), a matrix Riccati equation is generated by either approach from (3-23) and (3-24),

$$-P = PA + A^{T}P - PBR^{-1} B^{T}P + Q$$
 (3-25)

where P = P(t) and must be positive definite P = P(t).

and the equation is subject to the boundary condition P(T) = 0. Ordinarily, this equation can be integrated backward in time from the known terminal condition over the time period of interest. P approaches zero as T is increased towards infinity, and the P matrix becomes a constant designated as \overline{P} . The optimum feedback matrix is then

$$F = -R^{-1}B^{T}\overline{P} \tag{3-26}$$

as derived from the approaches cited. Equation (3-23) can now be rewritten as a function of the state variables only

$$\dot{x} = (A-BF)x = (A+BR^{-1}B^{T}\overline{P})x \qquad (3-27)$$

Note that this equation implies that <u>all</u> the state variables must be fed back to obtain an optimal control system. Careful selection of state variables, or filtering of a set of measured variables, will be required

for feedback control of large flexible vehicles. These structures are actually a network of distributed spring and mass parameters, rather than a finite number of discrete or lumped elements.

An application of the LQR technique to the control of a flexible vehicle, represented by discrete parameters, is demonstrated in Section 5 of this report. A solution of the system's matrix Riccati equation is given, along with an optimal closed loop simulation.

3.3 MULTIVARIABLE NYQUIST ARRAY (MNA)

The MNA control method used here is combined with a pole placement technique. The basic MNA approach will be described first and will then be followed by a brief description of the pole placement procedure.

3.3.1 MNA Design Procedure

The fundamental objective of the MNA design method is to decrease crosscoupled system interaction to such an extent that the closed loop system design reduces to a set of independent single loop design problems. Although simply stated, the actual reduction procedure proposed by Rosenbrock (Reference 3-6) and implemented by Munro (Reference 3-7) requires a high degree of designer intervention and is fundamentally a trial and error process.

In Figure 3-2, G(S) is an mxm transfer matrix representing the coupling of m inputs and m outputs. Restriction of G(s) to a square matrix simplifies the analysis, programming and computational effort considerably.

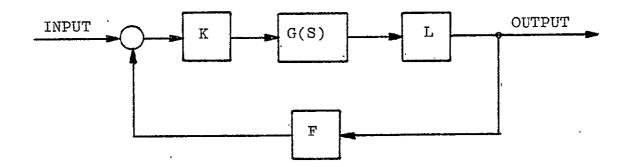


FIGURE 3-2 MULTIVARIABLE SYSTEM CONFIGURATION

The pre- and post-compensator matrices K and L, respectively are each of dimension mxm. The feedback gain matrix, F, is assumed to be diagonal and of similar dimensions. Clearly, if

$$Q(S) = LG(S)K (3-28)$$

is diagonal, loop closure may proceed on an individual loop basis with a guarantee of zero loop interaction. It is this premise upon which the MNA design philosophy is based. The adherence to strict diagonalization is relaxed, however, with the substitution and exploitation of the concept of diagonal dominant matrices.

A matrix Z(S) is diagonal dominant if either or both of the following conditions are present for all S:

a.
$$\begin{array}{c|c} m \\ \Sigma \\ j=1 \\ i\neq j \end{array} |z_{ij}(S)|/|z_{ii}(S)| \leq \theta_i < 1 \text{ for all } i=1,2,---m \ (3-29)$$

b.
$$\sum_{\substack{j=1\\j\neq i}}^{m} |z_{ji}(S)|/|z_{ii}(S)| \leq \theta_{i} < 1 \text{ for all } i = 1,2,---m \quad (3-30)$$

Equation (3-29) defines row dominance while (3-30) defines the column dominance condition where θ_i is the level of dominance obtained for the ith diagonal element.

Before the design process can proceed further, Q(S) for the direct Nyquist array (DNA) method or $Q^{-1}(S)$ in the inverse Nyquist array (INA) method must be made dominant by manipulation of the elements of the compensator matrices. Once dominance is achieved the design process is completed using single loop theory to select the diagonal elements of F. This selection process is enhanced through application of the Gershgorin and the Ostrowski theorems for dominant matrices.

The Gershgorin theorem (Reference 3-6) states that the eigenvalues of a matrix (either Q(S) or Q⁻¹(S)) are located in the union of the bands centered about the diagonal elements with widths determined by the sum of the moduli of the off diagonal elements by row or by column. Using the envelope procedure developed by Crossley (Reference 3-8) and considering each control loop separately, a graphical display of open loop system interaction results. The feedback gain selection for control loop i is then made in correspondence with the generalized Nyquist criterion and the stability theorems of Rosenbrock (Reference 3-6).

The Ostrowski theorem may be used to further shrink the Gershgorin bands, thereby reducing the area of uncertainty in each loop. This set of bands is frequently referred to as a set of "fuzzy" Nyquist plots (or inverse Nyquist plots for the INA). Using the innermost band as a conservative estimate of the Nyquist contour in each loop, the design proceeds on a single loop basis. Feedback gain selection must be made exterior to the Gershgorin (Ostrowski) band. Thus, phase margin, gain margin and dynamic compensation may be used to evaluate and/or improve the loop design with a guarantee of low interaction from the closure of the remaining loops.

Diagonal dominance for the DNA method requires the selection of pre- and post-compensator matrix parameters so that (3-29) is satisfied when (3-28) represents the open loop transfer matrix. For the INA method $Q^{-1}(S)$ is used and the parameters of K^{-1} and L^{-1} must be selected.

An efficient and reliable method for the evaluation of the matrix coefficients is described in Reference 3-9. The dominance algorithm uses a conjugate direction function minimization algorithm to adjust the parameter set until a performance index composed of the dominance definitions in (3-29) and (3-30) is minimized. For the INA method in a row dominance mode, the optimization problem can be separated into three independent optimization efforts; one for each row. Here the performance index by row is

$$J_{i}(K_{ij}) = Max \quad \sum_{\substack{j=1\\i\neq i}}^{m} |\hat{q}_{ij}(S)| / |\hat{q}_{ii}(S)|, i=1,2,---,m \quad (3-31)$$

where $\hat{q}_{ij}(S)$ is an element of $Q^{-1}(S)$. For each i, the ith row of K^{-1} is adjusted until $J_i(K_{ij})$ is minimized. In practice, the ratio in (3-31) is computed for each discrete frequency point in the range of interest. This array is then scanned to identify the maximum ratio. Adjusting the elements of row i in K^{-1} yields a set of final dominance levels

$$\Theta_{i} = \underset{K_{ij}}{\text{Min }} J_{i}(K_{ij})$$
 (3-32)

If the dominance levels in (3-32) are less than unity, diagonal dominance has been achieved. In the event that some of the dominance levels are greater than one, the designer may initiate a dominance sharing search or restart the program using new starting values for the unspecified compensator parameters.

The concept of dominance sharing is detailed in Reference 3-10. It is fundamentally a rescaling of the compensator matrices to the extent that low dominance levels may be intentionally increased to a point where the previous non-dominant levels may be shifted to a range of acceptability. This procedure has been automated in the latest version of the dominance algorithm and is initiated by the designer after the final set of dominance levels have been evaluated.

Once a set of coefficients has been determined for dominance of the open loop transfer matrix, each control loop may be treated independently using single-input/

single-output control theory. The dominance algorithm briefly outlined above shifts the burden of establishing the dominance condition from the designer to an automated procedure. Thus designer intervention is only required during the actual design process and is no longer needed to establish the requisite dominance condition. Experience with the algorithm suggests that dominance may often be obtained within several CPU minutes or less depending upon the characteristics of G(S).

Using the appropriate transfer functions for the vehicle model, a DNA design was initiated over a frequency range which includes the critical modes. Recent results described in reference 3-11 for finite frequency Nyquist array design established this range as acceptable for design and stability purposes. For this DNA design the post compensator matrix was prespecified as the identity matrix with the precompensator matrix selected in accordance with the dominance algorithm in reference 3-9. The closed loop diagram for vehicle control, with

$$Q(S) = L G(S)K$$

representing the open loop transfer matrix, is shown in Figure 3-3.

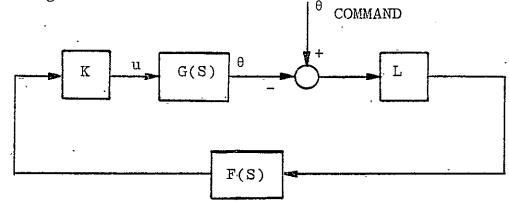


Figure 3-3 Closed Loop Spacecraft Control Design

3.3.2 Retallack Pole Placement Method

The dyadic pole placement technique developed by Simon and Mitter, reference 3-12, and further refined by Retallack and MacFarlane, reference 3-13, utilizes the model structure of a linear system to give the designer direct control over the movement of given system modes to desired closed loop locations. This method is particularly attractive from a design viewpoint whenever the open loop poles can be directly associated with specific parts of the physical system. In this way only those poles directly associated with the subsystem will be shifted. Let λ_j (j=1,...,n) represent the open loop poles of the system and let $\rho_{i}(i=1,\ldots,n)$ be the desired closed loop set. Several algorithms are presently available to shift the eigenvalue set $\{\lambda_{j}\}$ to the desired set $\{\rho_i\}$. However there is no guarantee that any particular eigenvalue $\boldsymbol{\lambda}_k$ will be moved to a specific location ρ_k . Without the eigenvalue location assignment flexibility, the resulting control in light of sensor and/or actuator failures could result in very unsatisfactory performance.

Consider the linear, time-invariant, multivariable system described by

$$\dot{x}$$
 =Ax+Bu (3-34)

where x is n vector of states, u is m vector of inputs and $m \le n$. If constant gain state feedback of the form $u = \gamma - Kx$ (3-35)

is introduced into the system of (3-34) the resulting

system obeys

$$\dot{x} = (A - BK)x + By \tag{3-36}$$

where γ is the external control. The open-loop poles $(\lambda_1,\ldots,\lambda_n)$ of the system of (3-34) and the closed loop poles (ρ_1,\ldots,ρ_n) of the system (3-36) are related by the Hsu-Chen equation (reference 3-14).

$$|I_{n}-(SI_{n}-A)^{-1}BK| = \frac{\prod_{i=1}^{n} (S-\rho_{i})}{\prod_{j=1}^{n} (S-\lambda_{j})}$$

The Jordan canonical form for A is given by

$$\Lambda = U^{-1}AU \tag{3-38}$$

where U is a modal matrix for A. Let $(\lambda_1, \lambda_2, \ldots, \lambda_p)$ p<m be the open loop poles to be shifted and define the modal controller K in terms of the unity rank dyadic product

$$K=fd^{T}V$$
 (3-39)

where f is an m vector d is a p vector and V contains the prows of U^{-1} corresponding to $(\lambda_1,\ldots\lambda_p)$. With this definition, K Retallack (reference 3-13) reduces equation (3-37) to

$$1 + d^{T}(SI_{p} - \tilde{\Lambda})^{-1} \beta = \frac{\prod_{i=1}^{m} (S - \rho_{i})}{\prod_{j=1}^{p} (S - \lambda_{j})}$$
(3-40)

where

$$\beta = VBf \qquad (3-41)$$

and $\tilde{\Lambda}$ is the pxp Jordan submatrix for $(\lambda_1, \lambda_2, \dots \lambda_p)$. The remaining open-loop modes $(\lambda_p+1, \dots \lambda_n)$ are unchanged

under dyadic feedback.

To overcome some of the numerical difficulties associated with the computation of the modal controller when clustered poles appear near the imaginary axis (reference 3-15) the system in (3-34) is transferred to the Luenberger canonical form (reference 3-16),

$$\hat{\mathbf{w}} = \hat{\mathbf{A}}\hat{\mathbf{w}} + \hat{\mathbf{B}}\mathbf{u} \tag{3-42}$$

where w=U-1x

$$\hat{A} = U^{-1} \hat{A} U$$
 (3-43)
 $\hat{B} = U^{-1} \hat{B}$ (3-44)

$$\hat{B} = U^{-1}B$$
 (3-44)

An efficient algorithm to realize this transformation is presented in reference 3-17. Since the eigenvalues of $(\hat{A}-\hat{B}\hat{K})$ are identical to those of (A-BK), the pole placement process can be accomplished in the closed loop system of (3-42), rather than in the closed loop system of (3-34). Once the gain matrix K has been determined for the canonical system, the desired modal controller K for the original system (3-34), is given by

$$K = \hat{K}U^{-1} \tag{3-45}$$

This pole placement method was used in this study to shift the open loop poles of the vehicle model for analysis and control system design purposes.

3.4 REFERENCES

- 3-1 Wismer, D.A., "Optimal Control of Distributed Parameter Systems Using Multilevel Techniques", Ph.D. dissertation, University of California, Los. Angeles, 1966.
- 3-2 Chichester, F.D., "Application of Multilevel Control Techniques to Classes of Distributed Parameter Plants", Dr. Eng. Sci. dissertation, New Jersey Institute of Technology, 1976.
- 3-3 Chichester, F., "Application of Multilevel Control to a Single Axis Torsional System, Bendix Corporation MT-40,808. Issue A, May 16, 1978.
- 3-4 Melsa, J.L. and Schultz, D.G., State Functions and Linear Control Systems, 1967, McGraw-Hill
- 3-5 Kwakernaak, H. and Sivan, R., Linear Optimal Control Systems, 1972, Wiley-Interscience.
- 3-6 Rosenbrock, H.H., Computer-Aided Control System Design, Academic Press (London), 1974.
- 3-7 Munro, N., "Conversational Mode CAD of Control System", IEE Int. Conf. on CAD, England, 1972.

- 3-8 Crossley, T.R., "Envelope Curves to Inverse Nyquist Array Diagrams", Int. J. Control, Vol. 22, No. 1, 1975.
- 3-9 Leininger, G.G., "Diagonal Dominance for Multivariable Nyquist Array Methods Using Function Minimization", Automatica, Vol. 15, No. 3, pp. 339-346, 1979.
- 3-10 Leininger, G.G. "The MNA-Concept of Dominance Sharing," NEC International Forum on Alternatives for Linear Multivariable Control, Chicago, 1977.
- 3-11 Leininger, G.G. "New Dominance Characteristics for the Multivariable Nyguist Array Method", to Appear International Journal of Control, 1979.
- 3-12 Simon, J.D. and Mitter, S.K., "A Theory of Modal Control", Information and Control, Vol. 13, No. 4, pp. 316-353, October 1968.
- 3-13 Retallack, D.G. and MacFarlane, A.G.J., "Pole-shifting Techniques for Multivariable Feedback Systems", Proc, IEE, Vol. 117, No. 5, pp. 1037-1038, May 1970.
- 3-14 Hsu, C.H. and Chen, C.T.", A Proof of the Stability of Multivariable Feedback Systems", Proc. IEEE, Vol. 56, pp. 2061-2062, 1968.

- 3-15 Wu, Y.W. Juang, J.N. and Rice, R.B., "Control of Large Flexible Space Structure Usign Pole Placement Design Techniques", AIAA Guidance and Control Conference, Boulder, Colorado, August, 1979.
- 3-16 Luenberger, D.G., "Canonical Forms for Linear Multivariable Systems", IEEE-AC, Vol. AC-12, pp. 290-293, June 1967.
- 3-17 Jordan, Dr., and Sridhar, B., "An Efficient Algorithm for the Calculation of the Luenberger Canonical Form", IEEE-AC, Vol. AC-18, pp. 292-295, June 1973.

SECTION 4

4.0 SIMULATION OF MULTILEVEL CONTROL

The principal objective of this section is the development of mathematical models of a flexible space vehicle that are amenable to application of multilevel control techniques and construction of digital computer simulations of each vehicle model and its associated multilevel control system. In this development effort mathematical models for attitude stabilization of the Space Construction Base (SCB) have been utilized because these models are deemed representative of the corresponding models of flexible space vehicles in general and because data were available at the outset for the SCB models.

The effort expended on the simulation of models of the vehicle with multilevel control since the last report, Chichester (4-1), has been divided into three main areas which are discussed in subsections 4.1, 4.2 and 4.3, respectively. Subsection 4.1 describes the development of a linearized scalar state variable form of the three dimensional discrete mass rotational model for Configuration 1 of the SCB from the model originally presented by Cornell (4-2). This subsection summarizes work presented in Lipski (4-3) and (4-4), and Chichester (4-5). The resulting models are suitable for direct application of multilevel control techniques.

Subsection 4.2 presents the application of multilevel. control techniques to the models of subsection 4.1. This application follows the sequence previously described in Chichester (4-1), (4-6). The resulting model is of rather high dimension for all but the minimum

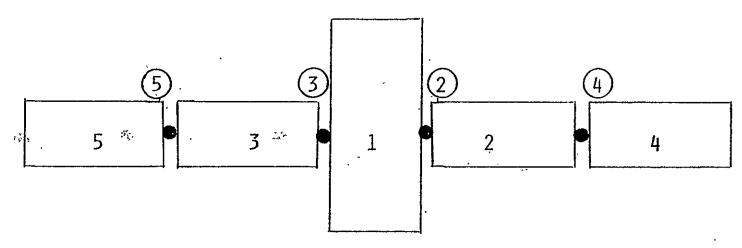
form of the SCB, Configuration 1, and the most limited application of control torques, application to the central body only.

Subsection 4.3 describes simple hybrid coordinate models of Configuration 1 of the SCB, linear models of lower dimension than the corresponding models of subsection 4.1. This subsection concludes with the application of multilevel control techniques to these hybrid coordinate models. The approach presented in this subsection is based upon work appearing in Likins (4-7) and Chichester, Kaczynski and Nachmias (4-8).

Subsection 4.4 presents conclusions based upon the work presented in Subsections 4.1 through 4.3 and recommendations for future work in the application of multilevel control to models of flexible space vehicles.

4.1 LINEARIZED THREE-DIMENSIONAL DISCRETE MASS ROTATIONAL MODEL FOR CONFIGURATION 1.

Configuration 1 of the SCB consists of two solar wings connected to four contiguous modules which are considered to be rigid relative to the solar wings. The simulation model for this configuration was derived using the discrete coordinate approach and approximation by five rigid bodies. Each solar wing was converted to two rigid bodies with overall designations as shown in Figure 4-1.



(The individual bodies are connected to each other via three degree of freedom spring hinge suspensions. Hinge numbers are circled.)

TOPOLOGICAL DIAGRAM OF SCB CONFIGURATION 1
FIGURE 4-1

4.1.1 Definitions

A Skew-symmetric matrix of the Gibbsian vector A.

$$\tilde{A} \quad \underline{\Delta} \begin{bmatrix} 0 & -a_z & a_y \\ a_z & 0 & -a_x \\ -a_y & a_z & 0 \end{bmatrix}$$

R_{i,j} Vector from C.M. of body i to hinge j in body i coordinates.

 $\dot{\omega}_{i}$ Inertial angular acceleration vector of body i expressed in body i coordinates.

 $A_{i,j}$ 3 x 3 submatrix of the 15 x 15 coefficient matrix as shown in paragraph 2.

 $\mathbf{j}^{T}_{\mathbf{i}}$ 3 x 3 transformation matrix from body i coordinates to body j coordinates.

m; Mass of body i.

ΣM Sum of masses of all five bodies.

I, Inertia matrix of body i.

A^T Matrix transpose of A.

 $\omega_{Ri,j} \triangleq \omega_i \times (\omega_i \times R_{i,j})$

T_{ei} External torque vector on body i.

Tai Actuator or control torque vector on body i.

T_{si,j} Suspension torque vector between bodies i and j.

4.1.2 Rotational Equations of Motion

The rotational equations of motion were derived using the method of discrete coordinates and take the generalized form:

For convenience, (4-1) can be expressed in terms of 3 x 3 submatrices and Gibbsian vectors as:

$$\begin{bmatrix} A_{1,1} & A_{1,2} & A_{1,3} & A_{1,4} & A_{1,5} \\ A_{2,1} & A_{2,2} & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & &$$

For the linearized discrete mass model,

$$i^{T}j$$
 = $\begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \bigvee i \text{ and } j$ (4-3)

Since the elements of the linearized coefficient matrix are constant, the matrix inverse need be computed only initially. Appropriate symmetry conditions for the linearized model of Configuration 1, may be stated as follows:

$$m_3 = m_2$$
 $m_5 = m_4$
 $I_3 = I_2$
 $I_5 = I_4$
 $R_{1,3} = R_{1,2}$
 $R_{3,3} = R_{2,2}$
 $R_{3,5} = R_{2,4}$
 $R_{5,5} = R_{4,4}$

Using skew-symmetric matrices as defined and the above listed symmetry properties, the 3×3 sub-matrices of (4-2) take the following form.

$$A_{1,1} = I_1 - 2(m_2 + m_4) \left[1 - 2(\frac{m_2 + m_4}{\Sigma M})\right] \tilde{R}_{1,2} \tilde{R}_{1,2}$$
 (4-5)

$$A_{2,2} = I_{2} + (m_{2} + m_{4}) \left(\frac{m_{2} + m_{4}}{\Sigma M} - 1\right) \tilde{R}_{2,2} \tilde{R}_{2,2}$$

$$+ m_{4} \left(1 - \frac{m_{2} + m_{4}}{\Sigma M}\right) \left\{\tilde{R}_{2,2} \tilde{R}_{2,4} + \tilde{R}_{2,4} \tilde{R}_{2,2}\right\}$$

$$+ m_{4} \left(\frac{m_{2}}{\Sigma M} - 1\right) \tilde{R}_{2,4} \tilde{R}_{2,4} = A_{3,3}$$

$$(4-6)$$

$$A_{4,4} = I_4 + m_4 (\frac{m_4}{\Sigma M} - 1) \qquad \tilde{R}_{4,4} \tilde{R}_{4,4} = A_{5,5}$$
 (4-7)

$$A_{1,2} = (m_2 + m_4) \{1 - 2(\frac{m_2 + m_4}{\Sigma M})\} \{\tilde{R}_{1,2} \tilde{R}_{2,2} + \tilde{R}_{1,2} \tilde{R}_{2,4} \}$$

$$= A_{1,3} = A_{2,1}^T = A_{3,1}^T$$
 (4-8)

$$A_{1,4} = m_{4} \{1 - 2(\frac{m_{2} + m_{4}}{\Sigma M})\} \quad \tilde{R}_{1,2} \quad \tilde{R}_{4,4} = A_{1,5}$$

$$= A_{4,1}^{T} = A_{5,1}^{T}$$
(4-9)

$$A_{2,3} = (m_2 + m_4) (\frac{m_2 + m_4}{\Sigma M}) \tilde{R}_{2,2} \tilde{R}_{2,2}$$

$$-(\frac{m_2 + m_4}{\Sigma M}) m_4 \tilde{R}_{2,2} \tilde{R}_{2,4} + \tilde{R}_{2,4} \tilde{R}_{2,2}$$

$$-\frac{m_4^2}{\Sigma M} \tilde{R}_{2,4} \tilde{R}_{2,4} = A_{3,2}$$

$$(4-10)$$

$$A_{2,4} = m_4 \left(\frac{m_2 + m_4}{\Sigma M} - 1 \right) \quad \tilde{R}_{2,2} \quad \tilde{R}_{4,4} + m_4 \left(1 - \frac{m_4}{\Sigma M} \right) \quad \tilde{R}_{2,4} \quad \tilde{R}_{4,4}$$

$$= A_{3,5} \quad = A_{4,2} \quad = A_{5,3} \quad (4-11)$$

$$A_{2,5} = m_4 \left(\frac{m_2 + m_4}{\Sigma M}\right) \tilde{R}_{2,2} \tilde{R}_{4,4} - \frac{m_4^2}{\Sigma M} \tilde{R}_{2,4} \tilde{R}_{4,4} \quad (4-12)$$

$$= A_{3,4} = A_{5,2}^T = A_{4,3}^T$$

$$A_{4,5} = \frac{m_4^2}{\Sigma M} \tilde{R}_{4,4} \tilde{R}_{4,4} = A_{5,4}^T \quad (4-13)$$

In the expansions of the 3×3 linearized coefficient submetrices of (4-5) through (4-13) triple vector products of the following form occur repeatedly.

$$R_{ik} \times (\dot{\omega}_{j} \times R_{j\ell}) = -\left[\tilde{R}_{ik} \tilde{R}_{j\ell} \right] \dot{\omega}_{j}$$
 (4-14)

These triple vector products may be transformed to the following form in order to derive the expressions for each element of the 3 x 3 coefficient submatrices

$$-\begin{bmatrix} \tilde{R}_{ik} & \tilde{R}_{jl} \end{bmatrix} \dot{\omega}_{j} = \begin{bmatrix} e_{11} & e_{12} & e_{13} \\ e_{21} & e_{22} & e_{23} \\ e_{31} & e_{32} & e_{33} \end{bmatrix} \begin{bmatrix} \dot{\omega}_{jx} \\ \dot{\omega}_{jy} \\ \dot{\omega}_{jz} \end{bmatrix}$$
(4-15)

The elements of the coefficient matrix in (4-15) can be expressed in terms of the scalar components of R_{ik} and $R_{j\ell}$ as follows.

$$e_{11} = R_{iky} R_{jly} + R_{ikz} R_{jlz}$$

$$e_{12} = -R_{iky} R_{jlx}$$

$$e_{13} = -R_{ikz} R_{jkx}$$

$$e_{21} = -R_{ikx} R_{jky}$$

$$e_{22} = R_{ikx} R_{jkx} + R_{ikz} R_{jkz}$$

$$e_{23} = -R_{ikz} R_{jky}$$

$$e_{31} = -R_{ikx} R_{jkz}$$

$$e_{32} = -R_{iky} R_{jkz}$$

$$e_{33} = R_{ikx} R_{jkx} + R_{iky} R_{jky}$$

The linearized vector components of the right side of (4-2) are the following vector sums:

$$C_{1} = T_{e1} + T_{a1} - T_{s1,2} - T_{s1,3}$$

$$C_{2} = T_{e2} + T_{a2} + T_{s1,2} - T_{s2,4}$$

$$C_{3} = T_{e3} + T_{a3} + T_{s1,3} - T_{s3,5}$$

$$C_{4} = T_{e4} + T_{a4} + T_{s2,4}$$

$$C_{5} = T_{e5} + T_{a5} + T_{s3,5}$$

$$(4-17)$$

4.1.3 Euler Angle Equations

Relative Euler angle rates between bodies 1 and 2,
bodies 1 and 3, bodies 2 and 4 and, bodies 3 and 5

are used based on a ψ , θ , ϕ rotational sequence about the Z, Y and X axes respectively. Euler rates are also determined relating body 1 to inertial space. Assuming small angles, the rates become:

4.1.4 Suspension Equations

The following torque equations are given in terms of rate and displacement constants (program parameters) and inertial rate differences and relative displacements.

$$T_{s1,2x} = -K_{s1,2x}^{\Delta\phi}_{1,2}^{-C}_{s1,2x}^{C\omega}_{2x}^{-\omega}_{1x}$$

$$T_{s1,2y} = -K_{s1,2y}^{\Delta\phi}_{1,2}^{-C}_{s1,2y}^{C\omega}_{2y}^{-\omega}_{1y}) \qquad (4-23)$$

$$T_{s1,2z} = -K_{s1,2z}^{\Delta\psi}_{1,2}^{-C}_{s1,2z}^{C\omega}_{2z}^{-\omega}_{1z})$$

$$T_{s1,3x} = -K_{s1,3x}^{\Delta\phi}_{1,3}^{-C}_{s1,3x}^{C\omega}_{3x}^{-\omega}_{1x})$$

$$T_{s1,3y} = -K_{s1,3y}^{\Delta\phi}_{1,3}^{-C}_{s1,3y}^{C\omega}_{3y}^{-\omega}_{1y}) \qquad (4-24)$$

$$T_{s1,3z} = -K_{s1,3z}^{\Delta\psi}_{1,3}^{-C}_{s1,3z}^{C\omega}_{3z}^{-\omega}_{1z})$$

$$T_{s2,4x} = -K_{s2,4x}^{\Delta\phi}_{2,4}^{-C}_{s2,4x}^{C\omega}_{4x}^{-\omega}_{2x})$$

$$T_{s2,4y} = -K_{s2,4y}^{\Delta\phi}_{2,4}^{-C}_{s2,4y}^{C\omega}_{4y}^{-\omega}_{2y}) \qquad (4-25)$$

$$T_{s2,4z} = -K_{s2,4z}^{\Delta\psi}_{2,4}^{-C}_{s2,4z}^{C\omega}_{4z}^{-\omega}_{2z})$$

$$T_{s3,5x} = -K_{s3,5x}^{\Delta\phi}_{3,5}^{-C}_{s3,5x}^{(\omega}_{5x}^{-\omega}_{3x})$$

$$T_{s3,5y} = -K_{s3,5y}^{\Delta\theta}_{3,5}^{-C}_{s3,5y}^{(\omega}_{5y}^{-\omega}_{3y})$$

$$T_{s3,5z} = -K_{s3,5z}^{\Delta\psi}_{3,5}^{-C}_{s3,5z}^{(\omega}_{5z}^{-\omega}_{3z})$$

$$(4-26)$$

4.1.5 Rotational State Equations

The rotational equations of motion, (4-1) and the Euler angle rate equations (4-18) through (4-22), may be transformed to scalar state variable form as follows:

<u>Definition of State Variables</u>

$$YO_{1} = \omega_{1x}$$
 $YO_{2} = \omega'_{1y}$
 $YO_{3} = \omega_{1z}$
 $YO_{4} = \omega_{2x}$
 $YO_{5} = \omega_{2y}$
 $YO_{6} = \omega_{2z}$
 $YO_{7} = \omega_{3x}$
 $YO_{8} = \omega_{3y}$
 $YO_{9} = \omega_{3z}$
 $YO_{10} = \omega_{4x}$
 $YO_{11} = \omega_{4y}$
 $YO_{12} = \omega_{4z}$
 $YO_{13} = \omega_{5x}$

$$yo_{14} = \omega_{5y}$$

$$yo_{15} = \omega_{5z}$$

$$yo_{16} = \Delta \phi_{2,4}$$

$$yo_{17} = \Delta\theta_{24}$$

$$yo_{18} = \Delta \psi_{24}$$

$$yo_{19} = \Delta \phi_{3,5}$$

$$yo_{20} = \Delta\theta_{35}$$

$$YO_{21} = \Delta \psi_{3,5}$$

$$yo_{22} = \Delta \phi_{1,2}$$

$$YO_{23} = \Delta\theta_{12}$$

$$yo_{24} = \Delta \psi_{1,2}$$

$$YO_{25} = \Delta \phi_{1,3}$$

$$yo_{26} = \Delta\theta_{1,3}$$

$$yo_{27} = \Delta \psi_{1,3}$$

$$yo_{28} = \phi_1$$

$$yo_{29} = \theta_1$$

$$yo_{30} = \psi_1$$

$$\underline{\text{YO}}_{1} = (\text{YO}_{1}, \text{YO}_{2}, ----, \text{YO}_{1\overline{5}})^{\text{T}}$$
 (4-28)

$$\underline{yo}_2 = (yo_{16}, yo_{17}, ----, yo_{30})^T$$
 (4-29)

$$FT_i = C_i \quad i=1,2,---,15$$
 (4-30)

$$\underline{FT} = (FT_1, FT_2 ---, FT_{15})^T \qquad (4-31)$$

Using the state variable definitions in (4-27), the right hand sides of (4-18) through (4-22) may be written in the following form:

$$D_{i} = YO_{i-6} - YO_{i-12}; i = 16, 17, ---21$$
 (4-32)

$$D_{i} = YO_{i-18} - YO_{i-21}; i = 22,23,24$$

$$D_{i} = YO_{i-18} - YO_{i-24}; i = 25,26,27$$

$$D_{i} = YO_{i-18} - YO_{i-24}; i = 25,26,27$$

$$D_{i} = YO_{i-27}; i = 28,29,30$$

$$(4-34)$$

$$D_{i} = YO_{i-18} - YO_{i-24}; i = 25, 26, 27$$
 (4-34)

$$D_i = YO_{i-27};$$
 $i = 28,29,30$ (4-35)

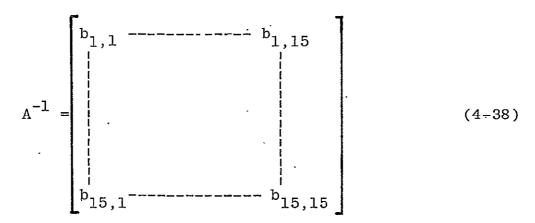
Substitution of (4-27) through (4-31) into (4-1) yields the following:

$$\underline{\underline{YO}}_{1} = A^{-1}\underline{FT} \tag{4-36}$$

where

$$A = \begin{bmatrix} a_{1,1} & & & a_{1,15} \\ & & & & \\ & & & & \\ a_{15,1} & & & & a_{15,15} \end{bmatrix}$$
 (4-37)

With the substitution,



(4-36) may be written in the following form.

$$\stackrel{\bullet}{\text{YO}}_{i} = \stackrel{15}{\sum}_{J=1}^{b} i, j^{\text{FT}}_{j}(\underline{\text{YO}}_{1}, \underline{\text{YO}}_{2}); i = 1, 2, ---15$$
(4-39)

Substitution of (4-27, (4-29)) and (4-32) through (4-35) into (4-18) through (4-22) yields the following form of the Euler rate equations.

$$\dot{YO}_{i} = D_{i} (\underline{YO}_{1}, \underline{YO}_{2}); i = 16, 17, ---30$$
 (4-40)

The set of equations (4-39) and 4-40) constitutes the scalar rotational state equations for the discrete mass mathematical model of SCB Configuration 1. This set of equations is linear and coupled in the state variables, YO_{1} . Since A is a constant matrix, A^{-1} is also and each YO_{1} is a linear function of the scalar components of YO_{1} and YO_{2} .

4.2 APPLICATION OF MULTILEVEL CONTROL TECHNIQUES TO A LINEARIZED DISCRETE MASS MODEL

The overall approach utilized in applying multilevel control techniques was outlined in a memorandum by Chichester (4-6) as follows:

- 1. Decompose mathematical model into a set of decoupled equations.
- 2. Construct performance index and form Hamiltonian.
- 3. Develop costate equations with associated coordination equations.
- 4. Develop control algorithm.
- 5. Construct subproblem hierarchy.
- 6. Discretize equations of each subproblem.

4.2.1 Decomposition

The first step in the application of multilevel control techniques to a system in coupled state variable form is the decomposition of the model to temporarily suppress the coupling between the equations of which it is comprised. With the omission of external and actuator torque terms, (4-40) may be written in the following form:

$$_{i}^{\bullet} = DTS_{i}^{*}YO_{i} + TSC_{i}(YO_{k}), k \neq i, i = 1, 2, ---15 (4-41)$$

$$DTS_{i} = \sum_{j=1}^{15} b_{i,j} \frac{\partial FT_{j}}{\partial YO_{i}}$$

$$TSC_{i} = \sum_{j=1}^{15} b_{i,j} \sum_{k=1}^{27} \frac{\partial FT_{j}}{\partial YO_{k}} *YO_{k}$$

$$k \neq i$$

$$(4-42)$$

27
$$\Sigma \quad \text{DTSC}_{i,k} \quad \text{YO}_{k}$$

$$k \neq i$$

$$(4-43)$$

$$DTSC_{i,k} = \frac{\partial TSC_{i}}{\partial YO_{k}} = \sum_{j=1}^{15} b_{i,j} \frac{\partial FT_{j}}{\partial YO_{k}}$$
(4-44)

From (4-17) and (4-23) through (4-27) it is evident that the partial derivatives in (4-42) and (4-43) are constants that can be determined.

All of the coupling terms in (4-39) are summed in (4-43). The rotational state coordination variables may thus be defined as follows:

$$D_{i} = \sum_{\substack{k=1\\k\neq i}}^{27} DTSC_{i,k} *YO_{k} \qquad i = 1, 2, ---15 \qquad (4-45)$$

With the external and actuator torque terms restored, the decomposed form of the first 15 rotational state equations may be written in the following form:

$$\overset{\bullet}{\text{YO}}_{\mathbf{i}} = \text{DTS}_{\mathbf{i}} * \text{YO}_{\mathbf{i}} + \text{D}_{\mathbf{i}} + \overset{15}{\sum} b_{\mathbf{i}\mathbf{j}} (\text{T}_{\mathbf{e}\mathbf{j}} + \text{T}_{\mathbf{a}\mathbf{j}}) \qquad (4-46)$$

From (4-32) through (4-35)

$$\frac{\partial D_{i}}{\partial YO_{i}} = 0$$
 for $i = 16, 17, --, 30$. (4-47)

Hence, (4-40) is in decomposed form with D_i as state coordination variables. The rotational scalar state equations are given by (4-39) and (4-40) with the corresponding state coordination equations (4-32) through (4-35) and (4-45).

4.2.2 Performance Index For The Linearized Model of SCB Configuration 1 With Control Torque Applied Only To Body 1.

For:

$$TA_1 = T_{alx}$$
 $TA_2 = T_{aly}$
 $TA_3 = T_{alz}$

(4-48)

$$P = \sum_{i=1}^{6} \int_{t_{0}}^{t_{f}} p_{i} dt \qquad (4-49)$$

$$p_i = W_i * (YO_i)^2 + W_{i+6} * (TA_i)^2 \quad i = 1, 2, 3$$
 (4-50)

$$p_i = W_i^* (YO_{i+24} - YO_{i+24}^*)^2 \quad i = 4, 5, 6$$
 (4-51)

 $\mathbf{W_{i}}$ and $\mathbf{W_{i+6}}$ are scalar weighting constants to be selected

 YO_{i+24}^{*} are specified optimal values of YO_{i+24}^{*} for i = 4,5,6

4.2.3 Hamiltonian for Linearized Model of SCB Configuration
1 With Control Applied Only to Body 1

$$TE_1 = T_{elx}$$

$$TE_2 = T_{elv} \tag{4-52}$$

$$TE_3 = T_{elz}$$

$$H = \sum_{i=1}^{6} H_{i}$$
 (4-53)

$$H_{i} = W_{i}(YO_{i})^{2} + W_{i+6}(TA_{i})^{2}$$

$$+\lambda_{i}(DTS_{i}*YO_{i}+D_{i}* + \sum_{j=1}^{15} b_{i,j}T_{ej} + \sum_{j=1}^{3} b_{ij}T_{aj})$$

$$+\beta_{i}(YO_{i}-YO_{i}*) \qquad i = 1, 2, 3 \qquad (4-54)$$

$$D_{i}^{*} = \sum_{\substack{k=1\\k\neq i}}^{27} DTSC_{i,k} * YO_{k}^{*} \quad i = 1, 2, 3$$
 (4-55)

$$H_{i} = W_{i} (YO_{i+24} - YO_{i+24}^{*})^{2} + \lambda_{i} D_{i+24}^{*} i = 4, 5, 6 (4-56)$$

4.2.4 Costate Equations For Linearized Model of SCB Configuration

$$\dot{\lambda}_{i} = -\frac{\partial H}{\partial YO_{i}}$$

$$\dot{\lambda}_{i} = -\frac{\partial H}{\partial YO_{i}}$$

$$= 2W_{i}(YO_{i+24}^{*} - YO_{i+24}) \qquad i = 4, 5, 6$$

4.2.5 Control Equations For Linearized Model of SCB Configuration 1

$$(TA_i)_{r+1} = (TA_i)_r - q_i \left(\frac{\partial H}{\partial TA_i}\right)_r \qquad (4-60)$$

$$\frac{\partial H}{\partial TA_{i}} = 2W_{i+6} * TA_{i} + \sum_{j=1}^{3} b_{j,i} \lambda_{j} \quad i = 1, 2, 3 \quad (4-61)$$

 q_i = scalar weighting coefficients

r = subscript identifying iteration number

 λ_i = ith costate variable

4.2.6 Additional Necessary Conditions for Linearized System

$$\frac{\partial H}{\partial \beta_{i}} = 0$$
: $YO_{i} = YO_{i}^{*}$ $i = 1, 2, 3$ (4-62)

$$\frac{\partial \mathbf{H}}{\partial \mathbf{YO}_{\mathbf{1}}^{*}} = \sum_{\mathbf{j=1}}^{3} \lambda_{\mathbf{j}} \quad \frac{\partial \mathbf{D}_{\mathbf{j}}^{*}}{\partial \mathbf{YO}_{\mathbf{1}}^{*}} + \sum_{\mathbf{j} = 4}^{6} \lambda_{\mathbf{j}} \quad \frac{\partial \mathbf{D}_{\mathbf{j+24}}^{*}}{\partial \mathbf{YO}_{\mathbf{1}}^{*}} - \beta_{\mathbf{i}} = \mathbf{O}$$

$$\mathbf{j \neq 1}$$

$$\beta_{i} = \sum_{\substack{j=1\\j\neq i}}^{3} DTSC_{j,i} \lambda_{j} + \lambda_{i+3}$$
 $i = 1, 2, 3$ (4-63)

$$\frac{\partial H}{\partial YO_{1}^{*}} = 2W_{1}^{*}(YO_{1}^{-}YO_{1}^{*}) = 0; \quad i = 28, 29, 30 \quad (4-64)$$

4.2.7 Summary of Coordination Equations for Linearized Model

$$D_{i} = \sum_{\substack{k=1\\k\neq i}}^{27} DTSC_{i,k}*YO_{k} \qquad i = 1, 2, ---, 15 \quad (4-46)$$

$$D_i = YO_{i-6} - YO_{i-12}$$
 $i = 16, 17, ---, 21$ $(4-32)$

$$D_i = YO_{i-18} - YO_{i-21}$$
 $i = 22, 23, 24$ (4-33)

$$D_i = YO_{i-18} - YO_{i-24}$$
 $i = 25, 26, 27$ $(4-34)$

$$D_i = YO_{i-27}$$
 $i = 28, 29, 30$ (4-35)

$$\beta_{i} = \sum_{\substack{j=1 \ j \neq i}}^{3} DTSC_{j,i} \lambda_{j}^{+} \lambda_{i+3} \qquad i = 1, 2, 3$$
 (4-63)

4.2.8 Vector Representation of Variables for Linearized Model of SCB Configuration 1 With Control Applied Only to Body 1

$$\underline{y_0} = (y_0_1, y_0_2, ---, y_0_{30})^T$$

$$\underline{p} = (p_1, p_2, --- p_{30})^T$$

$$\underline{TA} = (TA_1, TA_2, TA_3)^T$$

$$\underline{TE} = (TE_1, TE_2, ---, TE_{15})^T$$

$$\underline{\lambda} = (\lambda_1, \lambda_2, ---, \lambda_6)^T$$

$$\underline{\beta} = (\beta_1, \beta_2, \beta_3)^T$$

$$\underline{y_0} = (y_0_{28}, y_0_{29}, y_0_{30})^T$$

The subproblem hierarchy for the linearized discrete mass state variable rotational model of the Space Construction Base is depicted in Figure 4-2.

4.3 APPLICATION OF MULTILEVEL CONTROL TECHNIQUES TO A HYBRID COORDINATE MODEL

An important objective implicit in the construction of a mathematical model for the rotation and flexure of · Configuration 1 of the SCB is the development of technique that may be readily extended to successively larger configurations involving greater numbers of rigid bodies. The complexity and high dimension resulting from a discrete mass modeling of Configuration 1 in Section 4.1 motivated a search for a mathematical modeling approach that would yield a model of less complexity and smaller dimension. Linearization of the discrete mass model attained a reduction of complexity but not a reduction of dimension of the model. Hybrid coordinate modeling, an approach developed by Likins (4-7), was seen to offer promise of both linearization and reduction of dimension of the resulting model. To evaluate the efficacy of this approach a single axis torsional space vehicle was modeled in terms of hybrid coordinates and subjected to multilevel control techniques. The results of this particular study were published in a paper by Chichester, Kaczynski and Nachmias (4-8).

4.3.1 Discrete Rigid Body Model of a Spacecraft

The vehicle to be controlled is shown in Figure 4-1. It consists of a central body with appendages such as solar panels along each direction of the Z axis. Because of

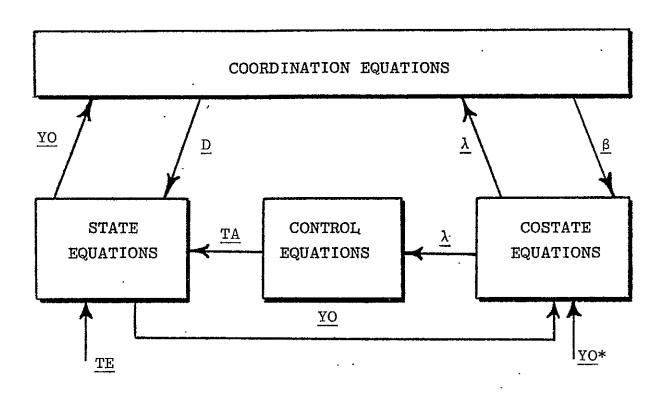


FIGURE 4-2
SUBPROBLEM HIERARCHY FOR LINEARIZED
SPACE CONSTRUCTION BASE
ROTATIONAL MODEL WITH MULTILEVEL CONTROL

symmetry, the five bodies of Figure 1 may be represented by three masses, following Porcelli (4-9) as depicted in Figure 4-3. The equations of motion for the vehicle are the following:

$$J_{0}^{\theta_{0}} = -K_{1}(\theta_{0} - \theta_{1}) + T_{0}$$

$$J_{1}^{\theta_{1}} = K_{1}(\theta_{0} - \theta_{1}) - K_{2}(\theta_{1} - \theta_{2})$$

$$J_{2}^{\theta_{2}} = K_{2}(\theta_{1} - \theta_{2})$$

$$(4-67)$$

where: θ_i = angular rotation of the ith body relative to an inertial frame of reference T_i = disturbance or control torque on ith body J_i = moment of inertia of ith body about the Z-axis K_i = torsional spring constant for spring between bodies i-l and i

4.3.2 Hybrid Coordinate Model

The standard form of the hybrid coordinate model of the vehicle described in (4-67) may be written as follows:

$$J_{t}^{\ddot{\theta}} \sigma^{-\delta} \underline{\dot{\eta}} = T_{0}$$

$$\underline{\dot{\eta}} + \left[2\zeta\sigma\right] \underline{\dot{\eta}} + \left[\sigma^{2}\right] \underline{\dot{\eta}} - \delta\theta_{0} = 0 \qquad (4-68)$$

where: $\zeta = \text{structural damping (same for all modes)}$

 $[2\zeta\sigma] = 2\zeta \ [\sigma]$, where $[\sigma]$ is a diagonal matrix of modal frequencies.

 $\eta = \phi^{-1}q = \text{vector of modal coordinates}.$

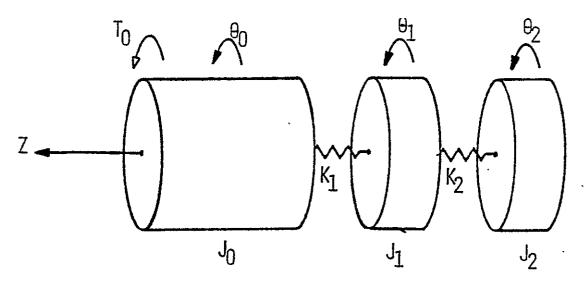


FIGURE 4-3 TORSIONAL MODEL OF THE VEHICLE

$$\underline{\mathbf{q}} = \begin{bmatrix} \mathbf{q}_1 \mathbf{q}_2 \end{bmatrix}^{\mathrm{T}} \tag{4-69}$$

$$q_{i} = \theta_{i} - \theta_{0} \tag{4-70}$$

$$\phi^{T}[K]\phi = [\sigma^{2}]$$

$$[\sigma^{2}] = [\sigma_{1}^{2} \quad O_{0}^{2}]$$

$$\begin{bmatrix} \mathbf{J} \end{bmatrix} = \begin{bmatrix} \mathbf{J}_1 & \mathbf{0} \\ \mathbf{0} & \mathbf{J}_2 \end{bmatrix}; \begin{bmatrix} \mathbf{K} \end{bmatrix} = \begin{bmatrix} (\mathbf{K}_1 + \mathbf{K}_2) & -\mathbf{K}_2 \\ -\mathbf{K}_2 & \mathbf{K}_2 \end{bmatrix}$$

$$\delta = -\phi^{\mathrm{T}} \left[J \right] \begin{bmatrix} 1 \\ 1 \end{bmatrix} = -\phi^{\mathrm{T}} \left[\begin{bmatrix} J \\ J^{\mathrm{I}} \\ 2 \end{bmatrix} \right]$$

 $J_{t} = J_{0} + J_{1} + J_{2} = \text{total vehicle moment of inertia}$

4.3.3 Decomposed Hybrid Coordinate Model

Expansion of equation set (4-68) into its scalar components, the substitutions $X_1=0$ 0, $X_2=0$ 0, $X_3=\eta_1$, $X_4=\eta_1$, $X_5=\eta_2$, $X_6=\eta_2$ and the simultaneous solution of the resulting equations for X_i , i=1,2,---,6, generate a coupled state variable hybrid coordinate model of the vehicle to be controlled. State coordination equations that temporarily suppress coupling between the scalar equations of the state variable model may be written in the following form.

$$C_i = g_i(X_c); i=1,2...,6*$$
 (4-71)

where:
$$X_c = [X_1, ..., X_{i-1}, X_{i,1}, ..., X_6]^T$$
 (4-72)

The resulting scalar equations of the decomposed (decoupled) state variable hybrid coordinate model are the following:

$$X_{i} = f_{i}(X_{i}) + u_{i}(T_{0}) + C_{i}$$
 (4-73)

where:
$$X_{i}(t_{0}) = X_{i0}$$
 (4-74)

When the mathematical model of the vehicle to be controlled is decomposed into subsystems, the corresponding decomposed performance index may be written in the form of a summation of terms each of which corresponds to one of the subsystems of the decomposed model. The decomposed Hamiltonian resulting from such a performance index also may be written in summation form. For the flexible vehicle treated here the decomposed Hamiltonian may be written as follows:

$$H = \sum_{i=1}^{6} H_{i}$$
 (4-75)

where:
$$H_{i} = p_{i} + \lambda_{i} (f_{i} + u_{1} + C_{i}) + \rho_{i} (g_{i} - C_{i})$$
 (4-76)

*This range for the subscript, i, will apply in the sequel unless a specific exception is stated.

$$p_{i} = W_{i,1}(X_{i}-X_{isp})^{2}+W_{i,2}u_{i}^{2}$$
 (4-77)

W_{i,j} = constant weighting coefficients

 λ_i = costate variable for subsystem i

 ρ_i = Lagrange multiplier for the coordination constraint, equation (4-71).

4.3.5 Costate and Costate Coordination Equations

Necessary conditions for effecting optimal control are
stated in terms of partial derivatives of the Hamiltonian.

Two such conditions for the flexible vehicle treated
in this section may be stated as follows:

$$\lambda_{i} = \frac{-\partial H}{\partial X_{i}} \tag{4-78}$$

$$\frac{\partial H}{\partial C_{i}} = 0 \qquad (4-79)$$

The first of these conditions generates the following costate equations.

$$\lambda_{i} = -\frac{\partial p_{i}}{\partial X_{i}} - \frac{\partial f_{i}}{\partial X_{i}} \lambda_{i} - \sum_{\substack{j=1 \ j \neq i}}^{6} \frac{\partial g_{j}}{\partial X_{i}} \rho_{j}$$

$$(4-80)$$

where:
$$\lambda_i(t_f) = 0$$
 (4-81)

The second generates the costate coordination equations which follow:

$$\rho_{i} = \lambda_{i} \tag{4-82}$$

4.3.6 The Control Algorithm

The iterative relationship for successive values of the control torque may be expressed as follows:

$$\left(T_0 \right)_{r+1} = \left(T_0 \right)_r - q \left(\frac{\partial H}{\partial T_0} \right)_r$$
 (4-83)

where r is the iteration index and q is a constant to be chosen on the basis of the rate of approach of the performance of the controlled vehicle to optimality. From (4-73), (4-76) and (4-77) it may be seen that the partial derivative in (4-83) is a function of λ_i .

- 4.3.7 Construction of the Subproblem Hierarchy
 The state equations, (4-73) and also (4-74) may be
 regarded as comprising a state subproblem. Similarly,
 the costate equations (4-80) and (4-81) may be assembled
 into a costate subproblem, and the control equations (4-83)
 may be associated in a control subproblem. The state
 coordination equations (4-71) and the costate coordination
 equations (4-82) may be combined into an overall coordination subproblem. Then a hierarchy of these subproblems
 can be assembled as depicted in Figure 4-4.
- 4.4 CONCLUSIONS AND RECOMMENDATIONS

 From the work reported in Subsections 4.1 through 4.3, the following conclusions may be drawn:
 - 1) The three dimensional five body discrete mass rotational model for Configuration 1 of the SCB has been transformed in such a way that it may readily be simulated on a digital computer. The resulting

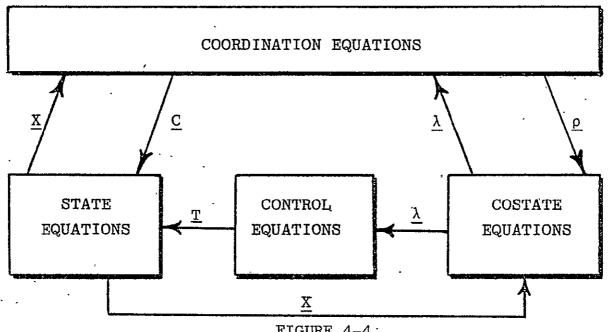


FIGURE 4-4
SUBPROBLEM HIERARCHY FOR
MULTILEVEL CONTROL

model is in scalar state variable form.

- 2) Multilevel control techniques have been applied to the scalar state variable form of the three dimensional discrete mass model for Configuration 1. The resulting hierarchy of subproblems to be solved may be easily simulated on a digital computer.
- 3) The multilevel hierarchical rotational form of the three dimensional discrete mass model for Configuration 1 of the SCB is nonlinear and of relatively high dimension. (30 scalar state variables) The remaining 11 Configurations would require discrete mass rotational models of still higher dimension. (Up to 120 state variables)
- 4) The nonlinear discrete mass rotational models of Configuration 1 of the SCB have been linearized using the assumption of small angular displacements.
- 5) Hybrid coordinate modeling appears to yield models that are lower in dimension than the corresponding models generated by the discrete mass approach. Hybrid coordinate models also tend to be linear in most instances. Both of these factors render the model more amenable to the application of multilevel control techniques.
- 6) In extending the combined application of hybrid coordinate modeling and multilevel control techniques from models of low dimension to models of higher

dimension, some of the modal coordinates of the hybrid model should be truncated.

The following recommendations are offered for further work in the application of multilevel control to flexible space vehicles and the computer simulation of the resulting mathematical models.

- 1) Simulation of the linearized scalar state variable form of the three dimensional discrete mass rotational model of Configuration 1 of the SCB should be completed.
- 2) A three dimensional hybrid coordinate rotational model of Configuration 1 of the SCB with multilevel control should be developed for digital computer simulation.
- 3) Candidate control techniques other than multilevel control should be applied to either of the three dimensional rotational model simulations listed above for purposes of comparison.
- 4) Since most of the candidate control techniques presently contemplated require access to all of the state variables, techniques for generation of observers required to sythesize inaccessible state variables should be developed.
- 5) Modeling, control and simulation techniques developed for Configuration 1 rotational models of the SCB

should be extended to other Configurations involving more masses.

4.5 REFERENCES

- (4-1) Chichester, F. D., "Application of Multilevel Control Techniques to Space Construction Base,"

 Section 7 of Space Construction Base Control

 System Final Report, NASA Contract No. NAS8-32660,
 The Bendix Corporation, Guidance Systems Division,
 October 27, 1978.
- (4-2) Cornell, G. A., "Space Base Mathematical Model,"
 Bendix Research Laboratories Internal Memorandum,"
 December 14, 1977.
- (4-3) Lipski, D. B., "Discrete Coordinate Approach to Analytic Modeling of Flexible Bodies," Bendix Research Laboratories Internal Memorandum, February 22, 1979.
- (4-4) Lipski, D. B., "Linearized Five Body Space Base Simulation Model," Bendix Research Laboratories Internal Memorandum, April 23, 1979.
- (4-5) Chichester, F. D., "Multilevel Modeling of the Space Construction Base," Proc. of the Tenth

 Annual Pittsburgh Conference on Modeling and

 Simulation, The University of Pittsburgh, Pittsburgh, Pennsylvania, April, 1979.

- (4-6) Chichester, F. D., "Application of Multilevel Control to a Single Axis Torsional System,"

 Bendix Corporation MT-40,808, Issue A, May 16, 1978.
- (4-7) Likins, P., "Dynamics and Control of Flexible Space Vechicles," Jet Propulsion Laboratory, Technical Report 32-1329 Revision 1, January 15, 1970.
- (4-8) Chichester, F. D., R. F. Kaczynski and S. Nachmias
 "Application of Hybrid Coordinate Modeling and
 Multilevel Control Techniques to a Single Axis
 Torsional Model," Proc. of the Tenth Annual
 Pittsburgh Conference on Modeling and Simulation,
 The University of Pittsburgh, Pittsburgh, Pennsylvania,
 April, 1979.
- (4-9) Porcelli, G., "Attitude Control of Flexible Space Vehicles," AIAA Journal, Vol. 10, No. 6, June, 1972, pp. 807-812.

SECTION 5

5.0 SIMULATION OF LQR CONTROL

The linear quadratic regulator (LQR) approach is applied to single axis control of Configuration 1 of the Space Construction Base (SCB). A single axis vehicle model is defined and converted to the state variable form for application of the LQR technique. A control performance index is then defined and weighting factors are selected. A matrix Riccati equation for the system is then solved as a function of time. This result is used to specify the optimal feedback gain coefficients. These feedback gains were used in a simulation of the vehicle control system, and the time responses are presented. A description of an alternate application of LQR is then discussed.

5.1 VEHICLE EQUATIONS

Configuration 1 of the SCB (References 5-1 and 5-2) is shown in Figure 5-1. The vehicle XYZ axes are parallel to the principal axes of inertia. The vehicle is represented here by discrete masses with three-axis hinge springs between adjacent masses. The vehicle is divided into five masses: one central body between the solar wings, and each solar wing is divided into two equal masses. of the symmetry and the absence of product of inertia terms, the SCB can be represented as a three-mass rotational model as shown in Figure 5-2. Body 1 is the central body; both inboard solar wing sections are represented as body 2 and both outboard sections as body 3. Module and solar wing dimensions and the inertia properties were obtained from Reference 5-1. Center of mass locations are given in Figure 5-2 relative to the reference origin for the XYZ coordinates. $\boldsymbol{\bar{x}}_1$ is the center of mass (CM) location

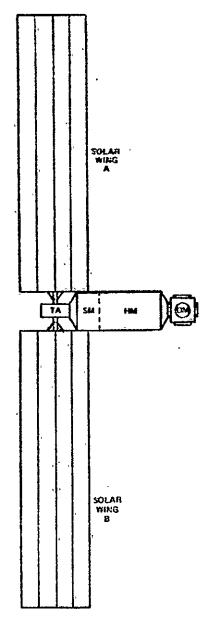


FIGURE 5-1
SPACE CONSTRUCTION BASE-CONFIGURATION 1

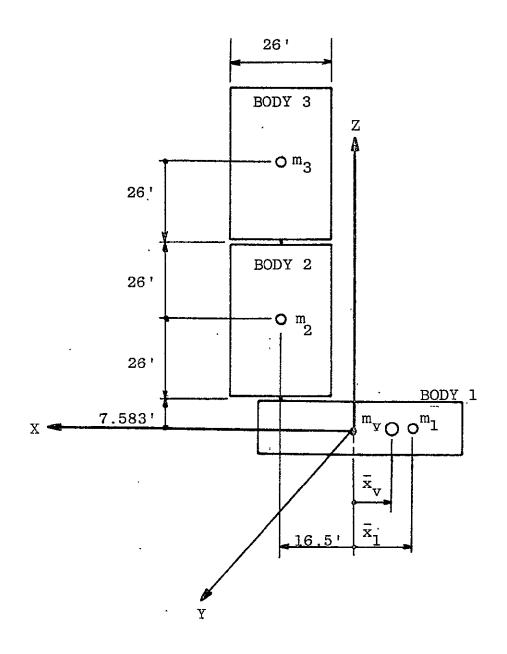


FIGURE 5-2
INERTIA MODEL FOR CONFIGURATION 1

of body 1 along the X axis and \bar{x}_{V} is the CM of the total vehicle.

With the vehicle modeling limited to the Z axis, the inertia characteristics of the central body (No. 1) are listed in Table 5-1. Key outputs of the table are the CM location and the Z axis moment of inertia about the CM for body 1. It is convenient to represent the single axis vehicle as the torsional model (as in Reference 5-3) of Figure 5-3, where the masses are connected by hinge springs K_1 and K_2 . For the Z axis,

$$J_1 = I_1 + \frac{m_1}{m} (m_2 + m_3) R_{12}^2$$
 (5-1)

where J_1 = effective MOI of body 1

I₁ = MOI of body 1 about it's CM

 m_{i} = mass of the i-th body

$$m = m_1 + m_2 + m_3$$

R₁₂ = distance from the CM of body 1 to the contact
 point with body 2 (the X axis component only in
 this case)

The MOI of bodies 2 and 3 are obtained by assuming that each solar wing section is a rectangular plane. The MOI about the Z axis of each is then

TABLE 5-1
INERTIA CHARACTERISTICS OF BODY 1

•
$$\bar{x}_1 = \Sigma W_i x_i / \Sigma W_i = -88.74'' = -7.40'$$

MODULE	WEIGHT (LBS)	POSITION (IN)			RAD. OF GYRATION (IN)	POSITION WRT CM	MOMENT OF INERTIA WRT CM (SLUG-FT ²)
	W	х	У	Z	Kz	x -x̄1	^I 1
SM	16,440.	66	oʻ	0	57.8	+154.7	96,757.6
HM	16,487.	-156.	0	0	100.	-67.3	51,693.7
TA	650.	198.	0	0	43.5	+286.7	11, 7 95.2
DM	5,625.	-377.	0	0	55.1	-288.3	104,578.9
TOTAL	39,202						264,825.

SM - Subsystems Module

HM - Habitability Module

$$I_1 = \frac{w}{g} \left[K_z^2 + (x - \bar{x}_1)^2 \right]$$

TA - Turret Assembly

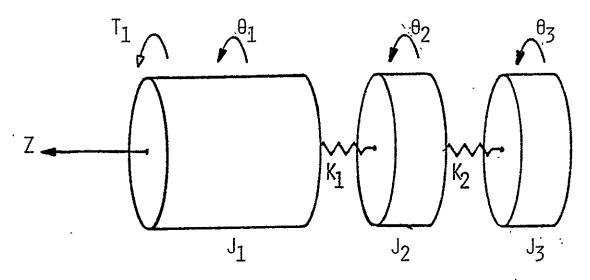


FIGURE 5-3 TORSIONAL MODEL OF THE VEHICLE

$$I_2 = I_3 = (26)^2 \ 26.445/12 = 1490 \ \text{slug-ft}^2 \ \text{and}$$
 $J_2 = I_2 \ \text{and} \ J_3 = I_3.$

Note that the mass of each section is doubled since it represents <u>both</u> inboard or <u>both</u> outboard portions of the solar wings.

The equations of motion for the torsional model (Reference 5-4) are then defined as

$$J_{\theta}^{\bullet}$$
 = sum of constraint and disturbance torques (5-2)

where
$$J = \begin{bmatrix} J_1 & 0 & 0 \\ 0 & J_2 & 0 \\ 0 & 0 & J_3 \end{bmatrix}$$
 (5-3)

$$\frac{\mathbf{\ddot{\theta}}}{\mathbf{\ddot{\theta}}} = \begin{bmatrix} \mathbf{\ddot{\theta}}_1 & \mathbf{\ddot{\theta}}_2 & \mathbf{\ddot{\theta}}_3 \end{bmatrix} \mathbf{T} \tag{5-4}$$

Springs K_1 and K_2 and dampers D_1 and D_2 cause constraining torques, while the disturbance is limited to a control torque vector \underline{u} with a component on each body. The equation in matrix form is then

$$J\underline{\theta} = D\underline{\theta} + K\underline{\theta} + \underline{u}$$
 (5-5)

where
$$K_{\cdot} = \begin{bmatrix} -K_1 & K_2 & 0 \\ K_1 & -(K_1 + K_2) & K_2 \\ 0 & K_2 & -K_2 \end{bmatrix}$$
 (5-6)

$$D = \begin{bmatrix} -D_1 & D_2 & 0 \\ D_1 & -(D_1 + D_2) & D_2 \\ 0 & D_2 & -D_2 \end{bmatrix}$$
 (5-7)

$$\underline{\mathbf{u}} = \begin{bmatrix} \mathbf{u}_1 & \mathbf{u}_2 & \mathbf{u}_3 \end{bmatrix}^{\mathrm{T}} \tag{5-8}$$

and the $\frac{\theta}{2}$ and $\frac{\dot{\theta}}{2}$ vector are defined in a manner similar to $\frac{\ddot{\theta}}{2}$. K_2 is selected to obtain a l rad/sec resonance with J_2 ,

$$K_2 = J_2 W^2 \tag{5-9}$$

 $\rm K_1$ is selected to be equal to $\rm K_2$. $\rm D_2$ is set to obtain a damping factor of 0.005 with $\rm K_2$ and $\rm J_2$ and $\rm D_1$ is set equal to $\rm D_2$. All numerical values are summarized in Table 5-2. Each matrix formed by these parameters is printed out on Figure 5-4.

To place the model in state variable form, both sides of the equation are premultiplied by J^{-1}

$$\frac{\dot{\theta}}{\dot{\theta}} = J^{-1}D\underline{\dot{\theta}} + J^{-1}\underline{K}\underline{\theta} + J^{-1}\underline{u} \qquad (5-10)$$

This can be redefined as follows, while also setting $u_2 = u_3 = 0$:

$$\underline{\underline{\theta}} = A_{\underline{D}}\underline{\underline{\theta}} + A_{\underline{K}}\underline{\underline{\theta}} + B\underline{\underline{u}}$$
 (5-11)

Matrices J^{-1} , A_{K} , A_{D} and the transpose of B are printed out in Figure 5-5.

TABLE 5-2 SUMMARY OF PHYSICAL CONSTANTS

- Z AXIS OF CONFIGURATION 1
- $R_{12} = (16.50 + 7.40)FT. = 23.9 FT ALONG X AXIS$

	MASS	M.O.I. ABOUT EACH C.M.	EFFECTIVE M.O.I.	SPRING CONSTANT	DAMPING CONSTANT
	M _i	i	^J i	K.	D _i
i	(slugs)	(slug-ft) ²	$({ m slug-ft})^2$	(ft-lb/rad)	(ft-lb-sec)
1	1218.21.	264,825.	293,767.	1490.	14.9
2	26.445	1490.	1490.	1490.	14.9
3	26.445	1490.	1490.	- <u>-</u> -	

$$J_{1} = I_{1} + \frac{m_{1}}{m} (m_{2} + m_{3}) R_{12}^{2}$$

$$m = m_{1} + m_{2} + m_{3}$$

 ${
m R}_{
m 12}={
m DISTANCE}$ IN BODY 1 FROM IT'S CM TO POINT OF CONTACT WITH BODY 2

DAMPING SELECTED TO GIVE A DAMPING FACTOR OF 0.005.

	J⊨	0,29377D	06	0.0		0.0	•
•	1 .	0.0		0.14900D	04	0.0	
		0.0		0,0		0,14900D	04
		ц					
	K=	-0.14900D	04	0.14900D	04	0.0	
		0.14900D		-0.29800D	04	0.14900D	04
		0,0		0,14900D	04	+0,14900D	04
	D=	-0.14900D	02	0.14900D	02	0.0	
		0.14900D				0.14900D	02
		0.0		0.14900D		=0.14900D	

FIGURE 5-4 MATRIX PARAMETERS FOR DISCRETE INERTIA, SPRING AND DAMPING CONSTANTS

J INVERSE#	0.34041D=05	0.0	0.0
	0.0	0.67114D=03	0 0
	0.0	0.0	0.67114D=03
			<u></u>
AK=	-0.50720D-02	0,507200+02	0.0
	0.10000D 01	=0.20000D 01	
	0.0	0.10000D 01	-0.10000D 01
. AD=	-0.50720D=04	0,50720D=04	0.0 .
	0.10000D=01	-0.20000D=01	0.100000=01
	0.0	0.10000D#01	=0.10000D=01
	,		•
BT≖	0.340410-05	0.0	0.0

FIGURE 5-5 THE INVERSE OF INERTIA MATRIX, \boldsymbol{A}_{K} , \boldsymbol{A}_{D} AND \boldsymbol{B}^{T}

The system can be redefined as

$$\dot{x} = Ax + Bu \tag{5-12}$$

where
$$x = \begin{bmatrix} \theta_1 & \dot{\theta}_1 & \theta_2 & \dot{\theta}_2 & \theta_3 & \dot{\theta}_3 \end{bmatrix}^T$$
 (5-13)

and $u = u_1$

Then A is a recasting of \mathbf{A}_{K} and \mathbf{A}_{D} as follows:

$$A = \begin{bmatrix} 0 & 0 & 1 & 0 & 0 & 0 & 0 \\ -0.5072E - 2 & -0.5072E - 4 & 0.5072E - 2 & 0.5072E - 4 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 1 & 0.01 & -2 & 0.02 & 1 & 0.01 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0.01 & -1 & -0.01 \end{bmatrix}$$
(5-14)

And the dimension of B is increased to six:

$$B^{T} = \begin{bmatrix} 0 & .34041E-5 & 0 & 0 & 0 & 0 \end{bmatrix} (5-15)$$

5.2 OPTIMUM FEEDBACK GAIN

The linear optimum feedback control gain can be determined by setting a performance index (References 5-5, 5-6 and 5-7) as follows:

$$PI = \int_{0}^{\infty} (x^{T}Qx + u^{T}Ru) dt \qquad (5-16)$$

where Q, R = weighting factor matrices.

The diagonal of Q is selected to indicate the relative importance of each element of x. In this case,

where q is selected as $W_{BW}^4 = (0.1)^4 = 10^{-4}$, and W_{BW}^4 is the control loop bandwidth.R is a 1 by 1, where $r = (J_1)^{-2}$

Once the model is placed in the state variable form
$$\dot{x} = Ax + Bu$$
 (5-18)

the matrix Riccati equation which follows was solved until $\dot{P} = 0$:

$$\dot{P} = PA + A^{T}P - PBR^{-1}B^{T}P + Q$$
 (5-19)

The LQR feedback matrix for these conditions is defined as

$$F = -R^{-1} B^{T} \overline{P} = -[F_{1} F_{2} F_{3} F_{4} F_{5} F_{6}]$$
 (5-20)

where \overline{P} is the steady state solution of (5-19).

A block diagram of the system is given in Figure 5-6. The input constants (Q, A, B, R) used in the solution

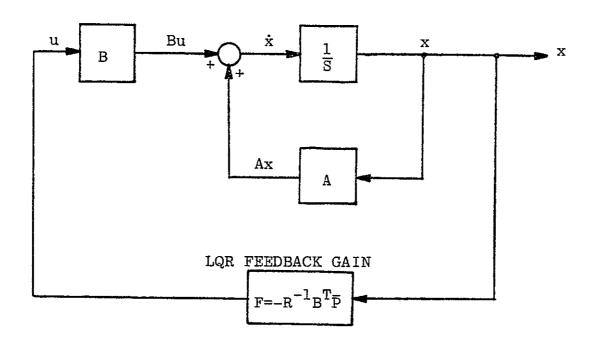


FIGURE 5-6
BLOCK DIAGRAM OF LQR-CONTROLLED SYSTEM

of the Riccati equation are given in Figure 5-7, along with the initial conditions which were used. Note that q and r were normalized with q = 1 and $r = (J_1^2 W_{BW}^4)^{-1}$. The final values of the solution, when $t \approx 200$ seconds, are shown in Figure 5-8. F is also printed out and the time solution provided the following component gains of F:

$$F_1 = 2906.$$
 $F_2 = 41320.$
 $F_3 = 15.0$
 $F_4 = 209.3$
 $F_5 = 15.1$
 $F_6 = 209.1$
(5-20)

It is interesting to note that:

$$F_1/J_1 \cong W_{BW}^2 = (0.1 \text{ rad/sec})^2$$

$$F_2/J_1 \cong 2\zeta W_{BW} = 2 (.707) (0.1)$$

Thus if the appendages were ignored, the same attitude and attitude rate gains would be obtained for central body feedback if a standard non-optimal servo technique was applied.

5.3 SIMULATION

The system was simulated on the digital computer using the full LQR feedback matrix for an initial attitude error of

BOLUTION	OF MATRI	X RICCA	TI EQUATION, 8	ca config 1, Z	AXI8				
CONSTANT DATA INPUT									
		90	0.10000D 01 0.0 0.0 0.0 0.0 0.0	0 4 0 0 4 0 0 4 0 0 4 0 0 4 0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	
٠		AB	0.0 +0.50720D+02 0.0 0.10000D 61 0.0	0.10000D 01 =0.50720D=04 0.0 0.10000D=01 0.0 0.0	0.0 0.50720D=02. 0.0 =0.20000D 01 0.0 0.10000D 01	0.0 0.50720D=04 0.10000D 01 =0.20000D=01 0.0 0.1000D=01	0.0 - 0.0 0.0 0.10000D 01 0.0 -0.10000D 01	0.0 0.0 0.0 0.10000D=01 0.10000D=01	
		30	0.0	0,340410+05	0.0	0.0	0,0	0.0	
		RĐ	0,11600D-06						
Tà	0.0 SEC	78	0.0	0.0	0.0	0.0	0 . 0,	0.0	
1786	1	7.	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 - 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0	
		PODTÉ	0.10000D 01 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0 0.0 0.0 0.0 0.0 0.0	

FIGURE 5-7 SYSTEM MATRICES A AND B, WEIGHTING FACTORS Q AND R, AND INITIAL CONDITIONS FOR SOLUTION OF THE MATRIX RICCATI EQUATION.

T# 8	200,0 SEC	fe	0,290600 04	0,413200 05	0,149960 02	0,209290 03	0,151200 02	0,209120 03
ITOW	24"	Pű	0.13438D 02 0.49024D 02 0.46313D=01 0.49206D 00 0.46380D=01 0.486940 00	0.99026D 02 0.14080D 04 0.51100D 00 0.71319D 01 0.51523D 00 0.71260D 01	0,68113D=01 0,511000 00 0,130320-02 0,255800-02 0,18129D=02 0,25369D=02	0.492060 00 0.713190 01 0.255800=02 0.385660=01 0.259440=02 0.800160=01	0.66580D=01 0.515230 00 0.181290=02 0.259440=02 0.277870=02 0.25806D=02	0.486940 00 0.712500 01 0.2530690-02 0.400160-01 0.458060-02 0.424360-01
		PDOTé	0.64494D=06 -0.18513D=04 0.45574D=06 0.75309D=05 -0.10095D=05 0.11843D=04	-0,18513D-05 0,86911D-04 0,64653D-05 -0,37108D-05 0,11246D-04 -0,59127D-04	0.45576D=06 0.646530=05 =0.42156D=06 =0.25362D=05 =0.48346D=07 =0.39768D=05	0.75309D=05 =0.37108D=04 =0.25362D=05 0.15801D=04 =0.46611D=05 0.25161D=04	#0.10095D=05 0.11246D=04 #0.48346D=07 =0.48611D=05 0.98620D=06 #0.73383D=05	0,11843D=04 =0,591270=04 =0,39768D=05 0,25151D=04 =0,73353D=05 0,40056D=04

FIGURE 5-8 "FINAL" CONDITIONS OF MATRIX RICCATI EQUATION SOLUTION AT TIME = 200 SECONDS

ORIGINAL PAGE IS OF POOR QUALITY

$$\underline{\theta}(0) = \begin{bmatrix} 1 & \text{degree} \\ 0 \\ 0 \end{bmatrix}$$
 (5-22)

The θ_1 , u, η_2 and η_3 variables are shown on print-plots of Figure 5-9 and 5-10, where:

$$η_2$$
 = relative motion of inboard appendage = $θ_2 - θ_1$
 $η_3$ = relative motion of outboard appendage = $θ_3 - θ_1$ (5-23)

Since the central actuator is located at body 1, the θ_1 transient is well behaved. η_2 and η_3 , however, oscillate at about 0.1 Hz and appear to be lightly damped. The control u also appears as a smooth transient — even though it is also dependent upon oscillatory states from bodies 2 and 3. All six states have been applied to minimize the performance index based upon the weighted integration of θ_1 and u.

To examine this further, the simulation was repeated with $F_3 = F_4 = F_5 = F_6 = 0$, since these gains were already very low in the optimal case. The result of this "partial LQR" feedback was basically the same as that obtained previously for $\theta_{\bar{1}}$, η_2 and η_3 (Figures 5-9 and 5-10). But the control torque u had a 0.1 Hz oscillatory component superimposed on the basic response obtained in Figure 5-9. These results are shown in Figures 5-11 and 5-12. Obviously, the performance index here is not minimal since the integral of the u^TRu term would approach infinity.

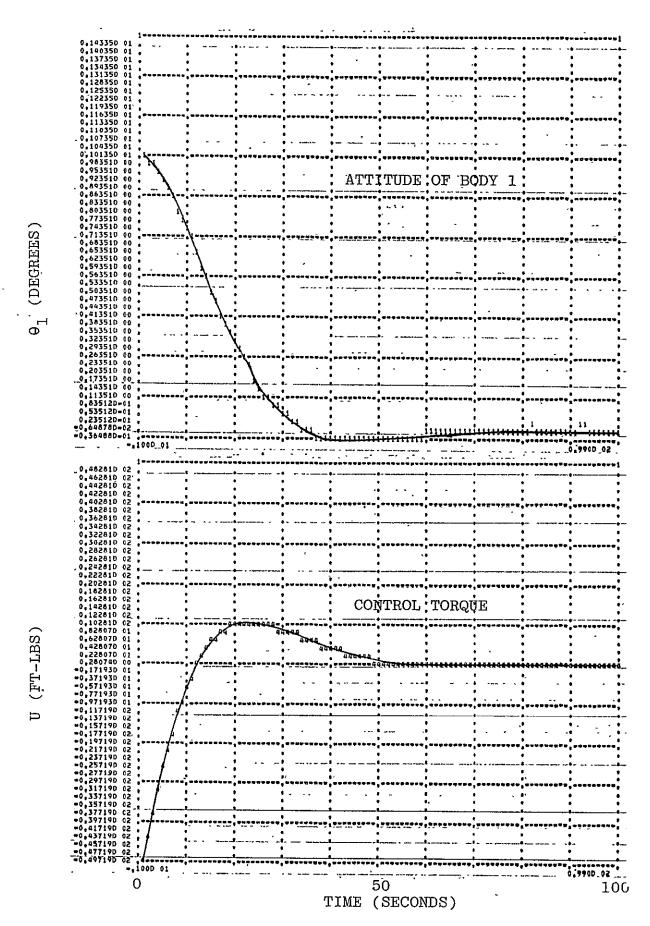


FIGURE 5-9 FULL STATE LQR FEEDBACK, CENTRAL BODY ATTITUDE AND CONTROL TORQUE INITIAL CONDITION: $\theta_1(0) = 1$ DEGREE

5-17

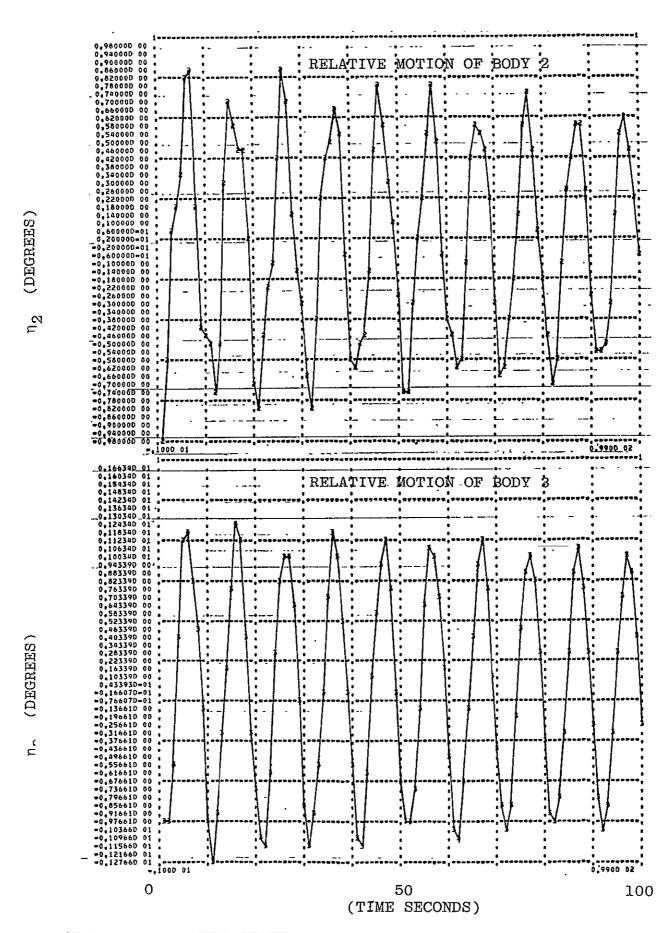


FIGURE 5-10 FULL STATE LQR FEEDBACK, RELATIVE MOTION OF INBOARD AND OUTBOARD APPENDAGES.

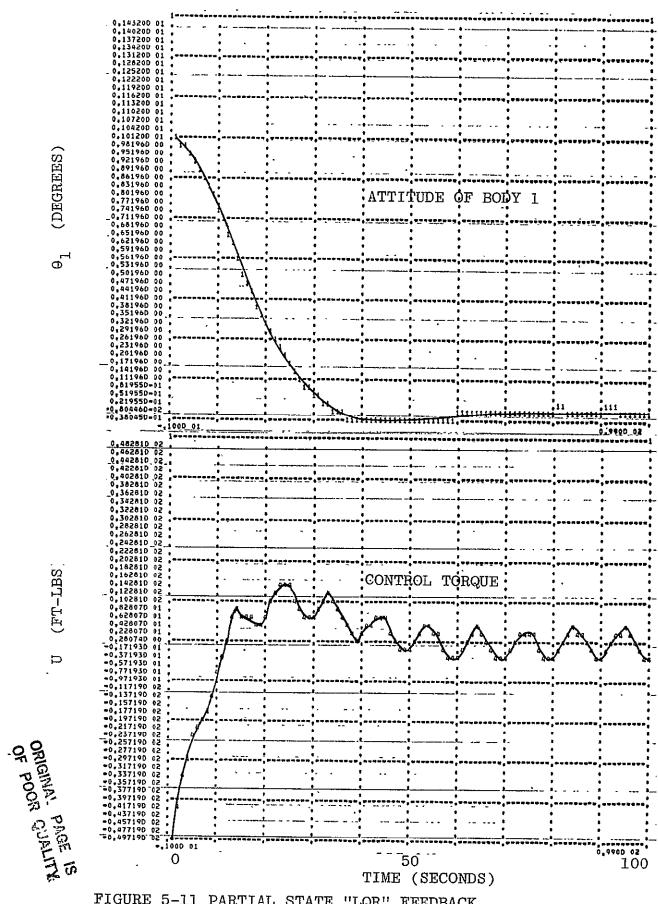


FIGURE 5-11 PARTIAL STATE "LQR" FEEDBACK CENTRAL BODY ATTITUDE AND CONTROL TORQUE INITIAL CONDITION: $\Theta_7(0) = 1$ DEGREE

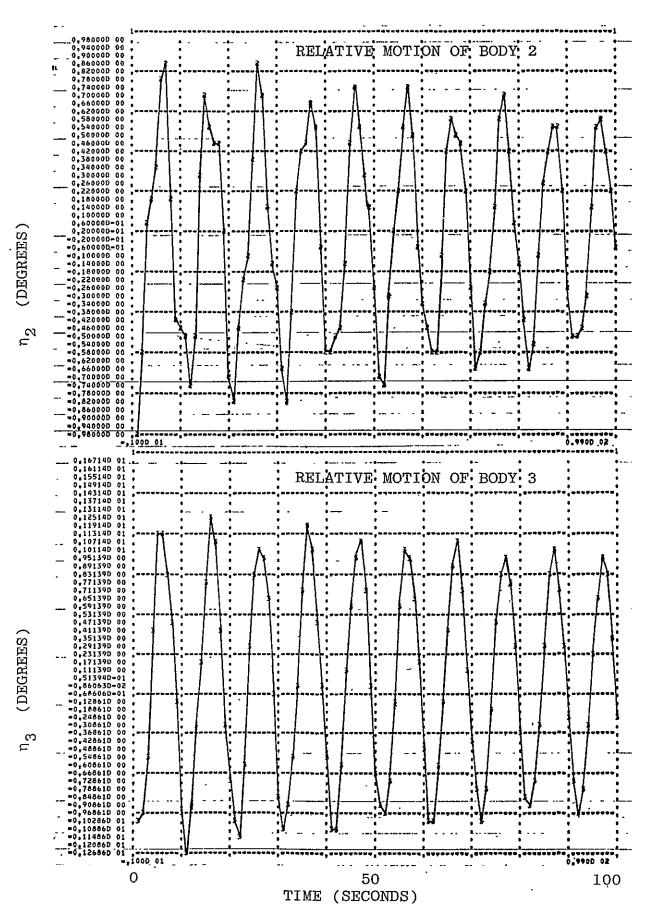


FIGURE 5-12 PARTIAL STATE "LQR" FEEDBACK
RELATIVE MOTION OF INBOARD AND OUTBOARD
APPENDAGES

5.4 DISCUSSION

In the previous sub-sections the LQR control technique described is a straight forward approach which is relatively easy to apply once a system is described in the state variable form. Some skill is involved in the selection of weighting factors (Q and R) for the performance index, otherwise the technique is relatively simple for linear, non-stochastic systems.

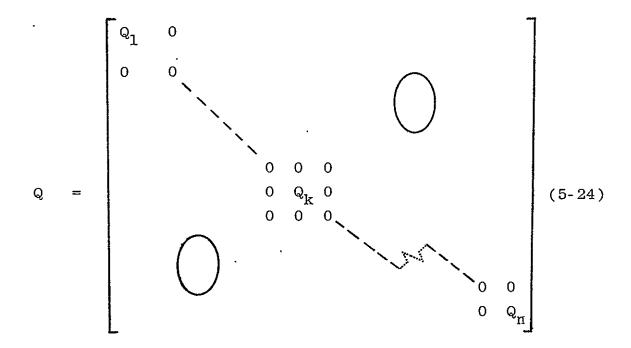
For the discrete mass and spring model defined here, only the full state variable feedback obtained completely satisfactory results. When solar wing appendage motion gains were reduced to zero, a lightly damped oscillation was obtained for the control torque u₁ — although the response of the other variables appeared to be unchanged. This raises the question as to how the system would react for a multi-dimensional finite element representation for the solar wings. Feeding back hundreds of signals to a single actuator set seems to be impractical. Representing flexible modes of the solar wings by hybrid coordinates (Reference 5-8) would be a more reasonable approach, where truncation of high frequency or low mass solar wing modes may be accomplished in a selective manner.

The LQR control approach could be expanded in several different directions:

a. More elements or dimensions as discussed above by modeling appendages from finite element data, which may then be represented in hybrid coordinates (Reference 5-9).

- b. Three axis vehicle models including cross coupling terms.
- c. Including feedback sensor (and possibly actuator)
 noise sources and generating a feedback filter to
 generate a better estimate of x, usually referred to
 as the linear quadratic Gaussian (LQR) approach.
- d. Attitude stabilize two or more locations on a large flexible spacecraft.

The application of LQR to d. can be demonstrated by a single axis representation of a long flexible vehicle as in Figure 5-13. If an intermediate mass and angle are represented as J_k and θ_k , respectively, locations I, k and n on the vehicle can be stabilized by selecting the relative magnitudes of weighting factors in \mathbf{Q}_1 , \mathbf{Q}_k and \mathbf{Q}_n :



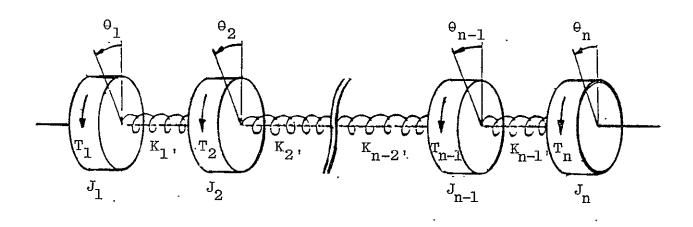


FIGURE 5-13 SINGLE AXIS N-DIMENSIONAL REPRESENTATION OF A LARGE FLEXIBLE VEHICLE

where
$$Q_i = \begin{bmatrix} q_{2i-1} & 0 \\ 0 & 0 \end{bmatrix}$$
 (5-25)

for i = 1, k, n.

The relative magnitudes of q_1 , q_{2k-1} and q_{2n-1} may be selected according to the pointing performance requirements of θ_1 θ_k and θ_n . If a pointing stability or "jitter" requirement is specified, at say location m, θ_m can be reduced by a high weighting of q_{2m} relative to q_{2m-1} and others.

5.5 REFERENCES

- 5-1 Space Construction Base Buildup Summary, Data Package Attachment to Exhibit A Scope of Work, Request for Quotation 1-7-ED-07552-AP131D, Marshall Space Flight Center, 10 March 1977.
- 5-2 Jennings, J., Definition of Space Base Buildup, Bendix Corporation MT-40,801, 21 October 1977.
- 5-3 Porcelli, G., Attitude Control of Flexible Space Vehicles, AIAA Journal Volume 10, No. 6, June, 1972, PP. 807-812.
- 5-4 Nachmias, S., The Application Of The Hybrid Coordinates Formulation To A Simple Torsional Model, Bendix Corporation MT-40,814, Dec. 12, 1978.

- 5-5 Melsa, J. L., and Schultz, D. G., State Functions and Linear Control Systems, 1967, Mc Graw-Hill.
- 5-6 Kwakernaak, H. and Sivan, R., Linear Optimal Control Systems, 1972, Wiley-Interscience.
- 5-7 Nachmias, S., The Linear Quadratic Regulator (LQR) Approach As Applied To Attitude Control, Bendix Corporation MT-40,812, Nov. 20, 1978.
- 5-8 Likins, P., Dynamics And Control Of Flexible Space Vehicles, Jet Propulsion Laboratory, Technical Report 32-1329, Revision 1, Jan. 15, 1970.
- 5-9 Chichester, F. D., Kaczynski, R. F. and Nachmias, S., Application of Hybrid Coordinate Modelling and Multilevel Control Techniques to a Single Axis Torsional Model, Tenth Annual Pittsburgh Conference on Modelling and Simulation, University of Pittsburgh, April 27, 1979.

SECTION 6

6.0 SIMULATION OF MNA CONTROL

Some findings regarding the mathematical analysis, control system design and simulation of a multivariable Nyquist array (MNA) control method are presented here, as they apply to control and stabilization of a large flexible vehicle.

The mathematical model for the space vehicle (SCB Configuration 1) was obtained using the discrete coordinate modeling method described in Section 2. The model was then simulated on a Systems Engineering Lab's SEL/32 digital computer for dynamic evaluation and control system synthesis.

The model was reconfigured into state space equation form for eigenvalue calculations and control system design. The full-order three-axis model was reduced to three five-body single-axis models to determine the effect of cross-axis coupling on the eigenvalues of the three-axis model. It was determined through eigenvalue assignment, that for control system design purposes, each axis could be independently controlled. Further analysis revealed that symmetry in the torsional axis could simplify the control design effort. This condition does not prevail, however, in either the normal or lateral axis.

Using the symmetric single axis model for the torsional mode, a control system design study was performed using the MNA method and the retallack pole placement procedure. The MNA design method reflects a need for single loop bridged-T compensation when a limited number of measurements are available to the control design. This is due primarily to the location of the lightly damped modes within the control system bandwidth. As the bridged-T compensator is a form of closed loop pole assignment, the remainder of the design study for the torsional axis was performed using the Pole Placement method.

Simulation results for the single axis reduced model and the full order three axis model were identical when the pole shifts where made parallel to the real axis. This type of pole shift is a form of "active damping" and was used successfully to achieve acceptable levels of closed loop system performances. The full scale test results confirm the negligible effects of cross-axis coupling from the torsional axis to the normal and lateral axis.

6.1 CONTROL DESIGN FOR THE Z-AXIS

It was decided at this point in the analysis to concentrate the control design effort on the Z axis of Configuration 1 for two reasons. First, the symmetry assumption detailed above simplified the mathematical model for design and analysis purposes. Since the design methods to be described later are new to the

flexible spacecraft application, a complete understanding of the advantages, disadvantages and limitations of the proposed methods is required before more involved models are used. Secondly, the control system design using the reduced Z axis model can be tested on the full five-body three-axis simulation and compared with the time response of the single axis reduced model simulation. A comparison of these time responses will provide the experience and knowledge necessary to pursue the more difficult X and Y axis designs for this and subsequent SCB configurations.

Using the five-body three-axis model, the transfer matrix $G_5(S)$ was computed using Danielevsky's method (reference 6-1). Several of the ninety transfer functions were plotted using Bode methods to reveal that all flexible modes are located within the control system bandwidth. Design problems related to this condition are detailed in References 6-2 and 6-3. This analysis was repeated for the symmetric Z-axis model with the rigid body dynamics removed. A typical magnitude Bode plot is indicated in Figure 6-1, which shows the modes as they appear in the system bandwidth. The complete set of transfer functions is indicated in Appendix B.

The eigenvalues for the reduced order model (ROM) are:

- a. 0.0
- b. 0.0
- c,d. -.00500564 + j1.00112
- e,f. -.00160836 + j0.32045

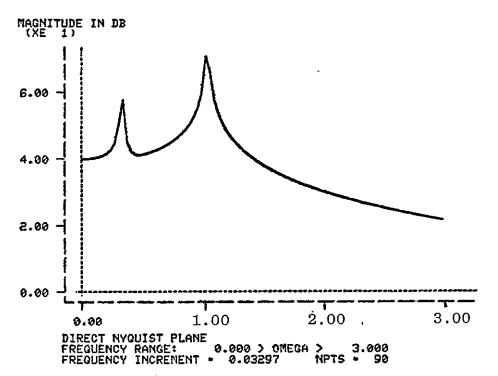


Figure 6-1. A Typical Bode Diagram for the Z Axis

This set corresponds to a denominator form of:

$${\rm S}^2 \ ({\rm S}^2 \ + \ 2 \delta_1 \omega_1 {\rm S} + \omega_1^2) \ ({\rm S}^2 + 2 \delta_2 \omega_2 {\rm S} + \omega_2^2)$$

where the roots of each quadratic term are:

$$S_1, S_2 = -\delta\omega + j\sqrt{\omega^2(1-\delta^2)}$$

For $\delta <<1,~S_1,S_2~\cong -~\delta \underline{\omega +}~j\omega$ and

$$\omega = Im(\lambda)$$

$$\delta = \text{Re}(\lambda)/\text{Im}(\lambda)$$

where λ is a complex eigenvalue. With the eigenvalue set above

$$\omega_1 = 1.00112
\omega_2 = .32045$$
 $\delta_1 = .00500004
\delta_2 = .00501907$

The control system design for the ROM Z-axis model will proceed using the MNA method and the Retallack pole placement method. The MNA method will be considered using only ω_1 and ψ_{21} as the controlled outputs with τ_{1Z} and τ_{2Z} as the system inputs. The pole placement method will shift specific eigenvalues to prescribed locations using full state feedback.

6.2 MNA DESIGN FOR ROM Z-AXIS

Using the appropriate transfer functions from Appendix B, a direct Nyquist array (DNA) design was initiated over the frequency range $0 \le \omega \le 3.0$ using the technique described in Subsection 3.3. Recent results described in Reference 6-4 for finite frequency Nyquist array designs establish this range as acceptable for design and stability purposes.

For this DNA design the postcompensator matrix was prespecified as the identity matrix with the precompensator matrix selected in accordance with the algorithm in Reference 6-5. The closed loop diagram for this axis with

$$Q(S) = L G(S) K$$
 (6-1)

representing the forward loop transfer matrix is indicated in Figure 6-2,

where: G(S) = spacecraft vehicle transfer matrix L, K = Post- and pre-compensator matrices F(S) = Feedback transfer matrix.

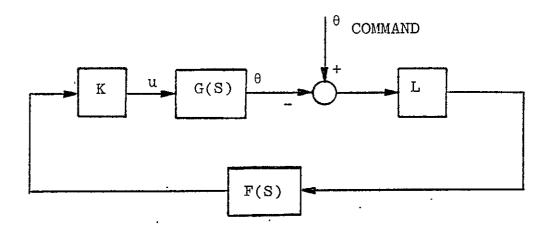
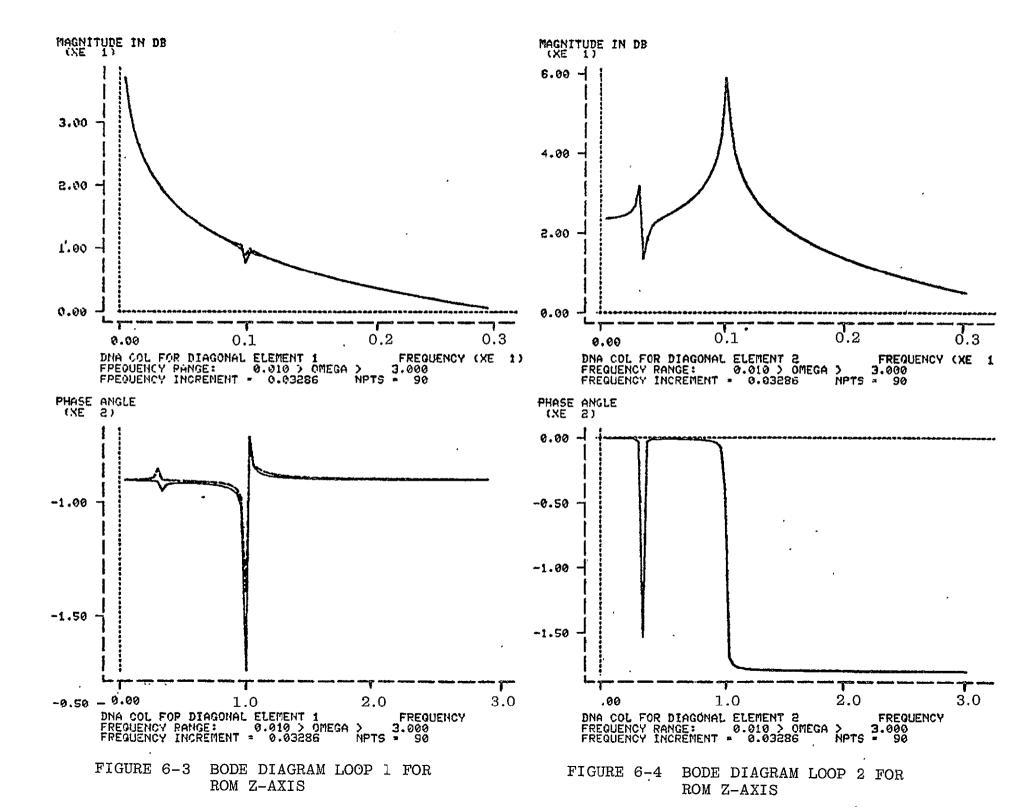


Figure 6-2. Closed Loop Spacecraft Control Diagram

In Reference 6-6, a procedure is described whereby Multivariable Bode diagrams can be obtained from MNA results using Reference 6-7. This procedure has been incorporated into an interactive design suite in Reference 6-8. Results for the ROM Z-axis are presented in Figures 6-3 and 6-4. The dominance levels obtained using equation (3-32) are very small, thus reflecting a decoupled condition as indicated by the virtual coincidence of the envelope curves in the Bode diagrams.

From Figure 6-3, the effect of solar wing interaction on the rigid body dynamics is seen to be negligible. Hence the control in loop 1 may proceed using a rigid body assumption. The dynamics indicated in Figure 6-4 reflect the lightly damped poles at $\omega=.32$ and $\omega=1.0$ and also indicate the presence of a



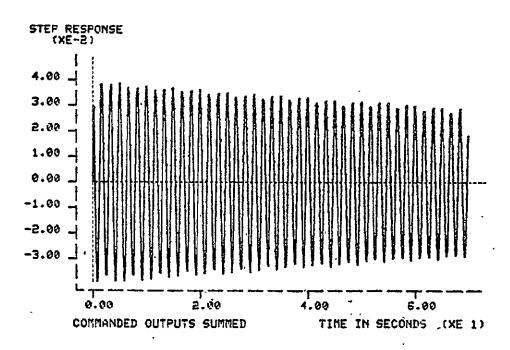
multivariable zero near ω = .32. Since this antiresonance is sharper than that of the pole at ω = .32, the damping ratio for the zero is less than 0.005.

One possibility for the control of the mode at $\omega=.32$ is to decrease the damping ratio of the pole via a bridged-T compensator and shift the pole location to that of the multivariable zero. This approach would correspond to a pole-zero cancellation in the traditional single-input single-output case. Uncertainties in the dynamic model could, however, have a deleterious effect on the overall system behavior.

Alternatively the poles could be shifted outside the control bandwidth (active stiffening) and/or reduce the pole resonance peaks (active damping). Figure 6-5 indicates the time response of ψ_{21} in the closed loop system without dynamic compensation. In Figure 6-6, the Bode diagram for loop 2 is presented following a bridged-T compensator insertion to increase the damping ratio at $\omega=1.0$ to $\delta=0.1$.

$$F_{22}(S) = \frac{S^2 + .01 S + 1.01}{S^2 + .2 S + 1.01}$$
 (6-2)

Figure 6-7 indicates the closed loop time response for $\psi_{21}(t)$ using (6-2). Retaining the pole at $\omega=1.0$ has the effect of reducing the impact of the resonance at $\omega=0.32$ as it will appear principally as an envelope modulation in the time response.



FIGUR E-5 CLOSED LOOP TIME RESPONSE FOR $\psi_{\mathbf{21}} \text{ WITH NO DYNAMIC COMPENSATION.}$

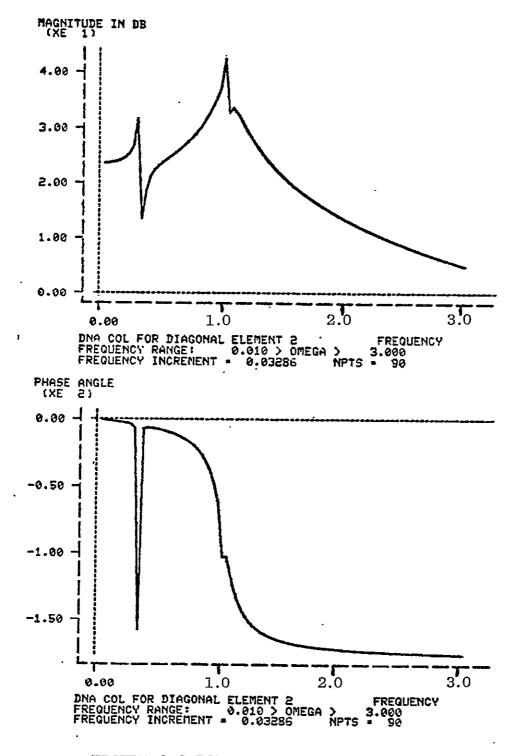


FIGURE 6-6 BODE DIAGRAM LOOP 2 WITH BRIDGED-T COMPENSATOR INSERTED

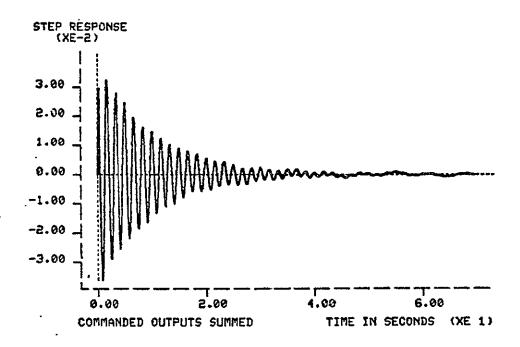


FIGURE 6-7 CLOSED LOOP ψ_{21} TIME RESPONSE FOR COMPENSATED SYSTEM

To examine the shift in frequency of the pole at $\omega = 1.0$, a bridged-T compensator was placed in loop 2 to increase the damping ratio to $\delta = 0.1$ and simultaneously shift the resonance to $\omega = 2.0$. This is equivalent to placing a complex zero pair at $\omega = 1.0$ and a complex pole pair at $\omega = 2.0$. The Bode diagram for this case is indicated in Figure 6-8 with the corresponding closed loop time response presented in Figure 6-9. Note that the zero placement removes the impact of the pole at $\omega = 1.0$ but increases the effect of the resonance at $\omega = .32$. This latter effect is due to the pole relocation at a higher frequency; i.e., system gain is effectively reduced by 50%. To recover the effect of Figure 6-7 the loop gain should be doubled. Alternatively, pole shifts in the resonance at $\omega = .32$ could be used. However, this would ultimately require a fourth order compensator for $f_{33}(S)$ in the closed loop control.

The above analysis and design synthesis for the ROM Z-axis model demonstrates the utility of the MNA method in the design of controls for flexible spacecraft. At this point, it was decided to postpone further design efforts using MNA procedures to examine the potential of the Retallack pole placement method.

6.3 RETALLACK POLE PLACEMENT FOR ROM Z-AXIS

The dyadic pole placement technique developed by Simon and Mitter (Reference 6-9) and further refined by Retallack and MacFarlane (Reference 6-10) utilizes the

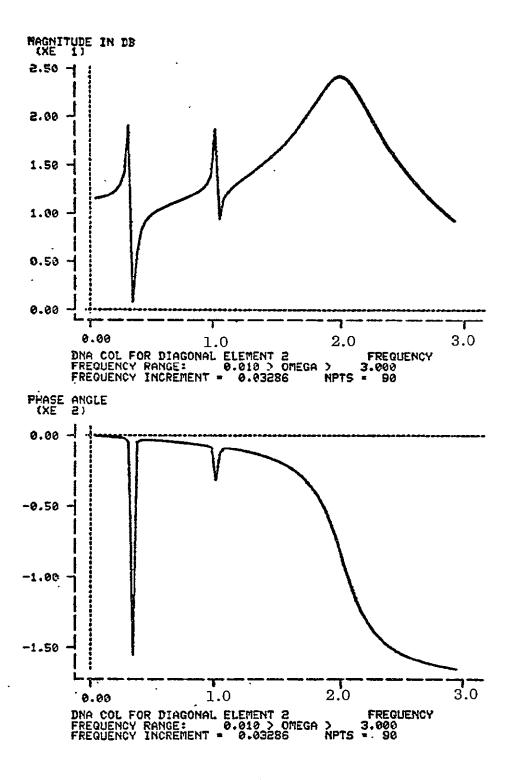
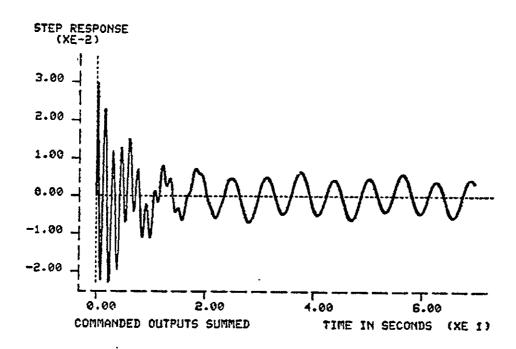


FIGURE 6-8 BODE PLOT FOR LOOP 2 WITH SIMULTANEOUS FREQUENCY AND DAMPING RATIO SHIFT OF POLE AT $\omega = 1.0$.



FUGYRE 6-9 CLOSED LOOP TIME RESPONSE FOR ψ_{21}

model structure of a linear system to give the designer direct control over the movement of given system modes to desired closed loop locations. Unlike other methods, the Retallack algorithm is a state feedback procedure which allows for the direct assignment of specific open loop poles to specific closed loop locations. This method is particularly attractive from a design viewpoint whenever the open loop poles can be directly associated with specific parts of the physical system. In this way only those poles directly associated with the subsystem will be shifted.

Let λ_j $(j=1,\cdots,n)$ represent the open loop poles of the system and let ρ_i $(i=1,\cdots,n)$ be the desired closed loop set. Several algorithms are presently available to shift the eigenvalue set $\{\lambda_j\}$ to the desired set $\{\rho_i\}$. However, there is no guarantee that any particular eigenvalue λ_j will be moved to a specific location $\dot{\rho}_i$. Without this eigenvalue location assignment flexibility, the resulting control in light of sensor and/or actuator failures could result in very unsatisfactory performance.

Given the dynamic system

$$\dot{x} = Ax + Bu \tag{6-3}$$

and the control law of the form

$$u(t) = r - Kx \tag{6-4}$$

where r is the set point control, the eigenvalues $\{\rho_{\mbox{\scriptsize j}}\}$ of the resulting closed loop system

$$\dot{\mathbf{x}} = (\mathbf{A} - \mathbf{B}\mathbf{K}) \mathbf{x} + \mathbf{B}\mathbf{r} \tag{6-5}$$

are related to the open loop eigenvalue (λ_j) by the Hsu-Chen equation (Reference 6-11)

$$\left| I_{n} - (SI_{n} - A)^{-1} BK \right| = \frac{\prod_{i=1}^{n} (S - \rho_{i})}{\prod_{j=1}^{n} (S - \lambda_{j})}$$
 (6-6)

The Jordan Cononical form for A is given by:

$$\Lambda = U^{-1} AU \tag{6-7}$$

where U is the modal matrix for A. Let $(\lambda_1, \lambda_2, \cdots, \lambda_p)$ p≤n be the open loop poles to be shifted and define the modal controller K using the unity rank dyadic product as

$$K = f d^{T} V ag{6-8}$$

where f is an m vector, d is a p vector and V contains the p rows of U^{-1} corresponding to $(\lambda_1, \dots, \lambda_p)$. Using (6-8), Retallack reduces (6-6) to

Using (6-8), Retallack reduces (6-6) to

$$1+d^{T} (SI_{p} - \Lambda)^{-1} \beta = \frac{\prod_{j=1}^{p} (S-\rho_{j})}{\prod_{j=1}^{p} (S-\lambda_{j})}$$
(6-9)

where

$$\beta = VBF \tag{6-10}$$

The remaining open loop poles ($\lambda_{p+1}, \dots, \lambda_p$) remain unchanged under dyadic feedback.

To overcome some of the numerical difficulties associated with the computation of the modal controller when clustered poles appear near the imaginary axis (Reference 6-12), the system in (6-3) is transformed to the Luenberger canonical Form (Reference 6-13),

$$\dot{\mathbf{w}} = \mathbf{\hat{A}}\mathbf{w} + \mathbf{\hat{B}}\mathbf{u} : \tag{6-11}$$

where $w = U^{-1} x$ and

$$\hat{A} = U^{-1}AU \qquad (6-12)$$

$$\hat{\mathbf{B}} = \mathbf{U}^{-1}\mathbf{B} \tag{6-13}$$

An efficient algorithm to realize this transformation is presented in Reference 6-14.

Since the eigenvalues of $(\hat{A}-\hat{B}\hat{K})$ are identical to those of A-BK, the pole placement process can be accomplished in the closed-loop system of (6-11) rather than in the closed-loop system in (6-3). Once the gain matrix K has been determined for the canonical system, the desired modal controller K for the original system (6-3) is given by

$$K = \hat{K}U^{-1} \tag{6-14}$$

For the ROM Z-axis model provided in Appendix B the system equations can be partitioned into two distinct sets: one for the rigid body dynamics and one

for the flexible appendage. The open loop eigenvalue sets are, respectively,

Set 1: 0.0, 0.0

Set 2: -.00500564 + j 1.00112 -.00160836 + j 0.320495

Here ψ_1 was added to the state vector to produce the second pole at the origin. The state variables are then $\omega_1,~\omega_{21},~\omega_{42},~\psi_{21},~\psi_{42},~$ and ψ_1 with controls τ_{1Z} and $\tau_{2Z}.$ For the five-body single-axis control implementation τ_{3Z} is set equal to τ_{2Z} since symmetry was used to generate the Z-axis ROM.

The rigid body eigenvalues were shifted to the following positions

a1. -.1, -.1

b1. -.2, -.2

c1. -.3, -.3

d1. -.7, -.7

while the modes corresponding to the solar wing were shifted to

a2. -.1 + j 1.00112

-.1 + j 0.320495

b2. -.2 + j 1.00112

-.2 + j 0.320495

c2. -.7 + j 1.00112

 $-.7 \pm j 0.320495$

The resulting control laws were implemented in a time domain simulation of the Z-axis reduced order model with ψ_1 (t_0) = .02 radians. Since all velocities, ψ_{21} (t_0) and ψ_{42} (t_0) are zero, this condition corresponds to an equilibrium point with all masses displayed .02 radians from the desired equilibrium point. In each case, the control restored the vehicle to the desired location in the manner indicated by the closed loop eigenvalue characteristics. Table 6-1 compares several of the important characteristics of the simulator responses.

The main purpose of this study was to demonstrate that the Retallack Pole Placement method can be effectively used in the control of flexible space vehicles of the SCB configuration. Several observations resulting from this effort are indicated below:

- 1. As the eigenvalues of the rigid body are moved further into the left half plane with fixed solar wing eigenvalues, the peak to peak excursions of ψ_{21} and ψ_{42} increase appreciably with little variation in the time to steady state.
- 2. For fixed rigid body eigenvalues and variable solar wing eigenvalues, the time to steady state decreases in proportion to the rate of increase in the damping ratio with small variations in the peak to peak excursions of ψ_{21} and ψ_{42} .

TABLE 6-1 CLOSED LOOP RESPONSE $\psi_1(0) = 0.02$

EIGENVALU		MAX	MAX	TIME TO STEADY STATE AND PEAK VALUE					
SET NUMBER		$ ^{\tau}_{1Z} $	$ ^{ au}_{2\mathrm{Z}} $	ψ_{1}		$^{\psi}$ 21;		$^{\psi}42$	
				SECONDS	RADIANS	SECONDS	RADIANS	5	RADIANS
a ₁ , a ₂		53.7	0.320	50.0	0.02	25.0	0.00050	25.0	0.0016
b ₁ , a ₂		214.82	1.112	29.0	0.02	30.0	0.0021	24.0	0.0047
c ₁ , a ₂		483.35	2.025	20.0	0.02	36.0	0.0041	30.0	0.0079
a ₁ , b ₂		53.7	0.461	50.0	0.02	21.0	0.00085	25.0	0.0017
b ₁ , b ₂		214.82	1.4518	29.0	0.02	25.0	0.0026	22.0	0.0051
c ₁ , b ₂	6-10 to 6-14	483.4	2.717	17.0	0.02	25.0	0.0051	17.0	0.0088
d_1 , b_2	6-15 to 6-19	2631.6	9.071	8.0	0.02	18.5	0.0171	18.5	0.0218
d ₁ , c ₂	6-20 to 6-24	2631.6	30.637	8.0	0.02	13.0	0.0207	12.0	0.0303

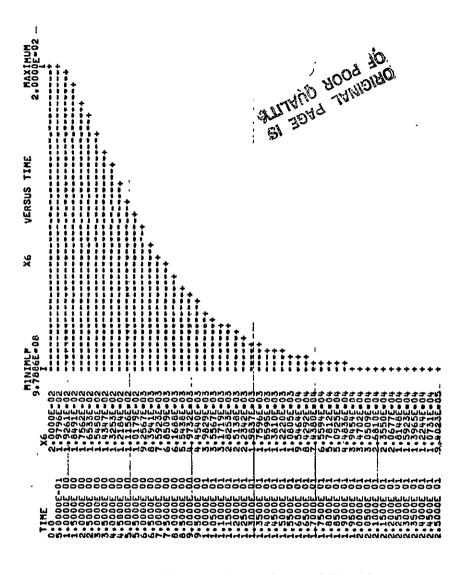


FIGURE 6-10 ANGULAR POSITION BODY 1

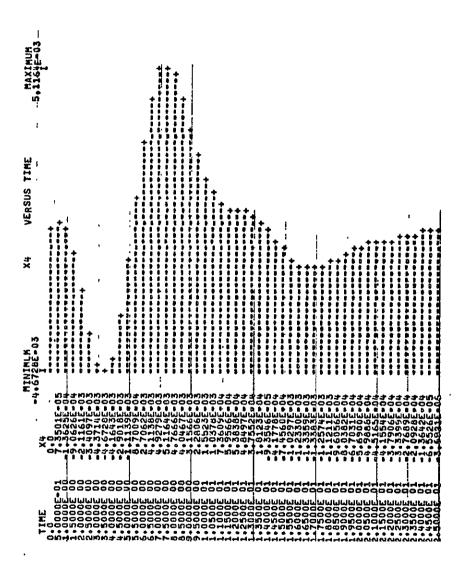


FIGURE 6-11 RELATIVE ANGULAR POSITION BODY 2

X5

FIGURE

6-12

RELATIVE ANGULAR POSITION

FIGURE

6-13

CONTROL TORQUE BODY

VERSUS TIME

8.8173E-03

VERSUS TIME 6.5330E-01 U1

MAL PAGE 15 SOOR QUALITY

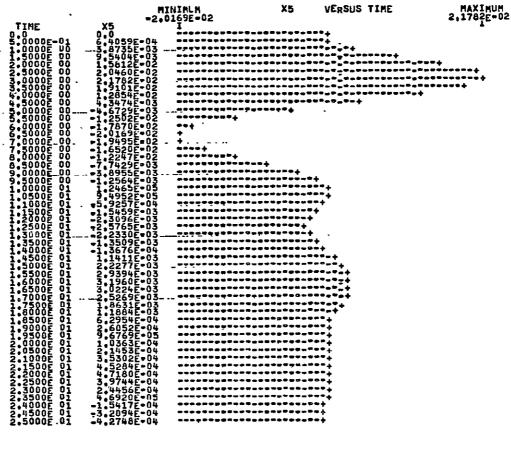
- پ

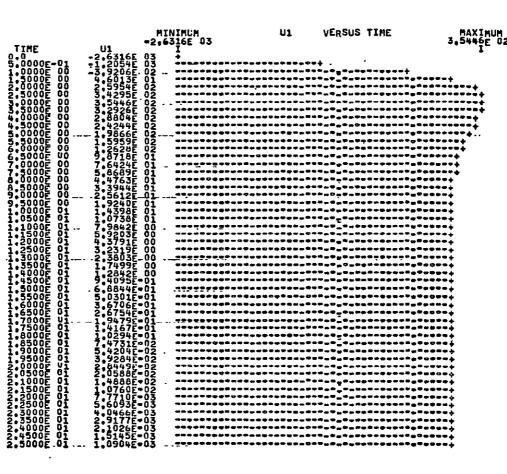
*-u	MINI 4.540	ๆบศ 5E+16 -	Х6	VERSUS TIME	MAXIMUM 2.0000E=02
FIGURE 6-15 ANGULAR POSITION BODY 1	277 E 02 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	•			
FIGURE 6-16 RELATIVE ANGULAR POSITION BODY 2	1. 443-142-142-142-142-142-142-142-142-142-142		X4	VERSUS TIME	#AXIMUM 1.7140E=82

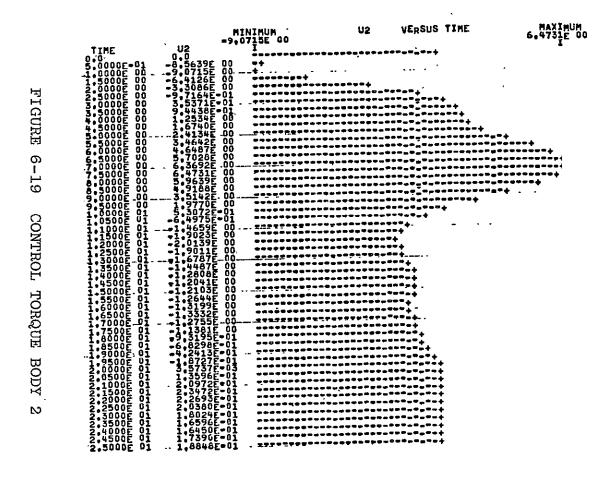
FIGURE 6-17 RELATIVE ANGULAR POSITION BODY 4

FIGURE 6-18 CONTROL TORQUE

BODY







#INITINUM X6 VERSUS TIME 2,000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

1000012-02

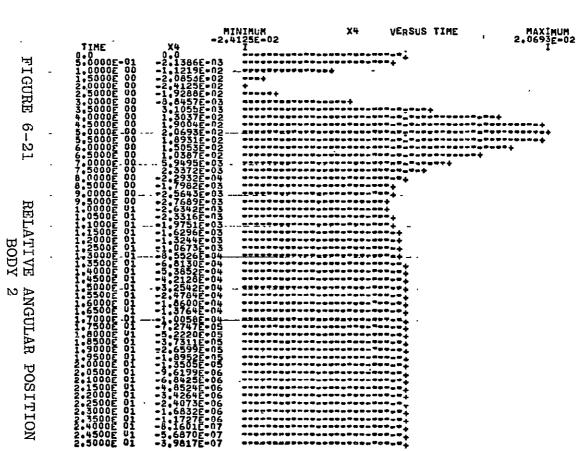
1000012-02

1000012-02

1000012-02

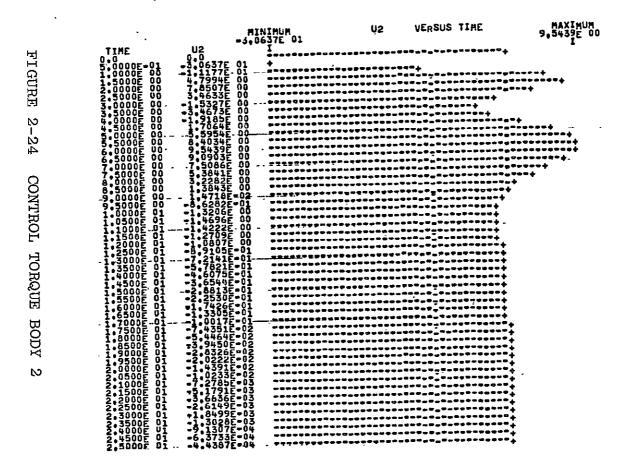
1000012-02

1000



X5

-2.2			3.0250E-02
TIME X5	I		1
0.0 5.0000E-01 3.1048E-03	**********	•	
1.0000E 00 1.4193E-02 1.5000E 00 2.5790E-02			
2.0000E 00 3.0250E-02 2.5000E 00 2.5514E-02			
2.0000E 00 3.0250E-02 2.5000E 00 2.5514E-02 3.0000E 00 1.4151E-02	****************		+ .
3,0000E 00 1.4151E=02 3,5000E 00 5.7218E=04			•
4.0000 00 -1.1289E-02 4.5000 00 -1.9116E-02	****		
.5.0000E .00	- 		
3.5000E 00 5.7218E-04 4.5000E 00 -1.1289E-02 4.5000E 00 -2.2339E-02 5.0000E 00 -2.1655E-02 6.5000E 00 -1.33927E-02 6.5000E 00 -1.33927E-02	+		
6.5000F 00 -1.3927E-02			
7.0000E 00 -5.3920E-03 7.5000E 00 -5.4672E-03 8.0000E 00 -2.5274E-03		•	
8.0000F 00 -2.5274F-03			
8.5000 00 -5.3521E-04 9.0000E 00 -4.3809E-04			
9.0000E 00 6.3809E 004 9.5000E 00	**************		
1.0000E 01	******************		
1.000E 01 1.3460E 03 1.1000E 011.2029E 03	,424524534444444444444444		
1.15000 01 1.02945-03	******************		
1.1500E 01 1.0294E-03 1.2000E V1 8.6165E-04 1.2500E 01 7.1349E-04	********		
-1-3000F - 015-8712F = 04			
1.1500E 01 1.0294E-03 1.200E 01 8.6165E-04 1.2500E 01 7.1374E=04-1.3500E 01 4.8003E-04 1.3500E 01 3.800E-04 1.4500E 01 3.8185E-04			
1.4500E 01 3.1105E-04 1.5000F.01 2.4492F=04			
1.5500E 01 1.8949E-04			
1.6500F 01 1.0751F=04			
1.7000E-017.9056E-05			
1.4000E 01 3.8887E-04 1.5500E 01 2.4422E-04 1.5500E 01 1.4398E-04 1.6000E 01 1.07556E-05 1.7000E-01 - 7.7556E-05 1.7500E 01 4.1398E-05 1.6500E 01 4.1398E-05 1.6500E 01 4.1398E-05 1.6500E 01 4.1398E-05 1.6500E 01 2.9156E-05			
1.85000 01 2.95580-05			
1.9000E 01 2.1100E-05 1.9500E 01 1.5059E-05			
1.9500F 01 1.5059E-05 2.0000E 01 7.664E-06 2.0000E 01 5.4770E-06 2.1000E 01 5.4770E-06 2.2000E 01 2.890E-06	************		
2.1000E 01 5.4770E-06			
2.1500F 01 3.8919F=06			
2.2500E 01 1.9309E-06			
2.3000E 01 1.3464E+06 2.3500E 01 9.3361E+07			
1.9500 01 2.9556 05 05 01 1.5056 05 05 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 06 01 1.5056 05 00 1 1.5056 05 05 00 1 1.5056 05 05 05 05 05 05 05 05 05 05 05 05 05			
2.4500E 01 4.4636E=07 2.5000E-01 3.1003E=07			
•			
, MI	NIMUM_ U1 !	VERSUS TIME	WYXIMUH MAXIMUH
TIME 1112.6	316E 03 -	•	MAXIMUM 3.5446E 02
TIME 1112.6	316E 03 -	•	MAXIMUM 3.5446E 02
TIME 1112.6	316E 03 -	•	MAXIMUM 3.544 E 02
TIME 1112.6	316E 03 -	•	MAXIMUM 3.5446E 02
TIME 1112.6	316E 03 -	•	MAXIMUM 3.5446E 02
TIME 1112.6	316E 03 -	•	MAXIMUM 3,5446E 02
TIME U111644 000 000 000 000 000 000 000 000 000	316E 03 -	•	MAXIMUM 3,5445E 02
TIME U111644 000 000 000 000 000 000 000 000 000	316E 03 -	•	MAXIMUM 3,5446E 02
TIME U111644 000 000 000 000 000 000 000 000 000	316E 03 -	•	MAXIMUM 3,5446E 02
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	316E 03.		
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1			
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	316E 03		
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2			
- 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2 - 2	316E 03.		



- $\hat{3}.$ The maximum absolute value of $\tau_{\rm 1Z}$ increases exponentially as the rigid body dynamics are moved farther into the left half plane. See Figure 6-25.
- 4. The maximum absolute value of τ_{2Z} is proportional to the peak to peak excursions in the state variables associated with the solar wings. From Table 6-2 the feedback gains increase significantly as the real part of the eigenvalues increase. Also the rate of increase in the gains associated with ψ_{21} and ψ_{42} is greater than the rate of increase in the gains associated with ω_{21} and ω_{42} as Re(λ) increases. The significance of this will appear when sensor failure studies are undertaken.

The above analysis relates to the time domain simulation of the Z axis reduced order model. Application of the control laws developed above were applied to the full scale five-body three-axis simulation.

These results are provided in Figures 6-26 through 6-30 for eigenvalue sets cl and b2 (corresponding to Figures 6-10 to 6-14 of the ROM). A comparison of the simulations for the full order model (FOM) with the simulations of the Z-axis reduced order model (ROM) demonstrates the effectiveness of the design method and the validity of the model reduction procedure.

The simulation results for the FOM for the other eigenvalue sets obtained using the ROM control also showed excellent. comparison with the ROM simulation results.

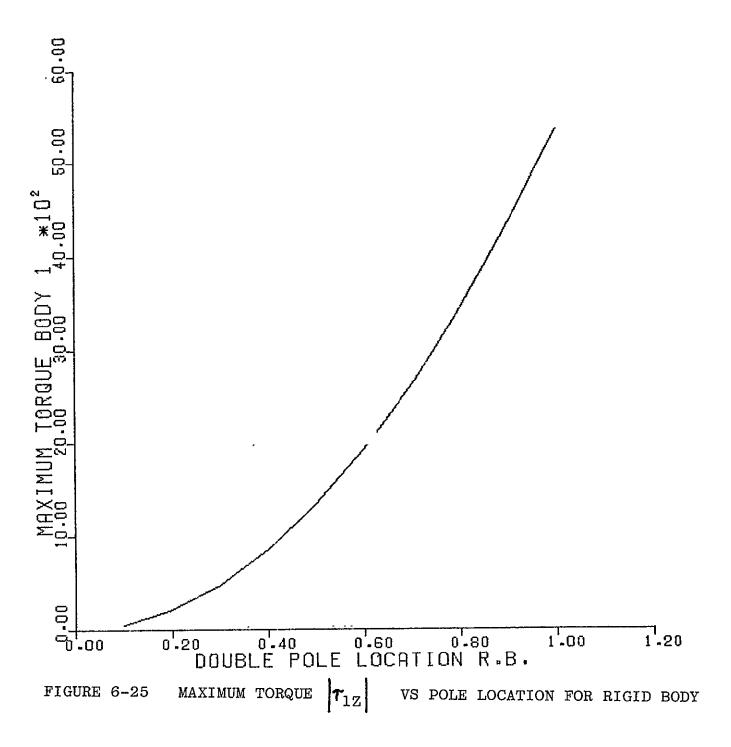


TABLE 6-2 . GAIN MATRIX FOR τ_{2Z} $\tau_{2Z} \doteq - \text{Kx(t)}$

REAL (λ)	ω ₁	^ω 21	^ψ 42	Ψ21	^ψ 42	Ψ ₁
0.10	0.0	1433.2	1140.2	68.411	30.98	0.0
0.20	0.0	, 3045,5	2449.4	291.98	124.97	0.0
0.70	0.0	19199.	17067.	5193.1	3003.8	0.0

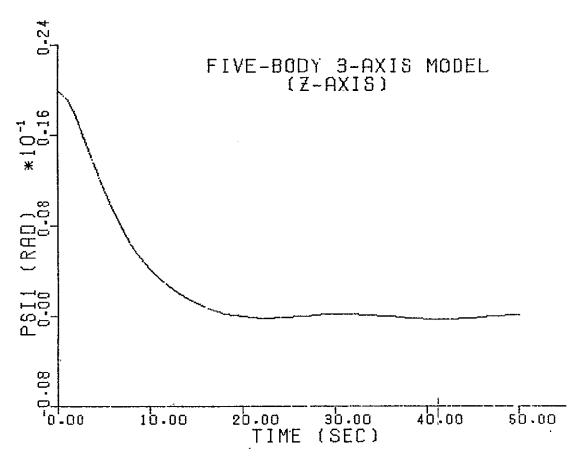


FIGURE 6-26- ANGULAR POSITION BODY 1

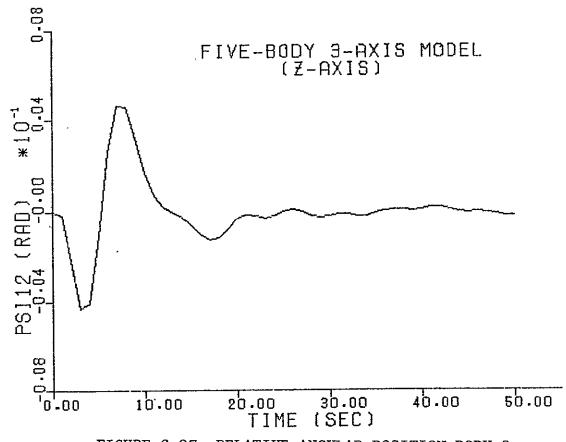


FIGURE 6-27 RELATIVE ANGULAR POSITION BODY 2 6-33

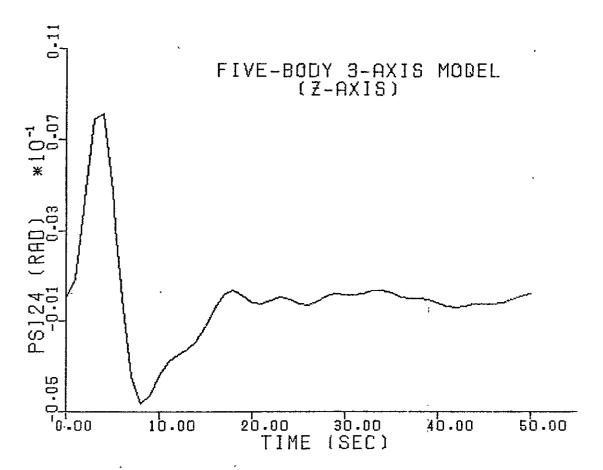


FIGURE 6-28 RELATIVE ANGULAR POSITION BODY 4

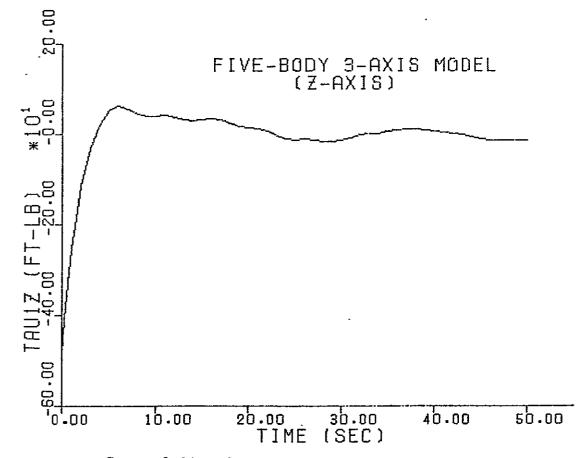


FIGURE 6-29 CONTROL TORQUE BODY 1

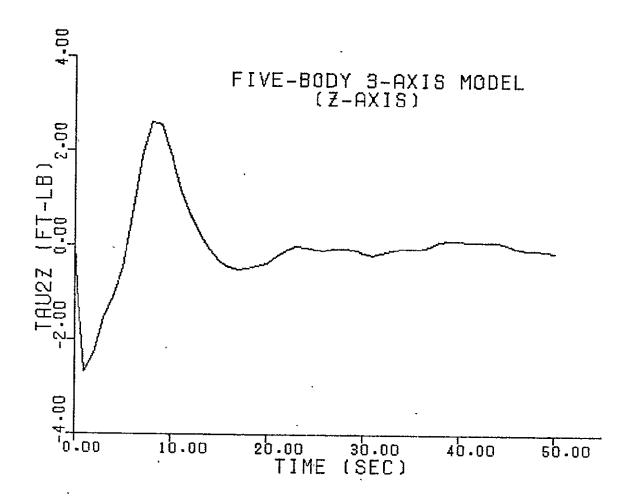


FIGURE 6-30 CONTROL TORQUE BODY 2

6.4 CONCLUSIONS AND RECOMMENDATIONS

An eigenvalue analysis of the five-body three-axis Space Construction Base/Configuration I vehicle shows that the eigenvalue shifts from a double pole configuration are due to the interaxis coupling of the solar wings. Cross-axis coupling for this vehicle has been shown to be negligible thus leading to the conclusion that from a control design viewpoint, each axis can be designed separately.

Using a symmetric reduced order model for the torsional axis, two new design procedures were studied. The multivariable Nyquist array method, a frequency domain design technique, was shown to be effective for the difficult case of the flexible modes within the control system bandwidth. Utilization of the multivariable Bode diagram facilitated the design process since standard single-input single-output methods could be used. Retallack pole placement technique when coupled with a computationally efficient numerical algorithm to obtain the Luenberger canonical form was effective in placing specific open loop poles in desired positions. domain simulations demonstrated the potential of this method.

It is apparent from the results obtained that the methods used in this study should be investigated further. Specifically, several areas of consideration are identified:

a) Design and evaluation associated with pole shifts in frequency as well as in damping ratio.

- b) Repeat design for the Y axis with and without the symmetry assumption. Compare designs using both MNA and pole placement procedures.
- c) Repeat the design for the X axis using MNA and pole placement.
- d) Sensitivity analysis of the control configuration under model parameter uncertainties.
- e) Sensor failure analysis in all axes and a simplification in the system gain space description for failure accommodation.
- f) Develope a test for robustness of the control design as a means of simplifying the design for future configuration studies.
- g) Incorporate design constraints on control magnitude and state measurement in the selection of control weighting vectors used in the pole placement procedure.
- h) Incorporate gain magnitude constraints and develop a criteria for gain selection based upon time domain waveforms.
- i) Consider a Kalman pole placement algorithm to sequentially place poles in desired locations using the criteria suggested above.
- j) Compare results using standard pole placement (Simon and Mitter) techniques and evaluate subsequent designs for robustness.

6.5 REFERENCES

- 6-1 Faddeeva, V.N., Computational Methods of Linear Algebra, Dover, Chapter, 3, 1979.
- 6-2 Porcelli, G., "Attitude Control of Flexible Space Vehicles", AIAA Journal, Vol. 10, No.6, June 1972.
- 6-3 Leininger, G.G., "Alternate Frequency Domain
 Design Methods for the Attitude Control of a Flexible Space Vehicle", Progress Report: Phase I prepared for Bendix Research Laboratory, May 1978.
- 6-4 Leininger, G.G. "New Dominance Characteristics for the Multivariable Nyquist Array Method", to appear International Journal of Control, 1979.
- 6-5 Leininger, G.G., "Diagonal Dominance for Multivariabl Nyquist Array Methods Using Function Minimization", Automatica, Vol 15, No.3, Pages 339-436, 1979
- 6-6 Leininger, G.G. "Compensator Design for Multivariable Systems Using Bode and Nichols Methods", IFAC - Symposium on Computer Aided Control System Design, Zurich, August 1979.
- 6-7 Crossley, T.R., "Envelope Curves to Inverse Nyquist Array Diagrams", Int. J. Control, Vol 22, No.1, 1975.

- 6-8 Leininger, G.G., "An Interactive Design Suite for the Multivariable Nyquist Array Method", IFAC- Symp. on Computer Aided Control System Design, Zurich, August 1979.
- 6-9 Simon, J.D. and Mitter, S.K., "A Theory of Modal Control", <u>Information and Control</u>, Vol. 13, No.4, pp. 316-3353, October 1968.
- 6-10 Retallack, D.G. and MacFarlane, A.G.J., "Pole-Shifting Techniques for Multivariable Feedback Systems", Proc. IEE, Vol. 117, No.5, pp. 1037-1038, May 1970.
- 6-11 Hsu, C.H. and Chen, C.T., "A Proof of the Stability of Multivariable Feedback Systems", Proc. IEEE, Vol 56, pp. 2061-2062, 1968.
- 6-12 Wu, Y.W., Juang, J.N., and Rice, R.B., "Control of Large Flexible Space Structures Using Pole Placement Design Techniques", AIAA Guidance and Control Conference, Boulder, Colorado, August 1979.
- 6-13 Luenberger, D.G., "Canonical Forms for Linear Multi-variable Systems", IEEE-AC, Vol AC-12, pp. 290-293, June 1967.
- 6-14 Jordan, D. and Sridhar, B., "An Efficient Algorithm for the Calculation of the Luenberger Canonical Form", IEEE-AC, Vol. AC-18, pp. 292-295, June 1973.

SECTION 7

7.0 ALTERNATE CONTROL APPROACHES

Among alternate approaches to the application of control to the Space Construction Base one of the most promising appears to be the general one presented in this section. In the sequel this approach is developed for a plant (system to be controlled) that may be represented by a broad class of linear, constant parameter multivariable mathematical models.

The general development of this approach begins with a description of the salient characteristics of the class of linear constant parameter multivariable plants for which the approach is applicable. The matrix properties of the plants are then utilized in the development of techniques for the generation of state regulator control and estimation gain matrices that optimize plant performance.

Following the development of the general approach to the design of state controllers and estimators for this class of linear constant parameter multivariable plants, the considerations involved in applying this general approach to the rotational mathematical model of the Space Construction Base are discussed. These considerations include treatment of cyclical aerodynamic disturbance torques, selection of weighting coefficients for state variable estimation error in the computation of optimal estimator gain and decomposition of the known portion of input disturbances into terms corresponding to gravity gradient, actuator reaction and actuator desaturation torques.

7:1 LINEAR, CONSTANT PARAMETER, MULTIVARIABLE CONTROL APPROACH

7.1.1 Plant

Consider the following plant

$$\frac{\dot{\mathbf{x}}}{\mathbf{p}} = \mathbf{A}_{\mathbf{p}} \mathbf{x}_{\mathbf{p}} + \mathbf{C}(\mathbf{u} + \mathbf{y}) + \mathbf{D}\mathbf{w}$$
 (7-1)

$$\underline{y} = B_{\mathbf{p}} \underline{x}_{\mathbf{p}} \tag{7-2}$$

where:

 \underline{x}_{p} = plant state vector of dimension n

u = plant control vector of dimension c

w = plant control disturbance vector of dimension c

w = plant disturbance vector of dimension d

y = plant measurement vector of dimension m

 A_{p} = uncontrolled plant matrix of dimension nxn

C = plant control matrix of dimension nxc

D = plant disturbance matrix of dimension nxd

 B_{p} = plant measurement matrix of dimension mxn

Suppose that the jth column of the plant control matrix is linearly dependent. Then we can write:

$$C(\underline{\mathbf{u}} + \underline{\mathbf{v}}) = C_{\mathbf{j}}(\underline{\mathbf{u}}_{\mathbf{j}} + \underline{\mathbf{v}}_{\mathbf{j}}) + \underline{\mathbf{c}}_{\mathbf{j}}(\mathbf{u}_{\mathbf{j}} + \mathbf{v}_{\mathbf{j}})$$

$$= C_{\mathbf{j}}(\underline{\mathbf{u}}_{\mathbf{j}} + \underline{\mathbf{v}}_{\mathbf{j}}) + C_{\mathbf{j}}\underline{\mathbf{c}}(\mathbf{u}_{\mathbf{j}} + \mathbf{v}_{\mathbf{j}})$$

$$= C_{\mathbf{j}}[\underline{\mathbf{u}}_{\mathbf{j}} + \underline{\mathbf{v}}_{\mathbf{j}} + (\mathbf{u}_{\mathbf{j}} + \mathbf{v}_{\mathbf{j}})\underline{\mathbf{c}}] = C'(\underline{\mathbf{u}}_{\mathbf{j}}^{\mathsf{T}} + \underline{\mathbf{v}}_{\mathbf{j}}^{\mathsf{T}})$$

$$(7-3)$$

where:

 $C_{j} = C$ minus the jth column

 $\underline{\underline{u}}_{j} = \underline{\underline{u}}$ minus the jth component.

 $\underline{v}_{i} = \underline{v}$ minus the jth component

 \underline{c}_i = jth column of C $u_j = jth component of \underline{u}$ $v_{i} = jth component of v$ c = constant vector of dimension c-1

Thus we can assume, without loss of generality, that C has rank c. If M is a real symmetric matrix, then M and M have the same rank. Hence, defining:

$$M *= (M^{T}M)^{-1}M^{T}$$
 (7-4)

we can write:

$$C(\underline{\mathbf{u}} + \underline{\mathbf{v}}) + D\underline{\mathbf{w}} = C(\underline{\mathbf{u}} + \underline{\mathbf{v}} + C^*D\underline{\mathbf{w}}) + (\mathbf{I} - CC^*)D\underline{\mathbf{w}}$$

$$= C(\underline{\mathbf{u}} + \underline{\mathbf{v}}^*) + D^*\underline{\mathbf{w}}$$
(7-5)

Since C^TD^{\prime} ;=0, we can assume without loss of generality that the columns of C are orthogonal to the columns of the plant disturbance matrix. Now suppose that the ith row of the plant measurement matrix is linearly dependent. Then we can write:

$$B_{p} = \underline{y}$$
 (7-6)

$$\mathbf{y}_{i} = \left[\left(\mathbf{B}_{p}^{T} \right)^{T} \underline{\mathbf{c}} \right]^{T} \underline{\mathbf{x}}_{p} = \underline{\mathbf{c}}^{T} \underline{\mathbf{y}}^{T}$$
 (7-7)

where:

 $B_p' = B_p$ minus the ith row $\underline{y}' = \underline{y}$ minus the ith component

 y_i = The ith component of y

 \underline{c} = a constant vector of dimension m-1

Thus we can assume without loss of generality that ${\bf B}_{\mbox{\it p}}$ has rank m. Furthermore, it is assumed that:

- 1) c < n and m < n
- 2) All matrices are constant
- 3) The unknown part of \underline{v} and \underline{w} can be written as $B_d\underline{x}_d$ where \underline{x}_d satisfies the following matrix differential equation.

$$\dot{\underline{\mathbf{x}}}_{\mathbf{d}} = \mathbf{A}_{\mathbf{d}} \dot{\underline{\mathbf{x}}}_{\mathbf{d}} \tag{7-8}$$

That is,

$$\underline{\mathbf{v}} = \underline{\mathbf{v}}_{\mathbf{k}} + \mathbf{B}_{\mathbf{v}}\underline{\mathbf{v}} \tag{7-9}$$

where:

$$\dot{\underline{x}}_{V} = A_{V} \underline{x}_{V} \tag{7-10}$$

and

$$\underline{\mathbf{w}} = \underline{\mathbf{w}}_{\mathbf{k}} + \underline{\mathbf{B}}_{\mathbf{w}}\underline{\mathbf{w}} \tag{7-11}$$

where:

$$\underline{\dot{\mathbf{x}}}_{\mathbf{w}} = \mathbf{A}_{\mathbf{w}} \underline{\mathbf{x}}_{\mathbf{w}} \tag{7-12}$$

7.1.2 Design of State Feedback Controller

We wish to design a state feedback control system for this plant so that the plant state vector will remain near some equilibrium plant state vector $(\underline{\mathbf{x}}_p)_d$.

Since
$$A_p(\underline{x}_p)_d = 0$$
, (7-13)

we can write:

$$\underline{\dot{x}}_{p} = A_{p}\underline{x}_{p} + C(\underline{u}+\underline{v}) + D\underline{w}$$
 (7-14)

$$\underline{y}' = B_{p}\underline{x}'_{p} \tag{7-15}$$

where:

$$\underline{\mathbf{x}'_{p}} = \underline{\mathbf{x}}_{p} - (\underline{\mathbf{x}}_{p})_{d} \tag{7-16}$$

and

$$\underline{y}' = \underline{y} - B_p(\underline{x}_p)_d \tag{7-17}$$

Hence, we can assume without loss of generality that:

Since

$$C^{T}D = 0, \qquad (7-19)$$

none of the plant disturbance vector can be cancelled by the plant control vector. However, all of the plant control disturbance vector can be cancelled. Therefore, we let:

$$\underline{\mathbf{u}} = \underline{\mathbf{g}}(\underline{\mathbf{x}}_{\mathbf{p}}) - \underline{\mathbf{v}} \tag{7-20}$$

To simplify the design, we will limit the feedback structure to a linear, time-invariant function so that

$$\underline{\mathbf{u}} = -G\underline{\mathbf{x}}_{\mathbf{p}} - \underline{\mathbf{v}}$$
 (7-21)

where G is a controller gain matrix of dimension $c \times n$. Substituting equation (7-21) into equation (7-1) yields:

$$\frac{\dot{\mathbf{x}}}{\mathbf{p}} = \mathbf{A}_{\mathbf{c}} \mathbf{x}_{\mathbf{p}} + \mathbf{D}_{\mathbf{w}}. \tag{7-22}$$

where the controlled plant matrix may be expressed:

$$A_{c} = A_{p} - CG \tag{7-23}$$

Note that if we could choose G such that

$$A_{C} = -\frac{1}{T} I, \qquad (7-24)$$

where $I = identity matrix of the same dimensions as <math>A_c$,

then the present plant state vector would be
$$\underline{x}_p(t) = e^{-\frac{t}{T}} \underline{x}(0) + D \int_0^t e^{\frac{\tau - t}{T}} \underline{w}(\tau) d\tau \qquad (7-25)$$

where $\underline{x}_{D}(0)$ is the initial plant state vector. This would be a desirable choice for G since, under the assumption that T is small, only recent, large plant disturbances could cause the present plant state not to However, since c is less than n, there generally is no matrix G that will satisfy equation (7-24). Therefore we will choose G to render a measure of the difference between the two matrices in equation (7-24) as small as possible.

We could define the measure of the difference between these two matrices in the same way as for the measure of the difference between two vectors as $(trE^{T}_{c}E_{c})^{\frac{1}{2}}$ where:

$$\mathbf{E}_{\mathbf{c}} = \mathbf{A}_{\mathbf{c}} + \frac{1}{\mathbf{T}}\mathbf{I} \tag{7-26}$$

This yields the following solution.

$$G = C*(A_p + \frac{1}{T}I)$$
 (7-27)

(The derivation and analysis of this solution appear in Appendix C)

However, we wish to make $\mathbf{E}_{\mathbf{c}}$ small in the sense that for any \underline{x}_p , $\underline{F}_c\underline{x}_p$ is small compared with \underline{x}_p . Furthermore, for various physical reasons, some plant state variables or combinations of plant state variables may be more important to control than others. Consequently we will

choose G to minimize the following quantity:

$$\max_{\underline{z}\neq 0} \frac{|\underline{W}_{\underline{c}}\underline{E}_{\underline{c}}\underline{z}|}{|\underline{W}_{\underline{c}}\underline{z}|} \tag{7-28}$$

where the columns of W_c are linearly independent.

Since $\mathbf{W}_{\mathbf{C}}^{\mathbf{T}}\mathbf{W}_{\mathbf{C}}$ is nonsingular, we can write:

$$\frac{\max_{\underline{z} \neq 0} \frac{|\underline{w}_{\underline{c}}\underline{z}|}{|\underline{w}_{\underline{c}}\underline{z}|} = \max_{\underline{z} \neq 0} \frac{|\underline{E}_{\underline{c}}\underline{z}'|}{|\underline{z}'|}$$
(7-29)

where

$$\mathbf{E}_{\mathbf{C}} = \mathbf{W}_{\mathbf{C}} \mathbf{E}_{\mathbf{C}} \mathbf{W}_{\mathbf{C}}^* \tag{7-30}$$

$$\underline{z}' = W_{c}\underline{z} \tag{7-31}$$

Dividing the numerator and denominator of the right hand side by $|\underline{z}|$ and then squaring, we see that the above problem is equivalent to choosing G to minimize the quantity:

$$\max \underline{z}^{T}(E_{c}^{'})^{T}E_{c}^{'}\underline{z}$$

$$|\underline{z}|=1$$
(7-32)

Introducing the constraint,

$$\left|\underline{z}\right| = 1, \qquad (7-33)$$

by the Lagrange multiplier approach, a necessary condition for a critical value of \underline{z} is:

$$\frac{\partial}{\partial \underline{z}} \left[\underline{z}^{\mathrm{T}} (\underline{E}_{c})^{\mathrm{T}} \underline{E}_{c} \underline{z} - \lambda (\underline{z}^{\mathrm{T}} \underline{z} - 1) \right] = 0$$
 (7-34)

where $\frac{\partial}{\partial z}$ indicates a gradient with respect to \underline{z} .

Completing the differentiation indicated on the left hand side and dividing by 2 yields:

yields:

$$\lambda = \underline{z}^{\mathrm{T}} (\mathbf{E}_{\mathbf{c}})^{\mathrm{T}} \mathbf{E}_{\mathbf{c}} \underline{z} \tag{7-36}$$

From equations (7-35) and (7-36), we see that: $\max \underline{z}^{T}(E_{c}^{-})^{T}E_{c}^{-}z = \text{largest eigenvalue of } (E_{c}^{-})^{T}E_{c}^{-}$ |z|=1(7-37)

Hence, we wish to choose G such that Λ , the largest eigenvalue of $(E_c^{-1})^T E_c^{-1}$, is a minimum where:

$$E_{c} = W_{c}(A_{p} - CG + \frac{1}{T}I)W_{c}^{*}$$
 (7-38)

Since G is unconstrained, a necessary condition for the minimum value of Λ is

$$\frac{\partial \Lambda}{\partial G} = 0 \tag{7-39}$$

where $\frac{\partial}{\partial G}$ indicates the gradient with respect to G.

Furthermore, since $(\mathbf{E}_c^{-1})^{\mathrm{T}}\mathbf{E}_c^{-1}$ is symmetric, Λ can be $\Lambda = \lim_{k \to \infty} \frac{|e_{\kappa+1}|}{|e_{\kappa}|} \quad (7-40)$ approximated by the fact that:

where:

$$\underline{\mathbf{e}}_{k+1} = (\mathbf{E}_{\mathbf{c}})^{\mathrm{T}} \mathbf{E}_{\mathbf{c}} \underline{\mathbf{e}}_{k} \tag{7-41}$$

(Appendix D gives a numerical algorithm for generating the optimum controller gain matrix).

7.1.3 Design of State Estimator

The plant control given by equation (7-21) requires complete knowledge of the present plant state and control disturbance. Generally, these quantities are not completely known. However, they can be estimated from the known part of the past plant disturbances and the past plant measurements. Let \underline{x}_e be defined as the solution to the following vector differential equation:

$$\underline{\dot{\mathbf{x}}}_{e} = (\mathbf{A} - \mathbf{H}\mathbf{B})\underline{\mathbf{x}}_{e} + \left[\mathbf{D}^{T} | \mathbf{0} | \mathbf{0}\right]^{T}\underline{\mathbf{w}}_{k} + \mathbf{H}\underline{\mathbf{y}}$$
 (7-42)

where:

$$A = \begin{bmatrix} A_{c} & 0 & DB_{w} \\ O & A_{v} & 0 \\ O & O & A_{w} \end{bmatrix}$$
 (7-43)

H = constant estimator gain matrix

$$\mathbf{B} = \begin{bmatrix} \mathbf{B}_{\mathbf{p}} & \mathbf{0} & \mathbf{0} \end{bmatrix} \tag{7-44}$$

$$\underline{\mathbf{x}}_{e}(0) = \mathbf{B}^{T}(\mathbf{B}_{p}\mathbf{B}_{p}^{T})^{-1}\underline{\mathbf{y}}(0)$$
 (7-45)

Combining the assumptions about the system disturbances with equations (7-2) and (7-22) yields:

$$\underline{\dot{\mathbf{x}}} = \mathbf{A}\underline{\mathbf{x}} + \begin{bmatrix} \mathbf{D}^{\mathrm{T}} & \mathbf{0} & \mathbf{0} \end{bmatrix}^{\mathrm{T}}\underline{\mathbf{w}}_{\mathrm{K}} \tag{7-46}$$

$$\underline{y} = B\underline{x} \tag{7-47}$$

where:

$$\underline{\mathbf{x}} = \left[\underline{\mathbf{x}}_{\mathbf{p}} \mid \underline{\mathbf{x}}_{\mathbf{v}} \mid \underline{\mathbf{x}}_{\mathbf{w}}\right]^{\mathbf{T}} \tag{7-48}$$

Subtracting equation (7-46) from equation (7-42) and substituting equation (7-47) for \underline{y} , it is evident that:

$$\underline{\Delta \dot{\mathbf{x}}} = (\mathbf{A} - \mathbf{HB}) \ \underline{\Delta \mathbf{x}} \tag{7-49}$$

where:

$$\underline{\Delta x} = \underline{x}_{e} - \underline{\dot{x}} \tag{7-50}$$

Therefore, if we choose H to satisfy:

$$A-HB = -\frac{20}{T}I \tag{7-51}$$

then \underline{x}_e would be a good estimate of \underline{x} since the solution to equation (7-49) would be

$$\frac{-20}{T}$$
 (7-52)

However, since $m \le n$, there exists no H such that equation (7-51) is satisfied. Furthermore, the estimator gain matrix that minimizes $(\text{trE}_e^T \text{E}_e)^{\frac{1}{2}}$

where:
$$E_e = A - HB + \frac{20}{T} I$$
 (7-53)

yields estimates for the unknown part of the control and plant disturbances of zero at all times. (Sée Appendix E for a derivation and analysis of this solution).

Consequently, we will choose H to minimize the largest eigenvalue of the matrix, $(\mathbf{E_e}^{\prime})^T\mathbf{E_e}^{\prime}$

where:

$$\mathbf{E}_{\mathbf{e}} = \mathbf{W}_{\mathbf{e}} \mathbf{E}_{\mathbf{e}} \mathbf{W}_{\mathbf{e}}^* \tag{7-54}$$

(See Appendix D for a numerical algorithm for generating the optimum estimator gain matrix.) Figure 7-1 depicts the relationships between the plant, state controller and state estimator in the complete system.

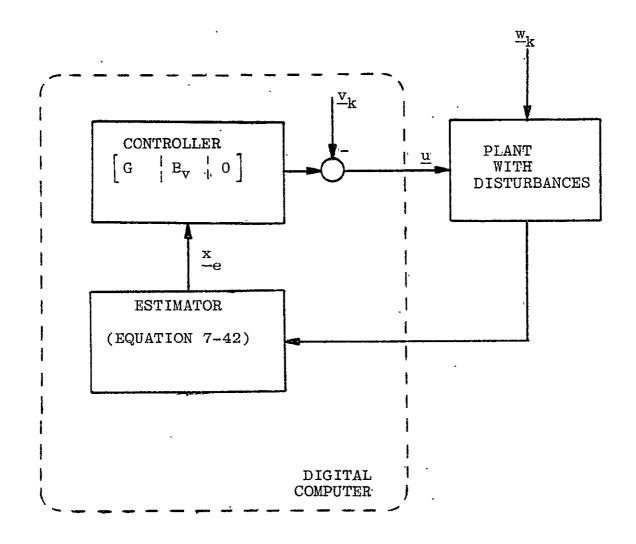


FIGURE 7-1
BLOCK DIAGRAM OF COMPLETE SYSTEM

7.1.4 System Design Parameters

Since the eigenvalues of equation (7-42) are approximately $-\frac{20}{T}$, the sampling frequency of the digital computer should be approximately $\frac{400}{T}$. The matrices C and B_p yield trade offs between control system performance and cost. The number of linearly independent actuators and sensors and, consequently, the system performance, increases as the ranks of these matrices increase. However, this better control system performance may not be worth the The scalar T also affords increased control system cost. a trade off between control system performance and cost. This trade off is more complex than those for C and B_n since smaller values of T not only increase control system cost but also may decrease control system per-A control system simulation and trial and formance. error will be necessary to choose the best values for C, B_{p} and T.

If a satisfactory control system cannot be found, it may be possible to significantly increase the performance and/or decrease the cost of the control system by making some relatively minor changes in the design of the uncontrolled plant. For instance, assume that

$$A_{p} = \left[f_{i,j}(\underline{\pi})\right] \tag{7-55}$$

where f $_{ij}$ $(\underline{\pi})$ is the ith row and jth column element of A and $\underline{\pi}$ is a vector of plant parameters which can be chosen to make control easier.

If we could render:

$$A_{p} = -\frac{1}{T}I \tag{7-56}$$

then G=0 and the control system would be optimal. However, since generally there will be no $\underline{\pi}$ such that these matrices are equal, we will render the difference between the two matrices of equation (7-56) as small as possible by choosing $\underline{\pi}$ to minimize the largest eigenvalue of $(E_p^-)^T E_p^-$ where:

$$E_{p}^{\prime} = W_{c} \left[f_{ij} \left(\underline{\pi} \right) \right] + \frac{1}{T} I W_{c}^{\prime *}$$
 (7-57)

7.2 APPLICATION TO SPACE BASE

A major problem in designing control systems for flexible spacecraft is the development of an accurate yet simple plant model. Because of the inherent difficulties of solving partial differential equations a finite element approach must be used. Space Base can be modeled as a number of rigid bodies connected in a tree configuration by either dissipative spring-hinges or electromagnetic torque actuators. The greater the number of rigid bodies used in the model, the better the accuracy of the model and hence the better the performance of the control system. However, if more rigid bodies are used than are necessary, then the order of the model and, consequently, the cost of the control system will be greater than necessary. It is conjectured that, for the control scheme of subsection 7.1, if the lowest resonant frequency of a physical structure is $\frac{20}{T}$ or higher, then that structure can be considered rigid.

Assuming that the control system is holding or very slowly changing the orientation of Space Base, the

equations of motion of the rigid body finite element model can be linearized and written in the form of equations (7-1) and (7-2) with the angular rate and position error of the most precisely pointed body and the relative angular rates and position of adjacent bodies as state variables.

7.2.1 Weighting of State Variables

There are two obvious reasons to weight the individual plant state variables when computing the optimum controller gain matrix. First, it makes no sense to add quantities of different physical dimensions such as angular rate and position. Second, it may be more important to control one section of Space Base than another. Consequently, if

$$\underline{\mathbf{x}}_{\mathbf{p}} = \left[\underline{\dot{\mathbf{e}}}^{\mathbf{T}} \mid \underline{\mathbf{e}}^{\mathbf{T}}\right]^{\mathbf{T}} \tag{7-58}$$

where the vector $\underline{\dot{\theta}}$ contains the angular rate plant state variables and the vector $\underline{\theta}$ contains the angular position plant state variables, then a logical choice for $\mathbb{W}_{\mathbf{C}}$ would be:

$$W_{C} = \begin{bmatrix} TW & O \\ \hline O & W \end{bmatrix}$$
 (7-59)

where the scalar, T, nondimensionalizes the angular rate plant state variables and W is a positive definite diagonal matrix which weights the relative importance of controlling the individual angular position plant state variables. For this choice of $W_{\rm C}$, we have:

$$W_{c}^{*} = (W_{c}^{T}W_{c})^{-1}W_{c}^{T} = \begin{bmatrix} \frac{1}{T}W^{-1} & 0 \\ 0 & W^{-1} \end{bmatrix}$$
 (7-60)

Furthermore, a better choice for the starting value of G in the algorithm of Appendix D might be:

$$K = (W_{c}C)^{*} \cdot W_{c}(A_{p} + \frac{1}{T}I)$$
 (7-61)

7.2.2 Aerodynamic Disturbance Torque

Assuming the earth's gravity gradient disturbance torque to be computed and thus known, the primary unknown disturbance torque acting on Space Base is aerodynamic. Since this torque is approximately sinusoidal with orbit frequency, ω_{O} , we can write:

$$\underline{\dot{\mathbf{v}}}_{\mathbf{u}} = \underline{\mathbf{a}} \cdot \cos \, \omega_{\mathbf{o}} \mathbf{t} + \underline{\mathbf{b}} \, \sin \, \omega_{\mathbf{o}} \mathbf{t} \tag{7-62}$$

where \underline{v}_u is the unknown part of the control disturbance torque and \underline{a} and \underline{b} are constant but unknown vectors. Differentiating \underline{v}_u twice with respect to time yields:

$$\begin{bmatrix} \underline{v}_{u} \\ \underline{v}_{u} \end{bmatrix} = \begin{bmatrix} 0 & | -\omega_{o}^{2} \mathbf{I} \\ ---| --- \end{bmatrix} \begin{bmatrix} \underline{v}_{u} \\ \underline{v}_{u} \end{bmatrix}$$

$$[7-63)$$

Accordingly,

$$\underline{\mathbf{x}}_{\mathbf{v}} = \begin{bmatrix} \underline{\mathbf{v}}_{\mathbf{u}}^{\mathbf{T}} & \underline{\mathbf{v}}_{\mathbf{u}}^{\mathbf{T}} \end{bmatrix}^{\mathbf{T}} \tag{7-64}$$

$$B_{V} = \begin{bmatrix} 0 & 1 \end{bmatrix} \tag{7-65}$$

$$A_{v} = \begin{bmatrix} 0 & -\omega_{0}^{2}I\\ I & 0 \end{bmatrix}$$
 (7-66)

Similarly,

$$\underline{\mathbf{x}}_{\mathbf{w}} = \begin{bmatrix} \mathbf{\dot{w}}_{\mathbf{u}}^{\mathbf{T}} & \mathbf{\dot{w}}_{\mathbf{u}}^{\mathbf{T}} \end{bmatrix}^{\mathbf{T}} \tag{7-67}$$

$$B_{w} = \begin{bmatrix} 0 & 1 \end{bmatrix} \tag{7-68}$$

$$A_{W} = \begin{bmatrix} 0 & -\omega_{0}^{2} I \\ --- & 0 \\ I & 0 \end{bmatrix}$$
 (7-69)

7.2.3 Weighting Coefficients For Disturbance State Variable Estimation Error

It is reasonable in computing the optimum estimator gain matrix to weight various combinations of the disturbance state variable estimation errors according to the magnitude and location of the jerk, acceleration and velocity they cause. Thus a logical choice for $W_{\rm e}$ is:

Wc T²W_cC Q (7-70) TWCC $T^2 w_c^D$ Q

For this choice of $\boldsymbol{W}_{\mbox{\scriptsize e}},$ we have

₩ *	==	* "c	0	0	0	0	
		0	1 (W _c C)*	. 0	0	0	
		0	0	$\frac{1}{T}(W_{c}^{C})^{*}$	0	0	(7-71)
		0	0	0	$\frac{1}{\mathrm{T}^2}(\mathrm{W_cD})*$	0	
		0	0	0	. 0	$\frac{1}{T}(W_{c}D)*$	

7.2.4 Known Input and Plant Disturbances
Assuming the use of rigid body momentum exchange
actuators, the known part of the input disturbance can
be divided into three components: gravity gradient,

$$\underline{\mathbf{v}}_{\mathbf{k}} = \underline{\mathbf{v}}_{\mathbf{g}} + \underline{\mathbf{v}}_{\mathbf{r}} + \underline{\mathbf{v}}_{\mathbf{d}}. \tag{7-72}$$

The known part of the plant disturbance is just gravity gradient.

actuator reaction and actuator desaturation as follows.

SECTION 8

8.0 STRUCTURAL ANALYSIS STUDY

The determination of flexibility body characteristics for a series of connected substructures is an important problem in the study of spacecraft dynamics. Assuming that the flexibility characteristics of each of the substructures comprising a vehicle system are known in terms of the free-free modes which are obtained from a discrete coordinate formulation of the individual substructures, a method (Reference 8-1) has been developed recently for combining the substructures by deriving the forces and torques—that exist at the connection points between contiguous bodies while satisfying the appropriate boundary conditions. It is the objective of this section to determine the validity of the above proposed method by considering a homogeneous beam as an example.

8.1 SUMMARY OF APPROACH

A homogeneous beam made of steel is considered as the example to investigate the validity of the method mentioned above. Initially, the beam is idealized to be composed of elastically interconnected discrete rigid bodies with no damping mechanism involved. The springs connecting the bodies are assumed to be capable of having both translational and rotational motion. The free-free modes of the beam are determined from the equations of motion of the discrete rigid bodies constituting the beam. Next, the beam is halved and

each half of the beam is modelled in a similar manner as the total beam. Hence, the free-free modes of each half of the beam can be determined. Then the two half-beams are connected by two connection points; and, by writing the forces and torques that exist at the connection points, the equations of motion of the connected beam are developed to obtain the free-free modes of the connected beam. This result is compared to the modes of the beam obtained previously.

8.2 TECHNICAL DISCUSSION

The beam is subdivided into 2n rigid bodies. The adjacent rigid bodies are connected by springs which are capable of both translational and rotational motion. Thus the idealized model of the beam, illustrated in Figure 8-1, is composed of elastically interconnected discrete rigid bodies with no damping mechanism involved. Figure 8-2 and Table 8-1 explain some of the nomenclature used in this Section.

It is assumed that the discrete bodies composing the beam undergo deformations so small that only terms involving the first-degree deformations need be retained in the analysis. Further, the beam is allowed unrestricted motion in response to any applied forces and torques. Before proceeding with the analyses, it is necessary to define the reference frame with respect to which all measurements are made. If an inertially fixed reference frame is chosen, the deformations relative to the frame may grow large if the beam

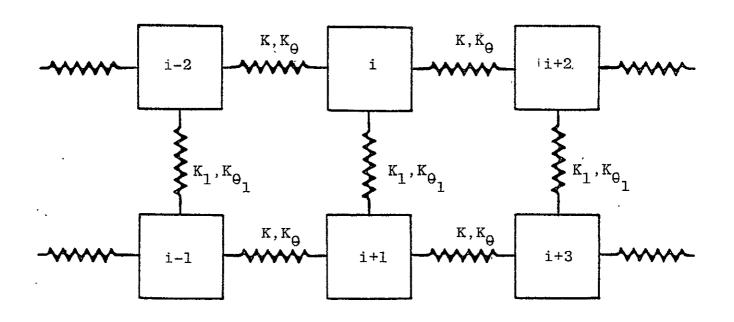


FIGURE 8-1 IDEALIZED MODEL OF THE BEAM

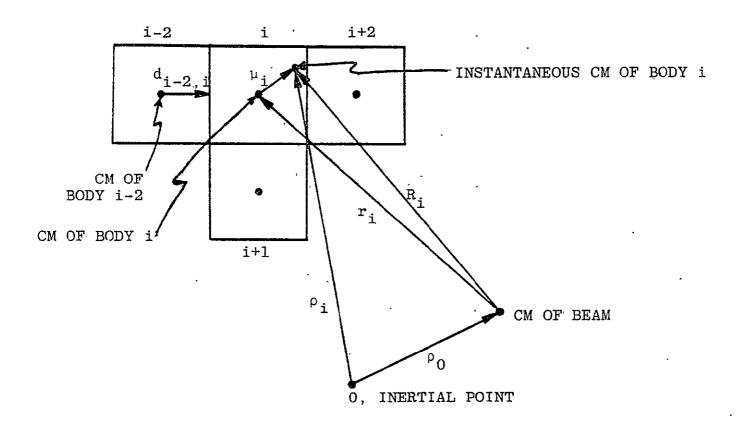


FIGURE 8-2 ILLUSTRATION OF SOME NOMENCLATURE

TABLE 8-1

NOMENCLATURE

ρ_{o}	vector from inertial point to CM of the beam
ρ _i	vector from inertial point to instantaneous (inst.) CM of body i
μ _i	vector from CM of body i to instantaneous (inst.) CM of body i
$\delta_{ extbf{i}}$	vector from inst. CM of body i to an elemental mass in body i
Υį	vector from CM of body i to the point of application of external force
ωo	inertial rate of the rigid body frame of the total beam
ω L	inertial rate of the rigid body frame of the half beam #1
ß.	angular rate of body i relative to the beam
$\epsilon_{\mathtt{i}}$	vector from the connection point to the CM of body i
^d ij	vector from the CM of body i to the interface point that lies on the line joining the CM's of bodies i and j.
F _{ij}	interface force between adjoining bodies i and j
$^{\mathrm{F}}$ c _{ij}	constraint force between adjoining bodies i and j
F _e _i	external force applied to body i
Hi	angular momentum of body i about the CM of the
	beam ·

TABLE 8-1 (CONT'D)

J _i	inertia of body i about its CM
K, K ₁	translational stiffness matrix between adjoining bodies
κ_{θ} , κ_{θ} 1	rotational stiffness matrix between adjoining bodies
2	refers to half-beam #1 for l=1 and to half beam #2 for l=2
mį	mass of body i
M _{ij}	interface torque at the adjoining bodies of i and j
$^{ ext{M}}\mathbf{c_{ij}}$	constraint torque at the adjoining bodies of i and j
$^{ m M}_{ m T}$	total mass of the beam
M _{T-L} .	mass of the half beam #1
n ´ ˙	the number of bodies constituting a half beam, or one-half of the number of bodies composing the beam
$Q_{0,Q_{\hat{2}}}$.	vector of the deformation coordinates
r _i	vector from the CM of the beam to the CM of body i
ℓ^r i	vector from the CM of half beam $\#\$ to the CM of body i in the half beam
$\mathbf{R_{i}}$	vector from the CM of the beam to inst. CM of body i
$^{\mathtt{T}}_{\mathtt{e}_{\mathtt{i}}}$	external torque applied to body i

undergoes an appreciable motion so that the analysis, using the assumption that the deformations are small, is However, if the reference frame is chosen not valid. such that it moves with the beam in a well-defined manner, then the deformations relative to this "floating" frame may be assumed to be small and hence the 'first order deformations only analysis can be carried out. The Tisserand frame (reference 8-2), with attractive properties for the purposes of this report, presents itself as such a floating reference frame. It is defined by the set of axes that moves in such a way as to set the internal angular momentum and the internal linear momentum always to zero. The latter requirement implies that the origin of the frame be located at the (rigid body) center of mass.

8.2.1 Preliminaries

The translational and rotational equation of motion 'for any discrete body i are given by:

$$F_{i} = m_{i}a_{i} \tag{8-1}$$

$$F_{i} = m_{i}a_{i}$$

$$T_{i} = H_{i}$$

$$(8-1)$$

where $\mathbf{F_{i}}$ and $\mathbf{T_{i}}$ are, respectively, the force and the torque exerted on body i, m_i is the mass of body i, a; the inertial acceleration of the center of mass (CM) of body i, and H, the angular momentum of body i referred to its CM. The small circle (o) indicates time differentiation with respect to inertial space.

The following equations are of use in the ensuing development of the equations of motion for the bodies of the beam. By the definition of the CM of the beam

$$2n$$

$$\Sigma \cdot m_{i} r_{i} = 0$$

$$i=1$$
(8-3)

and by the translational equation of motion of the beam

$$\begin{array}{ccc}
\mathbf{oo} & & & & & & \\
\rho_{O} & = & & & \frac{F}{M_{TP}} & & \\
\end{array} \tag{8-4}$$

where the total external force is given by

$$F_{e} = \sum_{i=1}^{2n} F_{e_{i}}$$
 (8-5)

and the total mass of the beam is given by

$$M_{T} = \sum_{i=1}^{2n} m_{i}$$
 (8-6)

The rotational equation of motion of the beam is given by:

$$J^* \overset{\mathbf{o}}{\omega}_0 = T_e \tag{8-7}$$

where the total external force is given by

$$T_{e} = \sum_{i=1}^{2n} T_{e_{i}}$$

$$(8-8)$$

and J^* is the inertia matrix about the CM of the beam. Since the beam is deformable, J^* is not a constant.

Equations (8-4) and (8-7) define the linear and angular accelerations of the Tisserand frame with respect to which all measurements are made.

8.2.2 Constraint Forces and Constraint Torques

Since the beam is modeled as elastically interconnected discrete rigid bodies, there exist constraint forces and constraint torques that are impressed on the discrete bodies due to the deformations of interconnected bodies. To derive the expressions for these forces and torques, the interconnection of a typical discrete body i with bodies i+2 and i+1 is illustrated respectively in Figures 8-3 and 8-4.

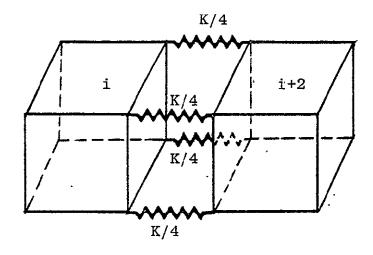


FIGURE 8-3 CONNECTION OF BODIES i AND i+2

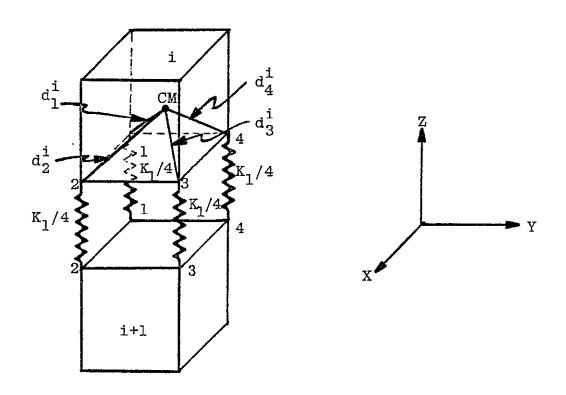


FIGURE 8-4 CONNECTION OF BODIES i AND i+1

Body i is connected to body i+2 (or i-2) via four springs, each with a translational spring constant $\frac{1}{4} K$ and a rotational spring constant $\frac{1}{4} K_{\Theta}$. Similarly, it is connected to body i+1 via four springs each with translational and rotational spring constants $\frac{1}{4} K_{\Theta}$ and $\frac{1}{4} K_{\Theta}$.

Let d_j^i denote the vector from the CM of body i to the vertex j of body i. Then the constraint force that is exerted on body i due to body i+1 can be written as

$$F_{c_{i,i+1}} = \int_{j=1}^{4} \frac{1}{2^{i}} K_{1} (\mu_{i+1-\mu_{i}}) + \int_{j=1}^{4} \frac{1}{4^{i}} K_{1} (\beta_{i+1} \times d_{j}^{i+1} - \beta_{i} \times d_{j}^{i})$$

$$(8-9)$$

Since

$$\begin{array}{ccc}
4 & & \\
\Sigma & d_j^i = 4d_{i,i+1}, \\
j=1 & & \end{array}$$

$$\sum_{j=1}^{4} d_{j}^{i+1} = 4d_{i+1,i}$$
(8-10)

$$d_{i,i+1} = -d_{i+1,i}$$

and with the skew symmetric matrix A defined by

where A_x , A_y , A_z are the x, y, z components of the vector A, equation (8-9) simplifies to

$$F_{c_{i,i+1}} = K_1(\mu_{i+1} - \mu_i) + K_1\tilde{d}_{i,i+1}(\beta_{i+1} + \beta_i)$$
 (8-12)

Similarly, the constraint force impressed on body i+1 due to body i is given by (8-13)

$$F_{c}$$
 = K_{1} ($\mu_{i}^{-}\mu_{i+1}$)+ $K_{1}^{d}d_{i+1,i}$ ($\beta_{i}^{+}\beta_{i+1}$)

In a similar manner, the constraint forces between bodies i and i+2 can be obtained to be

$$F_{c} = K(\mu - \mu) + K\tilde{d} (\beta + \beta)$$

$$i, i+2 \quad i+2 \quad i \quad i, i+2 \quad i+2 \quad i$$
(8-14)

$$F_{c_{i+2,i}} = K (\mu_{i} - \mu_{i+2}) + K d_{i+2,i} (\beta_{i} + \beta_{i+2})$$
(8-15)

It can be seen from the above equations that

The constraint torque that is experienced by body i due to body i+1 can be written as

$$M_{c_{i,i+1}} = \sum_{j=1}^{4} d_{j}^{i} \times \frac{1}{4} K_{1} (\mu_{i+1} - \mu_{i}) + \dots (8-16)$$

$$\sum_{j=1}^{4} d_{j}^{i} \times \frac{1}{4} K_{1} (\beta_{i+1} \times d_{j}^{i+1} - \beta_{i} \times d_{j}^{i})$$

With d_{oj}^i as the vector in the xy plane of the body if from the center of elasticity of the four springs connecting bodies i and i+1 (the center is the point of meeting of the vectors $d_{\underline{i},\underline{i+1}}$ and $d_{\underline{i+1},\underline{i}}$) to the jth spring, equation (8-16) using (8-10) can be written as

$$M_{c_{i,i+1}} = \tilde{d}_{i,i+1} K_{1} (\mu_{i+1} - \mu_{i}) + \sum_{j=1}^{4} \left[\frac{1}{4} (d_{i,i+1} + d_{oj}^{i}) \times K_{1} (d_{i,i+1} + d_{oj}^{i})^{-}\right] \beta_{i} - \sum_{j=1}^{4} \left[\frac{1}{4} (d_{i,i+1} + d_{oj}^{i}) \times K_{1} (d_{i+1,i} + d_{oj}^{i+1})^{-}\right] \beta_{i+1}$$

$$(8-17)$$

The coefficient of β_i in equation (8-17) the term in brackets, simplifies to (noting that $d_{oj}^i = d_{oj}^{i+1}$)

$$\tilde{d}_{i,i+1} K_1 \tilde{d}_{i,i+1} - \frac{1}{4} \sum_{j=1}^{4} \tilde{d}_{oj}^i \tilde{d}_{oj}^{i+1} K_1$$

The second term in the above expression may be recognized as the rotational spring constant between bodies i and i+1 and hence is replaced by $K_{\Theta_1^{-1}}$. Thus equation (8-17) can be written as

$$M_{c_{i,i+1}} = \tilde{d}_{i,i+1} K_{1} (\mu_{i+1} - \mu_{i}) + \\ \tilde{d}_{i,i+1} K_{1} \tilde{d}_{i,i+1} (\beta_{i+1} + \beta_{i}) + \\ K_{\theta_{1}} (\beta_{i+1} - \beta_{i})$$
(8-18)

Similarly, the constraint torque on body i+1 due to body i is given by

$$M_{c_{i+1,i}} = \tilde{d}_{i+1,i} K_{1} (\mu_{i} - \mu_{i+1}) + \\ \tilde{d}_{i+1,i} K_{1} \tilde{d}_{i+1,i} (\beta_{i} + \beta_{i+1}) + \\ K_{\theta_{1}} (\beta_{i} - \beta_{i+1})$$
(8-19)

In a similar way, the constraint torques between bodies i and i+2 may be obtained to be

$$M_{c_{i,i+2}} = \tilde{d}_{i,i+2} K (\mu_{i+2} - \mu_{i}) + \\ \tilde{d}_{i,i+2} K \tilde{d}_{i,i+2} (\beta_{i+2} + \beta_{i}) + \\ K_{\theta} (\beta_{i+2} - \beta_{i})$$
(8-20)

$$M_{c_{i+2,i}} = d_{i+2,i} K (\mu_{i} - \mu_{i+2}) + \frac{1}{d_{i+2,i}} K d_{i+2,i} (\beta_{i} + \beta_{i+2}) + \frac{1}{d_{i+2,i}} K d_{i+2,i} (\beta_{i} + \beta_{i+2,i}) + \frac{1}{d_{i+2,i}} K d_{i+2,i} (\beta_{i+2,i} + \beta_{i+2,i}) + \frac{1}{d_{i+2,i}} K d_{i+2,i} (\beta_{$$

8.2.3 Translational Equations of Motion for the Full Beam

The translational equation for a typical body i can be written, using equation (8-1) and recognizing that the constraint force between the adjacent bodies contributes to the total force impressed on body i, as

$$F_{e_{i}} + F_{c_{i,i-2}} + F_{c_{i,i+1}} + F_{c_{i,i+2}} = m_{i}^{oo}$$

$$i = 3.5, \dots, 2n-3$$
(8-22)

From Figure 8-2, it follows that

$$\rho = \rho + R_{i}$$

$$i \quad o \quad (8-23)$$

$$R_i = r_i + \mu_i$$
 (8-24)
 $i = 1, 2, ..., 2n$

Combining (8-23) and (8-24) and differentiating twice in the inertial frame results in

The terms appearing in the right-hand side of the above equation can be written in terms of body i rigid body coordinates:

$$r_i = \omega_0 \times r_i + \omega_0 \times \omega_0 \times r_i \approx \omega_0 \times r_i$$

$${\stackrel{\circ\circ}{\mu_i}}^{-\mu_i} + {\stackrel{\circ}{\mu_o}}^{x\mu_i} + 2 {\stackrel{\circ}{\mu_o}}^{x\mu_i} + {\stackrel{\circ}{\mu_o}}^{x\omega_o} {\stackrel{\circ}{x}}^{\mu_i} {\stackrel{\circ}{z}}^{\mu_i}$$

where the dot (•) indicates time differentiation in a reference frame located at the CM of body i. The approximation results due to the assumption that the deformations are small, which entails the deletion of nonlinear terms. Thus, with the above expressions and the equation (8-4), (8-25) becomes (writing the results in body i rigid body coordinates):

$$\stackrel{\circ o}{\rho_{i}} = \frac{F_{e}}{M_{rr}} + \stackrel{\circ}{\omega}_{O} \times r_{i} + \stackrel{\circ \circ}{\mu_{i}}$$
(8-26)

Substituting for ρ_i from (8-26) and for the constraint forces from section 8.2.2, the translational equation of motion for body i can be obtained as

Similarly, the translational equations of motion for the remaining bodies can be obtained. A summary of the translational equations is given in Appendix F.1.

8.2.4 Rotational Equations of Motion for the Full Beam

Using equation (8-2) and noting that the constraint torques, which include the effect of constraint forces between the adjacent bodies, contribute to the total torque applied to body i (again, a typical body in the top row of the beam model), the rotational equation of motion for body i can be written as

$$T_{e_{i}}^{+\gamma_{i}} x F_{e_{i}}^{+M} c_{i,i-2}^{+M} c_{i,i+1}^{+M} c_{i,i+2}^{-H} i$$
 (8-28)
 $i=3,5,...,2n-3$

The rate of change of the angular momentum of body i is given by

$$\begin{array}{ccc}
\bullet & & \bullet \\
H_{i} = & T_{i} & H_{i}
\end{array}$$
(8-29)

with

$$\dot{\mathbf{H}}_{\mathbf{i}} = \mathbf{J}_{\mathbf{i}} \mathbf{O} \mathbf{T}_{\mathbf{i}}^{\mathbf{t}} (\dot{\boldsymbol{\omega}}_{\mathbf{o}} + \dot{\boldsymbol{\beta}}_{\mathbf{i}}) + \mathbf{J}_{\mathbf{i}} \left[\mathbf{O} \mathbf{T}_{\mathbf{i}}^{\mathbf{t}} (\dot{\boldsymbol{\omega}}_{\mathbf{o}} + \dot{\boldsymbol{\beta}}_{\mathbf{i}}) \mathbf{x}_{\mathbf{o}} \mathbf{T}_{\mathbf{i}}^{\mathbf{t}} (\dot{\boldsymbol{\omega}}_{\mathbf{o}} + \dot{\boldsymbol{\beta}}_{\mathbf{i}}) \right]$$
(8-30)

where $_{0}^{T}$ is a fixed transformation from the rigid body coordinate frame of body i to that of the inertial (Tisserand) frame. Neglecting nonlinear terms in (8-30) and noting that the transformation matrix can be approximated by the identity matrix, equations (8-29) and (8-30) combine to yield

$$\begin{array}{ccc}
\mathbf{c} & & & & \\
\mathbf{H}_{\mathbf{i}} & & & & \\
\mathbf{i} & & & & \\
\end{array}$$
(8-31)

Substituting for the constraint torques from section 3.2, equations (8-28) and (8-31) with the following definitions.

$$K_{\psi} \stackrel{\stackrel{\triangle}{=} -\tilde{d}}{i, i \pm 2} \tilde{Kd}_{i, i \pm 2}$$
 (8-32)

$$K_{\psi_1} \stackrel{\triangle}{\stackrel{\sim}{=}} \tilde{d}_{i,i\pm 1} K\tilde{d}_{i,i\pm 1}$$
 (8-33)

for all i such that the subscripts are positive, yield $J_{\dot{\mathbf{1}}}\ddot{\beta}_{\dot{\mathbf{1}}}^{\phantom{\dot{\mathbf{1}}}}+(2K_{\Theta}+K_{\Theta})\dot{\beta}_{\dot{\mathbf{1}}}^{\phantom{\dot{\mathbf{1}}}}-K_{\Theta}}\beta_{\dot{\mathbf{1}}-2}^{\phantom{\dot{\mathbf{1}}}}-K_{\Theta}}\beta_{\dot{\mathbf{1}}+1}^{\phantom{\dot{\mathbf{1}}}}-K_{\Theta}}\beta_{\dot{\mathbf{1}}+2}$

$$^{+(2K_{\psi}+K_{\psi}}\underline{\textbf{i}})^{\beta}\underline{\textbf{i}}^{+K_{\psi}}}\underline{\textbf{i}}\underline{\textbf{i}}-2^{+K_{\psi}}\underline{\textbf{i}}\underline{\textbf{i}}+1^{+K_{\psi}}}^{\beta}\underline{\textbf{i}}+2$$

$$\tilde{d}_{i,i+1}^{K_1\mu_i-\tilde{d}_{i,i-2}^{K_{\mu_{i-2}}-\tilde{d}_{i,i+1}^{K_1}\mu_{i+1}-\tilde{d}_{i,i+2}^{K_{\mu_{i+2}}}}$$

$$= T_{e_{i}} + \gamma_{i} F_{e_{i}} - J_{i} \dot{\omega}_{o}$$

$$= 3, 5, \dots, 2n-3$$
(8-34)

The rotational equations for bodies $i=4,6,\ldots,2n-4$ can be written in a similar manner. To illustrate the nature of equations for the end bodies (i=1,2,2n-1,2n), the rotational equation of motion for body i is given:

$$J_{1}^{\bullet,\bullet}_{\beta_{1}} + (K_{\Theta} + K_{\Theta_{1}}) \beta_{1} - K_{\Theta_{1}} \beta_{2} - K_{\Theta} \beta_{3}$$

$$+ (K_{\psi} + K_{\psi_{1}}) \beta_{1} + K_{\psi_{1}} \dot{\beta}_{2} + K_{\psi} \beta_{3}$$

$$+ (\tilde{d}_{12} K_{1} + \tilde{d}_{13} K) \mu_{1} - \tilde{d}_{12} K_{1} \mu_{2} - \tilde{d}_{13} K \mu_{3}$$

$$= T_{e_{1}} + \gamma_{1} F_{e_{1}} - J_{1} \dot{\omega}_{0}$$

$$= T_{e_{1}} + \gamma_{1} F_{e_{1}} - J_{1} \dot{\omega}_{0}$$

The rotational equations for i=2, 2n-1 and 2n can be written in a similar manner. A summary of the rotational equations is given in Appendix F.2.

8.2.5 Matrix Equation of Motion for the Full Beam

In the equations of motion developed in the previous two sections, the right-hand sides (rhs) are functions of only external forces and torques, except seemingly for $\dot{\omega}_0$. The rate of change of the inertial rate of the rigid body frame of the beam, $\dot{\omega}_0$, may be defined as the product of the inverse of the inertia dyadic of the discrete bodies about the CM of the beam and the total external torque impressed on the beam; i.e.,

$$\dot{\omega}_{0} = J_{0}^{-1} T_{0}$$
 (8-36)

where:

$$J_{0} = \sum_{i=1}^{2n} (J_{i} - m_{i} r_{i} r_{i})$$
(8-37)

and
$$T_0 = \sum_{i=1}^{2n} T_{e_i} + \tilde{\gamma}_i F_{e_i}$$
 (8-38)

With the above definition (8-36), the rhs of the equations of motion is now only a function of external forces and torques.

The translational and rotational equations of motion of the discrete bodies constituting the beam may be combined into a single matrix equation to facilitate computations:

$$M_{O}\ddot{Q} + K_{O}Q = L_{O} \tag{8-39}$$

where M $_{\rm O}$ and K $_{\rm O}$ are, respectively, mass and stiffness matrices of the beam and are 12n x 12n, L $_{\rm O}$ is a 12n-column vector of external forces and torques, and Q is a 12n-column vector that characterizes the flexible beam deformations and is defined by

$$\mathbf{Q}^{\mathsf{t}} = \begin{bmatrix} \mathbf{p}^{\mathsf{t}} & \mathbf{\beta}^{\mathsf{t}} & \mathbf{p}^{\mathsf{t}} & \mathbf{\beta}^{\mathsf{t}} \\ 1 & 1 & 2 & 2 & \cdots & & 2n \end{bmatrix}$$

where $\mu_{\underline{i}}$'s and $\beta_{\underline{i}}$'s are 3-row vectors and the superscript t denotes the transpose of the matrix or vector.

The beam model that is used in the computer simulation consists of 20(n=10) identical bodies so that

$$m_{i} = m$$

$$J_{i} = J$$

for i=1,2,...,2n. Using the equations of motion developed in sections 8.2.3 and 8.2.4, the mass and stiffness matrices $\rm M_O$ and $\rm K_O$ can be defined as follows:

Mass Matrix Mo = mij

 m_{ii} : 3x3 matrix

O.: 3x3 null matrix

$$\mathbf{m_{ij}} = \begin{cases} \mathbf{m} & \text{i=j=1,3,....,4n-l} \\ \mathbf{J} & \text{i=j=2,4,....,4n} \\ \mathbf{o} & \text{i\neq j} \end{cases}$$

Stiffness Matrix $K_0 = [K_{ij}]$

K_{ij} : 3 x 3 matrix

0 : 3 x 3 null matrix

$$\mathbf{K}_{\mathbf{i}\mathbf{j}} = \begin{cases} \mathbf{K} + \mathbf{K}_{\mathbf{1}} & \mathbf{i} = \mathbf{j} = 1, 3, 4\mathbf{n} - 3, 4\mathbf{n} - 1 \\ \mathbf{K}_{\mathbf{0}} + \mathbf{K}_{\mathbf{0}} + \mathbf{K}_{\mathbf{\psi}} + \mathbf{K}_{\mathbf{\psi}} & \mathbf{i} = \mathbf{j} = 2, 4, 4\mathbf{n} - 2, 4\mathbf{n} \\ 2\mathbf{K} + \mathbf{K}_{\mathbf{1}} & \mathbf{i} = \mathbf{j} = 5, 7, \dots, 4\mathbf{n} - 5 \\ 2\mathbf{K}_{\mathbf{0}} + \mathbf{K}_{\mathbf{0}} + 2\mathbf{K}_{\mathbf{\psi}} + \mathbf{K}_{\mathbf{\psi}} & \mathbf{i} = \mathbf{j} = 6, 8, \dots, 4\mathbf{n} - 4 \end{cases}$$

$$\mathbf{K}_{\mathtt{i}\mathtt{j}} = \mathbf{K}_{\mathtt{j}\mathtt{i}}^{\mathtt{t}} = \left\{ \begin{array}{ll} -\mathbf{K} & (\mathtt{i},\mathtt{j}) = (1,5), (3,7), \dots, (4\mathrm{n}-5,4\mathrm{n}-1) \\ -\mathbf{K}_{\mathtt{1}} & (\mathtt{i},\mathtt{j}) = (1,3), (5,7), \dots, (4\mathrm{n}-3,4\mathrm{n}-1) \\ \mathbf{K}_{\psi} - \mathbf{K}_{\theta} & (\mathtt{i},\mathtt{j}) = (2,6), (4,8), \dots, (4\mathrm{n}-4,4\mathrm{n}) \\ \mathbf{K}_{\psi} - \mathbf{K}_{\theta} & (\mathtt{i},\mathtt{j}) = (2,4), (6,8), \dots, (4\mathrm{n}-2,4\mathrm{n}) \end{array} \right.$$

$$\mathbf{K}_{\mathbf{i}\mathbf{j}} = \mathbf{K}_{\mathbf{j}\mathbf{i}}^{\mathbf{t}} = \begin{cases} -\mathbf{K}_{\boldsymbol{\emptyset}} & (\mathbf{i},\mathbf{j}) = (1,6), (3,8), \dots, (4\mathbf{n}-5,4\mathbf{n}) \\ -\mathbf{K}_{\boldsymbol{\emptyset}} & (\mathbf{i},\mathbf{j}) = (1,4), (5,8), \dots, (4\mathbf{n}-3,4\mathbf{n}) \\ -\mathbf{K}_{\boldsymbol{\emptyset}} & (\mathbf{i},\mathbf{j}) = (2,5), (4,7), \dots, (4\mathbf{n}-4,4\mathbf{n}-1) \\ -\mathbf{K}_{\boldsymbol{\emptyset}} & (\mathbf{i},\mathbf{j}) = (2,3), (6,7), \dots, (4\mathbf{n}-2,4\mathbf{n}-1) \\ -\mathbf{K}_{\boldsymbol{\emptyset}} & (\mathbf{i},\mathbf{j}) = (5,6), (9,10), \dots, (4\mathbf{n}-7,4\mathbf{n}-6) \\ +\mathbf{K}_{\boldsymbol{\emptyset}} & (\mathbf{i},\mathbf{j}) = (7,8), (11,12), \dots, (4\mathbf{n}-5,4\mathbf{n}-4) \end{cases}$$

$$K_{ij} = K_{ji}^{t} = \begin{cases} -K_{\emptyset} & -K_{\emptyset}_{1} \\ -K_{\emptyset} & +K_{\emptyset}_{1} \\ K_{\emptyset} & -K_{\emptyset}_{1} \\ K_{\emptyset} & +K_{\emptyset}_{1} \end{cases}$$

$$(i,j) = (3,4)$$

$$(i,j) = (4n-3,4n-2)$$

$$(i,j) = (4n-1,4n)$$

 $K_{ij} = 0$ otherwise.

The following definitions have been used in the above characterization of the matrix $\mathbf{K}_{\mathbf{O}}\colon$

$$K_{\emptyset_{1}} \stackrel{\Delta}{=} \tilde{d}_{i,i+1} \quad K_{1}$$

$$K_{\emptyset} \stackrel{\Delta}{=} \tilde{d}_{i,i+2} K$$

$$K_{\psi_{1}} \stackrel{\Delta}{=} K_{\emptyset_{1}} \tilde{d}_{i,i+1}$$

$$K_{\psi} \stackrel{\Delta}{=} K_{\emptyset} \tilde{d}_{i,i+2}$$

Also note that

$$d_{ij} = -d_{ji}$$

and

$$d_{i,i+2} = -d_{i,i-2}$$

8.2.6 Split Beam - Interface Forces and Torques The beam is divided into two halves so that each half of the beam may be modeled to be composed of n(=10)elastically interconnected discrete rigid bodies. two halves of the beam are put together, as shown in Figure 8-5, by connecting the discrete bodies n-1 and n+1 and the bodies n and n+2. The beam thus connected is referred to as the 'split beam'. Since the two halves are modeled in a manner similar to that of the full beam, the free-free modes of the half-beams can be determined in a similar way as the full beam. free-free modes of the split-beam can be obtained from the free-free modes of the half-beams and the forces and torques acting at the connection points of the half-For computational simplicity, the above two steps can be combined to accomplish the same goal; namely, obtaining the free-free modes of the split-beam from the equations of motion of the 2n discrete bodies that compose the split-beam, keeping in mind that it is the interface forces and torques, not the constraint forces and torques, that act at connection points.

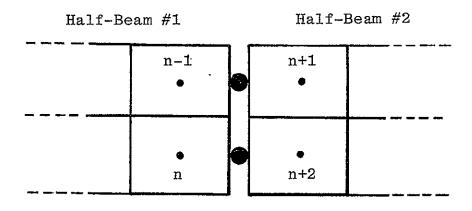


FIGURE 8-5 CONNECTION OF THE HALF-BEAMS

The equations of motion for the discrete bodies not involved in connections can be derived in an identical manner as for those of the full-beam. In order to derive the equations of motion for the bodies involved in the connections of the half-beams, it is first necessary to determine the interface forces and torques acting at each connection point.

The interface force at the connection point between bodies n and n+2 is determined by writing the translational equations of the bodies n and n+2:

$$F_{e_n} + F_{c_{n,n-1}} + F_{c_{n,n-2}} + F_{n,n+2} = m\rho_n$$
 (8-40)

$$F_{e_{n+2}} + F_{c_{n+2,n+1}} + F_{c_{n+2,n+4}} + F_{n+2,n} = m \rho_{n+2}$$
 (8-41)

where F_{ij} denotes the interface force at the connection point between bodies i and j. The bodies n and n+2 are connected such that they move as a rigid body so that $F_{n,n+2} = F_{n+2,n}$. Hence, the translational equation for this composite body can be written as

$$F_{e_n}^{+F}e_{n+2}^{+F}e_{n,n-1}^{+F}e_{n,n-2}^{+F}e_{n+2,n+1}^{+F}e_{n+2,n+4}^{+F}=2m \stackrel{oo}{\rho}_{n,n+2}$$

(8-42)

where $\rho_{n,n+2}$ is the vector from the inertial point to the connection point. Further,

$$\rho_{n} = \rho + \epsilon_{n}$$

$$(8-43)$$

$$\rho_{n+2} = \rho_{n,n+2} + \epsilon_{n+2} \tag{8-44}$$

From equations (8-40), (8-42) and (8-43), and noting that (neglecting nonlinear terms)

$$\varepsilon_{n}^{\circ \circ} = (\omega_{\circ 1}^{\circ} + \beta_{n}^{\circ}) \times \varepsilon_{n}^{\circ}$$

where ω_{01} is the inertial rate of the rigid body frame of the half-beam #1, the interface force can be solved

$$F_{n,n+2} = -m\tilde{\epsilon}_{n}\tilde{\beta}_{n} - m\tilde{\epsilon}_{n}\tilde{\omega}_{01}^{-\frac{1}{2}} \begin{cases} F_{c_{n+2,n+4}} + F_{c_{n+2,n+1}} \\ F_{c_{n+2,n+4}} - F_{c_{n+2,n-2}} \end{cases} + \frac{1}{2} (F_{e_{n+2}} - F_{e_{n}})$$

$$(8-45)$$

Using equations (8.41), (8-42) and (8-44),

$$F_{n+2,n} = -m\tilde{\epsilon}_{n+2}\dot{\beta}_{n+2} + \frac{1}{2} \left\{ F_{c_{n,n-2}} + F_{c_{n,n-1}} + F_{c_{n+2,n+1}} + F_{c_{n+2,n+4}} \right\}$$

$$-m\tilde{\epsilon}_{n+2}\dot{\omega}_{o2} + \frac{1}{2} (F_{e_n} - F_{e_{n+2}})$$
 (8-46)

where $\omega_{\rm O2}$ is the inertial rate of the rigid body frame of half beam #2.

Since the two halves of the beam have the same inertial rate; -i.e.,

rate; -i.e.,

$$\dot{\omega}_{o1} + \dot{\beta}_{n} = \dot{\omega}_{o2} + \dot{\beta}_{n+2}$$
(8-47)

and

 $\varepsilon_n = -\varepsilon_{n+2}$, it follows from (8-45) and (8-46) that

$$F_{n,n+2} = -F_{n+2,n}$$
 (8-48)

which is as expected and says that there is no net force acting at the connection point when the split-beam is viewed as a whole.

Similarly, from the translation equations of bodies n-l and n+l, the interface force at the connection point of these bodies can be obtained to be

$$F_{n-1,n+1} = -m\tilde{\epsilon}_{n-1} \tilde{\beta}_{n-1} + \frac{1}{2} \left[F_{c_{n+1,n+2}} + F_{c_{n+1,n+3}} - F_{c_{n-1,n}} - F_{c_{n-1,n}} + \frac{1}{2} F_{c_{n+1,n+2}} \right]$$

$$-m\tilde{\epsilon}_{n-1} \tilde{\omega}_{o1} + \frac{1}{2} F_{c_{n+1}} - F_{c_{n-1}}$$
(8-49)

$$F_{n+1,n-1} = -m\tilde{\epsilon}_{n+1} \quad \mathring{\beta}_{n+1} + \frac{1}{2} \left[F_{c_{n-1,n-3}} + F_{c_{n-1,n}} -F_{c_{n+1,n+2}} -F_{c_{n+1,n+3}} \right] + \frac{1}{2} \left[F_{e_{n-1}} - F_{e_{n+1}} \right]$$

$$-m\tilde{\epsilon}_{n+1} \quad \mathring{\omega}_{n+1} \quad \mathring{\omega$$

and again noting that
$$\epsilon_{n-1} = -\epsilon_{n+1}$$
 and
$$\dot{\omega}_{o1} + \dot{\beta}_{n-1} = \dot{\omega}_{o2} + \dot{\beta}_{n+1}$$
 (8-51)

it is seen that

$$F_{n-1,n+1} = -F_{n+1,n-1}$$
 (8-52)

which is as expected.

The interface torque at the connection point between bodies n and n+2 is determined from the rotational equations of the bodies n and n+2:

$$T_{e_{n}} + 1 \tilde{\gamma}_{n} F_{e_{n}} + M_{c_{n,n+2}} + M_{c_{n,n-1}} + \tilde{d}_{n,n+2} F_{n,n+2} + M_{n,n+2} = \tilde{H}_{n}$$

$$T_{e_{n+2}} + 2 \tilde{\gamma}_{n+2} F_{e_{n+2}} + M_{c_{n+2,n+4}} + \tilde{d}_{n+2,n+1} + \tilde{d}_{n+2,n} F_{n+2,n} + \tilde{d}_{n+2,n} + \tilde{d}_{n+2,n}$$

Since the net torque at the connection point should be zero it follows that $M_{n,n+2} = -M_{n+2,n}$ (8-55)

Using (8-55) in (8-53) and (8-54) results in the interface torque

$$M_{n,n+2} = \frac{1}{2} \left[M_{c_{n+2,n+4}}^{+} + M_{c_{n+2,n+1}}^{+} - M_{c_{n,n-1}}^{-} - M_{c_{n,n-2}}^{-} - \frac{1}{2} T_{e_{n,n+2}}^{+} \right]$$
(8-56)

where T denotes the total external torque on bodies ${\rm e}_{n,\,n+2}$ n and n+2. Use is made of the facts that

$$F_{n,n+2} = -F_{n+2,n}$$
 (equation(8-48))
 $d_{n,n+2} = -d_{n+2,n}$

that the inertial rates of the bodies n and n+2 are the same .

$$\beta_n + \omega_{o1} = \beta_{n+2} + \omega_{o2}$$

and that the inertia about the CM of bodies n and n+2 is the same; i.e.,

$$J_{n} = J_{n+2}$$

Similarly, the interface torque at the connection point of bodies n-l and n+l may be determined to be

$$M_{n-1,n+1} = \frac{1}{2} \left[M_{c_{n+1,n+3}}^{+M} c_{n+1,n+2}^{-M} c_{n-1,n}^{-M} c_{n-1,n-3} \right] - \frac{1}{2} T_{e_{n-1,n+1}}^{-1}$$
(8-57)

where $T_{e_n-1,n+1}$ is the total external torque on bodies n-1 and n+1. Again, the interface torques are such that

$$M_{n-1,n+1} = -M_{n+1,n-1}$$
 (8-58)

8.2.7 Translational Equations For Bodies of the Split-Beam The translational equation for a body i which is not involved in connections may be written, as before, as

$$F_{e_{i}}^{+F_{c_{i,i-2}}} + F_{c_{i,i+1}}^{+F_{c_{i,i+2}}} = m_{i}^{oo}$$

$$i \in I_{1,I_{3}}$$
 (8-59)

$$F_{e_{i}}^{+F}c_{i,i-2}^{+F}c_{i,i-1}^{+F}c_{i,i+2}^{=m_{i}} = m_{i}^{oc}$$

$$i \in I_{2}, I_{4}$$
(8-60)

where the indicator functions are defined as

$$I_{1} = \{3,5,\ldots,n-3\}$$

$$I_{2} = \{4,6,\ldots,n-2\}$$

$$I_{3} = \{n+3,n+5,\ldots,2n-3\}$$

$$I_{4} = \{n+4,n+6,\ldots,2n-2\}$$

From Figure 8-2, it follows that

$$\rho_{i} = \rho_{O} + r_{i} + \mu_{i} \tag{8-61}$$

where the preceding subscript ℓ can be either 1 or 2 which, respectively, refer to half-beams #1 or 2; and ℓ^r is the vector from the CM of half-beam # ℓ to the CM of body i in that half-beam. Differentiating (8-61) twice and retaining only the first-order terms in deformations, results in

For half-beam #1

$${\stackrel{\circ}{{}_{\ell}}} {\stackrel{\circ}{{}_{0}}} = {\stackrel{\mathcal{L}^{F}e}{{}_{M_{T_{0}}}}}$$

$$(8-63)$$

where $_{\ell}^{F}$ e and $_{T}^{\ell}$ are, respectively, the total external force applied on the half-beam # ℓ and the total mass of the half-beam # ℓ . Substituting equations (8-62) and

(8-63) in (8-59) and (8-60) results in the translational equations of motion for bodies not involved in connections. For example, the translational equation for bodies which are in the top row of the split-beam and are not involved in connection of the half-beams is given by

$$\begin{split} \mathbf{m_{i}}\ddot{\mu}_{i} + & (2\mathbf{K} + \mathbf{K_{1}})\mu_{i} - \mathbf{K}\mu_{i-2} - \mathbf{K_{1}}\mu_{i+1} - \mathbf{K}\mu_{i+2} - \mathbf{K_{1}}\ddot{\mathbf{d}}_{i,i+1}\beta_{i} \\ & + \mathbf{K}\ddot{\mathbf{d}}_{i-2,i}\beta_{i-2} + \mathbf{K_{1}}\ddot{\mathbf{d}}_{i+1,i}\beta_{i+1} + \mathbf{K}\ddot{\mathbf{d}}_{i+2,i}\beta_{i+2} \\ & = \mathbf{F_{e_{i}}} - \frac{\mathbf{m_{i}}}{\mathbf{M_{T_{k}}}} \mathbf{F_{e}} + \mathbf{m_{i}} \mathbf{k}\ddot{\mathbf{r}}_{i} \dot{\mathbf{o}}_{ok} \\ & \qquad \qquad & \mathbf{k} = 1 \text{ for } i \in \mathbf{I_{1}} \\ & \mathbf{k} = 2 \text{ for } i \in \mathbf{I_{3}} \end{split}$$

Comparing (8-64) with (8-27) it can be seen that in general, the left-hand sides of the translational equations of the bodies (not involved in connections) of the split-beam are identical to that of the corresponding bodies of the full-beam. Further, it may be noted that the right-hand side (rhs) of (8-64) is an appropriately modified form of the rhs of (8-27).

The translational equations of motion for the four bodies involved in the connection of the half-beams are as follows:

$$m\ddot{\mu}_{n-1} - F_{c_{n-1, n}} - F_{c_{n-1, n-3}} - F_{n-1, n+1} = F_{c_{n-1}} - \frac{m_{n-1}}{M_{T_1}} \cdot 1^{F_{c}} + \frac{m_{n-1}}{M_{T_1}} \cdot 1^{\tilde{r}} = \frac{m_{n-1}}{M$$

$$m\ddot{\mu}_{n}^{-F}c_{n,n-1}^{-F}c_{n,n-2}^{-F}c_{n,n+2} = F_{e_{n}}^{-\frac{m_{n}}{M_{T_{1}}}} \mathbf{1}^{F}e$$

$$+ m_{n} \mathbf{1}^{F}n \dot{\omega}_{O1}$$
(8-65)

Substituting into (8-65) for the constraint forces from section 8.2.2 and for the interface forces from section 8.2.6 results in the translational equations of motion for the bodies involved in connections. These equations are given in Appendix F.3.

8.2.8 Rotational Equations For Bodies of the Split-Beam

The rotational equation of motion for the bodies not involved in connections of the half-beams may be written, as in Section 8.2.4, as

$$T_{e_{i}}^{+} \ell^{\gamma_{i}} X_{e_{i}}^{+} + M_{c_{i,i-2}}^{+} + M_{c_{i,i+1}}^{+} + M_{c_{i,i+2}}^{+} = \tilde{H}_{i}^{*}$$
 (8-66)
 $\ell = 1 \text{ for } i \in I_{1}$
 $\ell = 2 \text{ for } i \in I_{3}$

$$T_{e_{i}}^{+} \ell^{\gamma_{i}} x F_{ei}^{+} C_{i,i-2}^{+} C_{i,i-1}^{+} C_{i,i+2}^{+} = H_{i}^{\bullet}$$

$$\ell = 1 \text{ for } i \in I_{2}$$

$$\ell = 2 \text{ for } i \in I_{A}$$

As in Section 8.2.4, the rate of change of the angular momentum of body i may be obtained to be

$$\overset{\circ}{H}_{i} = \begin{cases}
J_{i} & (\dot{\omega}_{01} + \ddot{\beta}_{i}) & i \in I_{1}, I_{2} \\
J_{i} & (\dot{\omega}_{02} + \ddot{\beta}_{i}) & i \in I_{3}, I_{4}
\end{cases}$$
(8-68)

Substituting for constraint torques from Section 8.2.2, equations (8-66) and (8-67) with the aid of (8-68) yield the rotational equations of motion for bodies not involved in connection. For example, for bodies in the top row of the beam, $J_{\bf i}$ ${}^{\dot{\beta}}_{\bf i}$ + $({}^{2}{}^{K}_{\theta}$ + ${}^{K}_{\theta}$, 3 ${}^{\dot{\beta}}_{\bf i}$ - ${}^{K}_{\theta}$, 3 ${}^{\dot{\beta}}_{\bf i}$ + $({}^{2}{}^{K}_{\theta}$, 4 , 3 ${}^{\dot{\beta}}_{\bf i}$ - 4 , 3 , 3 , 4

$$+(2K_{\psi} + K_{\psi_{1}}) \beta_{i} + K_{\psi} \beta_{i-2} + K_{\psi_{1}} \beta_{i+1} + K_{\psi} \beta_{i+2}$$

$$+K_{\phi_{1}} \mu_{i} + K_{\phi} \mu_{i-2} - K_{\phi_{1}} \mu_{i+1} - K_{\phi} \mu_{i+2}$$

$$= T_{e_{i}} + \tilde{\gamma}_{i} F_{e_{i}} - J_{i} \dot{\omega}_{o} \qquad (8-69)$$

$$\ell = 1 \text{ for } i \in I_{1}$$

$$\ell = 2 \text{ for } i \in I_{2}$$

Comparing (8-69) with (8-34), it is again seen that the left-hand sides of the rotational equations of the bodies (not involved in connections) of the split-beam are identical to that of the corresponding bodies of the full-beam. Further, the right-hand side of (8-69) is an appropriately modified form of the rhs of (8-34).

The rotational equations for bodies involved in the connection of half-beams may be written as

$$T_{e_{n-1}}^{+1} + \tilde{\gamma}_{n-1}^{+1} = I_{n-1}^{+M} c_{n-1,n}^{+M} c_{n-1,n-3}^{+d} - I_{n-1,n+1}^{+1} - I_{n-1,n+1}^{+1}$$

$$+ M_{n-1,n+1}^{+1} = J_{n-1} (\tilde{\omega}_{01}^{+} + \tilde{\beta}_{n-1}^{+1}) \qquad (8-70)$$

$$T_{e_{n+2}}^{+2} + 2\tilde{\gamma}_{n+2}^{+1} = I_{n+2}^{+M} c_{n+2,n+1}^{+M} + C_{n+2,n+4}^{+d} + \tilde{\alpha}_{n+2,n}^{+1} = I_{n+2,n}^{+1} + I_{n+2,n}^{+1} = I_{n+2}^{+1} + I_{n+2,n}^{+1} = I_{n+2}^{+1} + I_{n+2,n}^{+1} + I_{n+2,n}^{+1} = I_{n+2}^{+1} + I_{n+2,n}^{+1} + I_{n+2,n}^{$$

The rotational equations for bodies n+1 and n would be identical, respectively, to (8-70) and (8-71) because (i) The expressions for the interface torques have been derived using the rotational equations of bodies n-1 and n+1 and bodies n and n+2, (ii) The inertial rate of the two halves of the beam is the same and hence for the bodies in connection,

$$\dot{\omega}_{01} + \dot{\beta}_{n-1} = \dot{\omega}_{02} + \dot{\beta}_{n+1}$$
 (8-72)

$$\dot{\omega}_{O1} + \dot{\beta}_{D} = \dot{\omega}_{O2} + \dot{\beta}_{D+2} \tag{8-73}$$

If $\dot{\omega}_{ol} \neq \dot{\omega}_{o2}$, then (8-72) and (8-73) may be utilized as the rotational equations of bodies n + 1 and n, respectively. Substituting for the constraint and interface forces and torques from sections 8.2.2 and 8.2.6 into (8-70) and (8-71) results in the rotational equations of motion for bodies n-l and n+2. These equations are given in Appendix F.4.

Matrix Equation of Motion for the Split-Beam 8.2.9 If the inertial rates of the rigid body frames of the two half-beams are assumed to be equal, then these inertial rates must equal the inertial rate of the rigid body frame of the original beam. Hence, it is seen again that the rhs of the equations of motion developed in the previous two sections are functions of only external forces and torques.

> For the beam under consideration, $J_{o1} = J_{o2}$ and the inertial rates of the half-beams are equal; viz, ω_{ol} = $\dot{\omega}_{02}$. In such a case (8-72) and (8-73) cannot be used as the rotational equations of bodies n and n+1. Moreover, these equations imply that

$$\beta_{n+1} = \beta_{n-1}$$
 (8-74)
 $\beta_n = \beta_{n+2}$ (8-75)

$$\beta_{n} = \beta_{n+2} \tag{8-75}$$

Thus, β_n and β_{n+1} may be eliminated from the equations of motion. The resultant translational and rotational equations of motion of the bodies composing the splitbeam may be combined into the matrix equation

$$^{"}_{2}^{Q}_{2} + ^{K}_{2}^{Q}_{2} = ^{L}_{2}$$
 (8-76)

where ${\rm M}_2$ and ${\rm K}_2$ are the mass and stiffness matrices, respectively, of the split-beam and are (12n-6) x (12n-6). L₂ is a (12n-6) column vector of external forces and torques; and ${\rm Q}_2$ is a (12n-6) column vector that characterizes the flexible beam deformations (excluding the angular deformation of bodies n and n+1).

$$Q_{2}^{t} = \begin{bmatrix} \mu_{1}^{t} & \beta_{1}^{t} & \mu_{2}^{t} & \beta_{2}^{t} & \dots, \mu_{n-1}^{t} & \beta_{n-1}^{t} & \mu_{n}^{t} & \mu_{n+1}^{t} & \mu_{n+2}^{t} & \beta_{n+2}^{t} & \dots, \mu_{2n}^{t} & \beta_{2n}^{t} \end{bmatrix}$$

and is defined by

Let K_2' be the 12n x 12n stiffness matrix of the split-beam that can be obtained from the equations of motion of the bodies of the split-beam.

Since the left-hand sides of the equations of motion of the bodies which are not involved in the connection of the half-beams are identical to that of the corresponding bodies of the full beam, the rows of the ${\tt K}_2^{\ \ \ }$ matrix corresponding to the bodies not involved in connections would be identical to the corresponding rows of the stiffness matrix of the full beam, K_0 . So, let K_0' be the $12n \times 12n \text{ matrix } K_0$, but with rows 2n-3, 2n-2,...,2n+4which correspond to the equations of motion of the bodies in connection, set to zero. These rows are defined by the elements of a $12n \times 12n$ matrix, K_3 , which has all zero entries for rows $1,2,\ldots,2n-4,2n+5,2n+6,\ldots,4n$ which correspond to the equations of motion of bodies not involved in connections and for which the remaining rows are defined by the equations of motion of the bodies in However, the entries in rows 2n and 2n+2 connections.

are all equal to zero due to the rotational equations ((8-72) and (8-73)) of the bodies 2n and 2n+2. Once the 12nx12n matrix $K_2' = K_0' + \overline{K_3}$ is formed, the rows and columns corresponding to β_n and β_{n+1} have to be eliminated keeping in mind that $\beta_n = \beta_{n+2}$ and $\beta_{n+1} = \beta_{n+1}$ (for the case $\omega_{ol} = \omega_{o2}$). This is accomplished by adding column 2n to column 2n+4 and column 2n+2 to column 2n-2 and then deleting the columns and rows 2n and 2n+2, thus resulting in a (12n-6) x (12n-6) matrix which defines K_2 .

The (12n-6) x (12n-6) mass matrix is obtained from the equations of motion developed in sections 8.2.7 8.2.8 and noting the fact that $\beta_n=\beta_{n+2}$ and $\beta_{n+1}=\beta_{n-1}$ which helps eliminate β_n and β_{n+1} and results in the following:

$$\underline{\text{Mass Matrix}} \ \text{M}_2 = \left[\text{m}_{i,j} \right] \tag{12n-6} \times (12n-6) \text{ matrix}$$

 m_{ij} : 3x3 matrix 0 : 3x3 null matrix

$$\mathbf{m}_{i,j} = \begin{cases} & \mathbf{m}_{i=j=1,3,\ldots,4n-3} \\ & \mathbf{j}_{j=2,4,\ldots,2n-4,2n+4,2n+6,\ldots,4n-2} \\ & \mathbf{j}_{j=2n-2,2n+2} \\ & \mathbf{m}_{i=j=2n} \\ & \mathbf{m}_{i=j=2n-2,2n-2} \\ &$$

8.2.10 Determination of the Vibration Frequencies and Mode Shapes The equations of motion for the beam being considered can be written, as pointed out earlier, as:

$$MQ + KQ = L (8-77)$$

To determine the free-free modes of the system represented by (8-77), the external forces and torques on the rhs of (8-77) is set to zero. Thus, (8-77) may be written as:

as:

$$Q + RQ = 0$$
 (8-78)
where
 $R = M^{-1}K$ (8-79)

$$R = M^{-1}K (8-79)$$

The eigenvalues, which will be real and positive if M and K are mass and stiffness matrices of a stable structural system, of the matrix R represent the square of the (natural) frequencies (in radians) of the modes of vibration which are possible in the system. The eigenvectors of the matrix R corresponding to the eigenvalues computed, characterize the mode shape of the vibration. Thus, if λ_i is an eigenvalue of R and X_i is the eigenvector corresponding to λ_j , then $\sqrt{\lambda_i}/2\pi$ is a natural frequency of the system and the components of the vector X_i describe the mode shape of the vibration.

8.2.11 Stiffness Matrices et al

For simulation purposes, a 20'x2'x4' homogeneous beam made of steel is considered. The beam is modelled by the twenty 2 ft. cubes. For the material being considered, the modulus of elasticity, the modulus of rigidity and the density are, respectively, given by

$$E = 29x10^6 \text{ psi}$$

 $G = 11.5x10^6 \text{ psi}$
 $\rho = 0.283 \text{ lbs/in}^3$

With the coordinate system as defined in Figure 8-6, the following may be defined:

the axial spring constant
$$K_y = \frac{bc}{a} E$$

the shear spring constant $K_x = K_z = \frac{5}{6} \frac{bc}{a} G$

the bending spring
$$\begin{cases} K_{\theta_x} = \frac{b^3c}{12a} E \\ K_{\theta_z} = \frac{bc^3}{12a} E \end{cases}$$

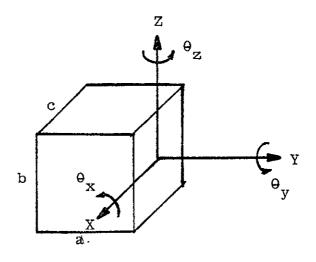


FIGURE 8-6 ILLUSTRATION OF THE COORDINATE SYSTEM

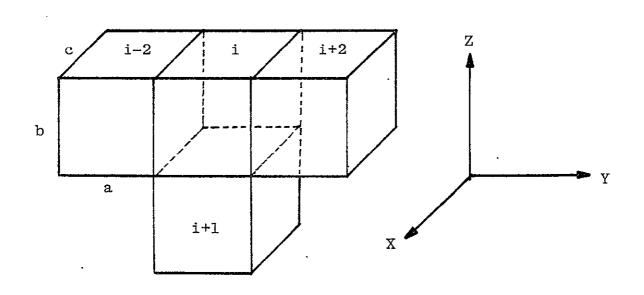


FIGURE 8-7 RELATIONSHIP BETWEEN BODIES

the torsional spring constant

$$K_{\Theta_y} = \frac{J_p}{a} G$$

where $J_{\rm p}$ is the polar moment of inertia and is given by

$$J_p = b^3 c \left[1/3 - 0.21 \frac{b}{c} (1 - \frac{b^4}{12c^4}) \right]$$

With the above definitions, the stiffness matrices for body i in relation to bodies i-2, i+1, and i+2 (see Figure 8-7) are as follows.

(i) the translational stiffness matrix for bodies i and $i\pm 2$:

$$K = \frac{1}{2} \begin{bmatrix} \frac{5}{6} \frac{bc}{a} & G & 0 & 0 \\ 0 & \frac{bc}{a} & 0 \\ 0 & 0 & \frac{5}{6} \frac{bc}{a} & G \end{bmatrix}$$

(ii) the translational stiffness matrix for bodies i and i+1:

$$K_{1} = \frac{1}{2} \begin{bmatrix} \frac{5}{6} \frac{bc}{a} & 0 & 0 \\ 0 & \frac{5}{6} \frac{bc}{a} & 0 & 0 \\ 0 & 0 & \frac{bc}{a} & E \end{bmatrix}.$$

(iii) the rotational stiffness matrix for bodies i and i+2:

$$K_{\Theta} = \frac{1}{2} \begin{bmatrix} \frac{b^{3}c}{12a} E & 0 & 0 \\ 0 & \frac{J_{p}}{a} G & 0 \\ 0 & 0 & \frac{bc^{3}}{12a} E \end{bmatrix}$$

(iv) the rotational stiffness matrix for bodies i and i+1:

$$K_{\Theta_{1}} = \frac{1}{2} \begin{bmatrix} \frac{a^{3}c}{12b} & 0 & 0 \\ 0 & \frac{ac^{3}}{12b} & 0 \\ 0 & 0 & \frac{J_{pp}}{a} & G \end{bmatrix}$$

where
$$J_{pp} = a^3c \left[1/3 - 0.21 \frac{a}{c} \left(1 - \frac{a^4}{12b^4} \right) \right]$$

The factor of one-half arises in the above definitions due to the fact that the spring rates of the adjacent bodies are in series.

The mass of each discrete body composing the beam can be computed from

$$m = \rho v/g$$

where v is the volume of each body and g is the gravitational acceleration.

The moment of inertia of a body about its CM is given by:

 $J = \int (\delta^T \delta I - \delta \delta^T) dm$

where δ is the vector from the CM of the body to an elemental mass dm and is given by

$$\delta^{T} = (ix, jy, kz)$$

and the elemental mass is given by

$$dm = \rho dx dy dz/g$$

For a body of a x b x c

$$J = \int_{-b/2}^{b/2} \frac{a/2 c/2}{-a/2 - c/2} (\delta^{T} \delta I - \delta \delta^{T}) \frac{\rho}{g} dx dy dz$$

Carrying out the integration results in the inertia dyadic

$$J = \frac{m}{12} \qquad \begin{bmatrix} a^2 + b^2 & 0 & 0 \\ 0 & b^2 + c^2 & 0 \\ 0 & 0 & c^2 + a^2 \end{bmatrix}$$

The various vectors that are required for the simulation of the equations of motion of the beam are as follows:

(i) the vectors from the CM of the beam to the CM of the body i:

$$r_i = (0, -\frac{n-2\left[\frac{i+1}{2}\right] + 1}{2} - a, (-1)^{i+1} \frac{b}{2})$$

 $i=1,2,\ldots,r$

$$\mathbf{r}_{2n-\mathbf{i}+1} = -\mathbf{r}_{\mathbf{i}}$$

where $\left[\frac{i+1}{2}\right]$ denotes the integer part of $\frac{i+1}{2}$.

(ii) the vectors from the CM of the half-beam #1 to the CM of the body i in the half-beam #1:

$$_{1}r_{i} = (0, -\left[\frac{\frac{n}{2} - i+1}{2}\right] a, (-1)^{i+1} \frac{b}{2})$$
 $_{i=1,2,...,\frac{n}{2}}$

$$1^{r}_{n-i+1} = -1^{r}_{i}$$

$$1^{r}_{i} = 2^{r}_{n+i}$$
 $j=1,2,...,n$

(iii) the vectors from the CM of body i to the interface point that lies on the line joining the CM of body i and the CM of the adjoining body:

$$d_{i,i+2} = (0, \frac{a}{2}, 0) \qquad i=1,2,\dots,2n-2$$

$$d_{i,i-2} = (0, -\frac{a}{2}, 0) \qquad i=3,4,\dots,2n$$

$$d_{i,i+1} = (0, 0, -\frac{b}{2}) \qquad i=1,3,\dots,2n-1$$

$$d_{i,i-1} = (0, 0, \frac{b}{2}) \qquad i=2,4,\dots,2n$$

(iv) the vectors from the connection point to the CM of body i: $\varepsilon_{n-1}=\varepsilon_n=-\varepsilon_{n+1}=-\varepsilon_{n+2}=(0,-\frac{a}{2},0)$

Finally, it may be pointed out that, for the beam example being considered,

$$a = b = c = 2 ft.$$

8.2.12 Simulation Results

The eigenvalues and the corresponding eigenvectors are obtained, as discussed in Section 8.2.10, for both the full beam and the split-beam. All the eigenvalues are, as expected, non-negative in both cases.

For the full beam, there are six zero eigenvalues which are associated with the six rigid body modes of the beam. The remaining 114 eigenvalues yield the beam's natural frequencies ranging from 58.2Hz to 2066.8Hz. The eigenvectors corresponding to these 114 eigenvalues, the imaginary parts being zero, are real and hence describe the mode shapes of the vibrations. Due to the truncation and roundoff errors in computations, four of the eigenvalues corresponding to the rigid body modes (instead of being zero) are complex conjugates with the real and imaginary parts being less than 10^{-6} and the other two eigenvalues are real and are less than 10^{-5} . Thus, the computed eigenvectors corresponding to these rigid body modes do not portray the shapes of the rigid body modes.

For the split-beam, there are twelve zero eigenvalues, six of which are associated with the rigid body modes of the beam and the rest of which result due to the way the half-beams are put together. The remaining 102 positive eigenvalues yield natural frequencies ranging from 66.8Hz to 2014.5Hz. Thus, there are twelve frequencies of vibration of the beam which are missing for the split-beam case; otherwise, the frequencies

of vibration of the split-beam compare very favorably with the natural frequencies of the full beam, the maximum error being 14.8%. A comparison chart of the frequencies of vibration obtained for the full beam and the split-beam is shown in Table 8-2.

The mode shapes of the non-zero natural frequencies of the split-beam compare, in general, quite favorably with the corresponding mode shapes obtained for the original beam. Since the angular deformations of two of the four bodies involved in the connection of the half-beams have been eliminated from the equations of motion of the split-beam, the mode shapes corresponding to these deformation coordinates are absent in the eigenvectors of the split-beam. In some cases, the relative amplitudes of vibration of the bodies involved in connections, given by the components (of the eigenvectors) corresponding to the deformation coordinates of the bodies in question, are close to zero. it may be pointed out that the corresponding components of the eigenvectors of the original beam are small, generally less than 20% of the maximum component of the eigenvector being considered.

In summary, the lower-order modes (that is, modes corresponding to the frequency range from the lowest to a frequency at least ten times the lowest frequency) of the split-beam compare very well with those of the original beam. The natural frequencies of the beam that are missing from those obtained for the split-beam are all in the high frequency range. Further, there

TABLE 8-2
COMPARISON OF THE FREQUENCIES OF VIBRATION
FOR THE ORIGINAL BEAM AND THE SPLIT-BEAM

ORIGINAL BEAM	SPLIT-BEAM
58.2	66.8
102.4	115.1
125.5	140.6
151.4	153.5
225.6	233.1
249.9	252.7
275.6	305.3
291.9	324.1
363.7	384.6
372.8	409.3
418	429.4
495.4	504.3
495.6	509.6
568.7	622.0
576.7	576.7
617.7	652.7
618.7	667.5
623.2	657.9
719.3	746.5
735.4	756.8
741.7	767.2
780.3	783.2
847.2	*
859.8	917.4
862.3	916.2

TABLE 8-2 CONT'D

- --

ORIGINAL BEAM	SPLIT-BEAM
873.4	929,1
933.1	933.1
934.5	974.9
948.3	951.8
965	984
989.9	1045
991	991
1024.8	1071.6
1037	*
1044.1	*
1054,1	1074.1
1096.9	1096.9
1128.6	1128.6
1131.3	1139.5
1145.4	1157.2
1184.7	1128
1192.3	1192.5
1192.5	1192.6
1199.4	1199.4
1200.4	1202.8
1201.5	1201.9
1205.9	1247.2
1209	1181.4
1229.8	1231.5
1263.7	1219.7
1278.4	1278.4
1289.3	1291.3
1290.8	1294.7

TABLE 8-2 CONT'D

ORIGINAL BEAM	SPLIT-BEAM
1307.9	1317.8
1309.9	1311.3
1316.3	1362.4
1319.6	1319.6
1319.6	*
1319.6	*
1324.9	1344.4
1340.5	*
1341.1	1346.3
1358.8	*
1359	1307.3
1373.1	1374.2
1376.5	*
1387.9	1387.9
1401.3	1399.6
1402.3	1419.8
1409.9	1410.4
1411.9	1427.3
1417.4	1378.8
1431.3	1394.9
1433.4	1408.6
1441.1	1485.7
1461.6	1413.8
1466.3	1492.7
1503.3	*
1509.8	1509.8
1513.2	1515.7
1517.4	1565.1

TABLE 8-2 CONT'D

ORIGINAL BEAM	SPLIT-BEAM
1529.2	*
1530.5	1546.6
1556	1554
1579.3	*
1579.8	1562.9
1600.8	1564.7
1601.3	1601.4
1601.9	1601.2
1611.3	*
1627	1656.3
1635.7	1624.8
1635.9	1636
1656.4	1634.1
1656.5	1623.5
1662.8	*
1663.4	1669.2
1686.9	*
1690.1	1691.5
1713.5	1719.6
1721	*
1723	1657.8
1751.2	1724.5
1759.7	1759.7
1761.6	1761.6
1774.8	1774.8
1786.3	1756.4
1786.9	1752.9
1800.2	1829.2

TABLE 8-2 CONT'D

ORIGINAL BEAM	SPLIT-BEAM
1843.2	1753.6
1866	1850
1944.8	2002.2
2017.5	2014.5
2066.8	*

^{*}Denotes frequencies for which there are no corresponding mode shapes.

are four split-beam's natural frequencies for which there are no corresponding mode shapes in the original beam. However, these are again in the high frequency range. The fact that the higher-order modes of the split-beam do not compare as well as the lower-order modes do with the corresponding modes of the original beam, poses no problem since the control systems associated with spacecraft are, in general, low frequency systems.

The computer outputs showing the natural frequencies and the mode shapes for the original beam and for the split-beam are given in Appendices G and H, respectively.

8.3 CONCLUSIONS

The computer simulation results indicate that the frequencies of vibration and the corresponding mode shapes obtained from the free-free modes of the halfbeams and using the method developed for combining the half-beams compare very favorably with those obtained for the original beam using the standard discrete The distortions that are coordinate formulation. encountered in the modes of the split-beam are mostly in the higher-order modes. These distortions are mainly due to the fact that the dynamic model of the split-beam includes, in effect, only 18 bodies whereas the original beam is modeled with 20 bodies. the bodies are "lost" because, for the split-beam, there are only 18 rotational equations and two of the 20 translational equations give rise to six more rigid body modes that are not in the original beam.

ten percent of the components of the system are, in effect, "lost" when the new modeling technique is utilized for a beam modeled with a small number of bodies. In practice, however, the number of bodies that constitute a spacecraft is large and the number of components involved in connections would be very small thus resulting in a very small percentage of the bodies being "lost" when the modeling technique being considered is used. Thus, in practice, it is expected that the difference between the flexible body characteristics obtained via the new method and the actual flexible body characteristics would be insignificant.

Hence, it can be concluded from the above remarks and the simulation results obtained that the method (reference 8-1) of combining substructures of a system achieves a good degree of fidelity in the determination of flexible body characteristics for the overall system from the characteristics of the substructures constituting the system.

8.4 REFERENCES

- 8-1 Rybak, S. C., A Method for Determining Overall Flexible Body Characteristics for a Series of Connected Substructures, Rocky Mountain Guidance and Control Conference, March 10-13, 1978, Keystone, Colorado.
- 8-2 Canavan, J. R. and Likins, P. W., Floating Reference Frames for Flexible Spacecraft, Journal of Spacecraft and Rockets, Vol. 14, No. 12, December 1977, pp 724-732.

SECTION 9

9.0 CONCLUSIONS AND RECOMMENDATIONS

Equations have been generated for three different approaches to controlling a large flexible spacecraft. Two of the three (LQR and MNA) were simulated controlling a single axis of the Space Construction Base (SCB), Configuration 1. The third approach, multilevel control, was developed for a three axis SCB simulation; but the computer program was too complex for the actual simulation to be completed before the end of this reporting period.

One control approach utilized some conventional optimization techniques based upon design in the time domain. This approach (LQR) can be easily expanded in dimensions (more axes, actuator locations, flexible modes, etc), readily extended to include noise sources at sensors and actuators, and the filtering of state measurements.

The second control method (MNA), is esentially based upon design in the frequency domain. It utilizes system matrix manipulation to obtain diagonal dominance, thereby reducing the problem to a set of independent single loop designs.

The third control method utilizes a multilevel hierarchal technique which is amenable to implementation by a digital processor. Optimization of the control system is obtained through a performance index using weighting factors on components of the state variable and control vectors.

The other portion of the study was related to mathematical modeling of flexible spacecraft dynamics. previously generated SCB vehicle equations were derived for large angular displacements of the central body and the appendages (solar wing elements). The model was simplified considerably by restricting motion to small This linearized model was then angular displacements. utilized in single-axis control simulations and the multilevel, three-axis, simulation equations. three axis linearized equations were also examined with respect to MNA control while including the cross-coupling between axes (the full order mode, FOM). The reduced order model (ROM) was generated to study control of the SCB without cross-coupling, thereby reducing the problem from one larger three-axis analysis to three much simpler single-axis analyses.

A structural analysis study (Section 8) illustrated a technique whereby the structural characteristics of two or more submodules may be combined when the submodules are firmly connected, as through docking or berthing ports. Prediction of the resulting dynamics may be based upon the theory presented. This was verified by means of an example of connecting two shorter beams to obtain one which is longer.

9.1 CONCLUSIONS

The following conclusions are based upon the formulation of control equations and the simulations of Configuration 1 of the Speae Construction Base:

- a. Excellent simulation results were obtained when feeding back the full state variable vector (for LQR, MNA and Retallack pole placement).
- b. The results for partial feedback of the state variable vector were satisfactory, but power expended at the central body actuator system was excessive when appendage deflection states were omitted (LQR).
- c. The MNA approach also produced good performance for the difficult case of vehicle flexible modes being within the closed loop bandwidth of the attitude control system.
- d. The Retallack pole placement method was very successful in placing specific open loop poles in desired positions when the control system loop is closed.
- e. The three-dimensional, five-body, linearized vehicle model was transformed into a scalar state variable equation set which was readily programmed for a digital computer.
- f. The three-axis, five-body multilevel control method was similarly transformed into an equation set amenable to programming.
- g. Cross-axis coupling of the subject vehicle was virtually negligible; that is, differences between the reduced order model (ROM) and the full order

model (FOM) were negligible.

In addition, the structural analysis technique developed in Section 8 was fairly successful in predicting the frequencies of vibration and mode shapes of the "splitbeam" structure where the two submodules are fastened end-to-end. This is particularly fortunate since the number of finite elements used was not very high; 20 bodies were used in defining the original full beam and two sets of 10 bodies were used for each of the two connected submodules. Finite element modules for space-craft in later stages of design usually are defined to a much higher degree; the fidelity of the method described, therefore, is actually expected to be much better when applied to clusters of "real" space vehicle modules.

9.2 RECOMMENDATIONS

The following items are recommended for future studies regarding control of large flexible space vehicles:

- a. All three control methods should be expanded to stabilize space vehicles modeled with more discrete elements and dimensions.
- b. Similarly, the control should be expanded to stabilize vehicles modeled in three axes, including crosscoupling.

- c. More attention must be devoted to quick, accurate generation of spacecraft mathematical models. For vehicles such as Configuration 1 of the SCB, the hybrid coordinate technique is an excellent candidate for this type of study because of the flexible solar wings. Decisions for truncating modes may then be more confidently made on the basis of modal dominance and frequencies.
- d. Noise on sensor measurements of states and at actuators may be included in future studies; these are customarily extensions to the LQR method.
- e. The MNA and pole placement method should be expanded to placement of closed loop poles with regard to the magnitude of frequency (in addition to damping factor).
- f. Control simulations of the LQR and MNA with pole placement methods should be repeated for the X and Y axes of the same vehicle configuration.
- g. Because of uncertainties of vehicle model parameters, sensitivity analyses must be included in control system evaluation to determine variations in performance.
- h. It may be desirable to try other pole placement techniques (the standard Simon and Mitter technique and the Kalman pole placement algorithm), and evaluate the subsequent designs and performance.

- i. A test should be developed for robustness of the control design as a means of simplifying design for future configurations.
- j. The three-axis multilevel control simulation should be completed (the SCB Configuration 1 model equations have previously been programmed).
- k. When access to measurement of essential state variables is impractical, filtering techniques must be developed for generation of observers required for the inaccessible states.
- 1. The LQR method should be expanded for stabilization of two or more locations on a large flexible space vehicle; for example, when multiple Instrument Pointing Systems (IPS) are used. There may be a need for stabilization of all six degrees of freedom at the mounting location, particularly when the center of mass of the IPS inner gimbal and payload is not located at each gimbal pivot axis.

It is recommended also, that the structural analysis technique that was developed and evaluated on beams with a limited number of elements, be verified for a high degree of fidelity on more complex structural models with many more finite elements. Further, the problem of substructure model truncation prior to determining the overall system's characteristics should be examined.

APPENDIX A

NUMERICAL VALUES OF MATRICES USED IN ANALYSIS AND DESIGN

• Space Construction Base, Configuration 1

Values of matrices P, N, KD, KS, A, and B used for analysis and control system design purposes are shown on the following pages. A list of constants used in the model is also shown in this Appendix.

Most of the parameter values used in the simulation of five-body three-dimension model of Configuration I are based upon the request issued by Marshall Space Flight Center.

*** P ARRAY (P * (NDOT) = Q) *** TWO LINES PER A ROW

0. 3205759E 05 0. 00000000E	00 0.48828136	:-03	04 0.1424752E-73	0.0000000E 00 0.	4884074E 04 0.00000000E 00
FL MODODODE 00 0. 1504288E	04 0.00000006		00 0.1504288E 04	0.0000000E 00 0.	00000000E 00
0.0000000E 00 0.2948331E	96 9, 9 09090908	. 00 0 . 0000000E	00 0.4884078E 04	0.0000000E 00 0.	0000000E 00 0.4884074E 04
0.0000000E 00 0.0000000E	99 9, 1 5942886	. 04 0. 0000000E	00 0.0000000E 00	0.1504288E 04 0.	0000000E 00
0.0000000E 00 0.0000000E	00 0. 2938206E	06-0,2556577E	05 0.0000000E 00	9.0000000E 00 0.	2556577E 05 0.0000000E 00
0.0000000E 00 0.2717345E	05 0. 2834020E	05 0,0000000E	00 0.7874219E 04	9.0000000E 00 0.	
0.4884078E 04 0.00000000	00-0.2556577E	05 0.5356800E	05 0.0000000E 00	0. 00000000E 00 0.	9802957E 03 0.0000000E 00
0.0000000E 00 0.1868064E	05 0.0000000E	00 0.0000000E	00 0.3019297E 03	0. 0000000E 00 0.	0000000E 00
0.3635371E 46 0.4884078E	04 0.0000000E	: 00 0 . 0000000E	00 0.54326 81E 0 5	0.0000000E 00 0.	0000000E 00 0.9802957E 03
0.0000000E 00 0.0000000E	00 0.1868064E	: 05 0 . 0000000E	00 0.0000000E 00	0.3019297E 03 0.	0000000E 00
0.0000000E 00 0.0000000E	00 0.00000000	. 00 0 . 0000000E	00 0.0000000E 00	0.7571689E 03 0.	0000000E 00 0.0000000E 00
0.0000000E 00 0.0000000E	00 0.0000000	. 00 0 . 0000000E	00 0.0000000E 00	0.0000000E 00 0.	0000000E 00
0. 4884074E 04 0. 0000000E	00 0. 2 556 5 77 6	05 0.9802957E	03 0.0000000E 00	0.0000000E 00 0.	5356797E 05 0.0000000E 00
0. 0000000E 00 0. 3019294E	03 0. 0 0000006	00 0.0000000E	00 0.1868063E 05	0.0000000E 00 0.	0000000E 00
9, 3009090E 00 0, 4884074E	04 0.00000000	00 0. 0000000E	00 0.9802957E 03	0.0000000E 00 0.	0000000E 00 0.5432678E 05
0 0000000E 00 0, 0000000E	00 0.3019294E	03 0 .0000000E	00 0.0000000E 00	0.1868063E 05 0.	0000000E 00
0.0000000E 00 0.0000000E 0.7571692E 03 0.0000000E	00 0.0000000E	00 0.0000000E	. 00 0.0000000E 00 . 00 0.0000000E 00	0.0000000E 00 0. 0.0000000E 00 0.	0000000E 00 0.0000000E 00 0000000E 00
0. 1504288E 04 0. 0000000E	00 0.2717345E	05 0.1868064E	05 0.0000000E 00	0.0000000E 00 0.	3019294E 03 0.0000000E 00
0. 0000000E 00 0. 1180585E	05 0.0000000E	00 0.0000000E	00 0.9299382E 02	0.0000000E 00 0.	0000000E 00
0.0000000E 00 0.1504288E 0.0000000E 00 0.0000000E	04 0.2834020E 00 0.1256466E	05 0.0000000E	00 0.1868064E 05 00 0.0000000E 00	0.0000000E 00 0. 0.9299382E 02 0.	0000000E 00 0.3019294E 03
0.0000000E 00 0.0000000E 0.0000000E 00 0.0000000E	00 0.0000000E	00 0.0000000E 00 0.7571689E	00 0.0000000E 00 03 0.0000000E 00	9. 0000000E 00 0 . 0. 0000000E 00 0.	0900000E 00 0.0000000E 00
0. 1504288E 04 0. 00000000	00 0.7874219E	04 0.3019297E	03 0.0000000E 00	9. 90909089E 99 9,	1868063E 05 0.0000000E 00
0. 0000000E 00 0. 9299382E	02 0.0000000E	00 0.0000000E	00 0.1180585E 05	9. 9999999E 99 9,	0000000E 00
0,0000000E 00 0,1504288E	04 0.0000000 E	00 0 . 0000000E	00 0,3019297E 03	0.0000000E 00 0.	0000000E 00 0.1868063E 05
0 9000000E 00 0,0000000E	00 0.9299382E	02 0 . 0000000E	00 0,0000000E 00	0.1256466E 05 0.	0000000E 00
0.0000000E 00 0.0000000E	00 0.00000 005	00 0.0000000E	. 00 0. 0000000E 00	0. 00000000E 00 0.	0000000E 00 0.0000000E 00
0.6000000E 00 0.0000000E	00 0.0 0000006		. 00 0. 0000000E 00	0. 0000000E 00 0.	7571692E 03

BENDIX RESEARCH LABORATORIES

*** N ARRAY *** (W = N* XH1)

1. 00	9. 00	Ø. 00	<u> 9</u> . 80	0. 00	0, 00	9. 99	0. 00	0. 00	0. 00	0. 60	0. 00	9 . 99	Ø. ØØ	0. 00
0 . 00	1. 00	0.00	0. 00	Ø. 00	9. 00	· 0. 00	Ø. ØØ	0. 00	0. 00	0. 00	0. 00	0. 00	0.00	Ø. ØØ
0.00	0.00	1. 00	9. 99	0. 00	0. 00	0. 00	9 . 9 9	9. 00	0. 00	0. 00	0. 00	0. 00	0. 0 0	0.00
1, 00	9 . 00	Ø. 0 <u>9</u>	1. 00	0. 00	0. 00	9. 00	ø. øø	0. 0 0	0. 00	0.00	0. 00	0 . 00	0.00	0. 00
0. 00	1. 00	9. 09	0. 00	1, 00	0. 00	9 . 00	9. 00	0. 00	0. 00	0. 00	0. 00	0. 00 ·	0 . 00	0. 00
0. 00	0.00	1. 00	0. 00	0.00	1. 00	0. 00	Ø. ØØ	0. 00 ·	0. 00	0.0 0	0. 00	0. 00	0. 00	0. 00
1. 00	ø. 00	Ø. 00	0. 00	0. 00	Ø. ØØ	1. 00	0. 00	9. 00	0. 00,	0. 00	0. 00	0.00	0.00	0. 00
0. 00	1.00	0. 00	0. 00	Ø. ØØ	0. 00	0. 00	1. 00	0. 00	0. 00	0. 00	0. 00	Ø. ØØ ·	0. 00	0. 00
0 . 00	0.00	1. 00	0. 00	9. 00	0. 00	Ø. ØØ	Ø. ØØ	1. 00	0. 00	0. 00	0. 00	0 . 00	0. 00	0. 00
1. 00	9 . 00	0. 00	1. 00	0. 00	9. 99	0. 00	0. 00	9. 99	1. 00	0. 00	0. 00	Ø. ØØ	0. 00	Ø. 0 <u>0</u>
0.00	1. 00	9. 00	0. 00	1. 00	0. 00	0. 00	0 . 0 0	0. 00	0. 00	1. 00	0. 00	Ø. ØØ	0. 00	0. 00
0 . 00	0.00	1. 00	9. 00	0. 00	1. 00	0. 00	Ø. ØØ	0. 00	Ø. ØØ	0. 00	1. 00	0.00	0 . 00	0 . 00
1.00	8 . 00	0. 00	0. 00	0. 00	0, 00	1. 00	0 . 00	0. 00	Ø. ØØ	0. 00	0. 00	1. 00	0.00	Ø. 00
0. 00	1.00	0. 00	0. 00	0. 00	0. 00	Ø. ØØ	1. 00	0. 00	0. 00	Ø. ØØ	0. 00	0 . 00	1. 00	0. 00
0. 00	0. 00	1. 00	0. 00	0. 00	0. 00	0. 00	0. 0 0	1. 00	0. 00	Ø. ØØ	0. 00	0.00	0. 00	1. 00

*** KD DAMPING CONSTANT ARRAY *** (TWO LINES PER A ROW)

						•																	
Ø.	0000000E	90	0, 1	0000000E	99	0.	00000000E	ยย	и.	ดอดออออต	80	υ.	00000000E	00	υ.	00000000							
_			_		-00	_	0000000	90	α	GOOGGOOF	aa	ø	2677729E 00000000E	ดร	Ø.	AAAAAAAAE	0 0	Ø. 1	9000000E	0 0	Ø. '	2677729E	03
_				0000000	-00		0000000	aa	a	000000BE	aa	a	00000005E 00000005E	ρP.	Я	3587900E	91	0.	9999999E	99	0.	0000009E	00
			_			_		00		2004 0005	62	a	00000000E	ផង	а	GOGGGGGE	90	Ø.	0000000E	0 0	0.	0000000E	99
_			_			_	~~~~~~	- 00	•	annanar.	20-	-a	2677729E 0000000E	ดร	ด	аварарае	99	0.	0000000E	00	Ø	0999999E	98
_			_			_	0000000			00000000	aa	a	0000000E	ผด-	-a	3587900E	01	0.	999999E	99	0.	9999999E	99
_			_				0000000	. 00		aggggggE	aa	a	0000000E	ØО	а	ARREGUEE	00-	-0.	3621600E	02	0.	000000E	89
_			_			_	0000000			0000000	00	a	0000000E	aa	Я	ADDRAGOE	00	Ø.	0000000E	99	-0.	2677729E	0 3
_			_							00000000	80	a	00000000E	aa	а	арарарая	99	Ø.	0000000E	99	0.	0000000E	00
			_				0000000	- 00		0000000	00	a	. 00000000E . 00000000E	ดด	ด	9999999E	00	Ø.	0000000E	00	0.	0000000E	00
_			_				0000000	- 00		00000005	aa	a	AGGGGGGF	ดด	а	рарарара	99	0.	000000E	99	0.	9999999E	00
_			_				6000000	- 00		COCCOCC	- 00	a	. 0000000E	o a	Ø	даррара Е	90	0.	0000000E	00	0.	. 0000000E	00
0.	0000000	E 00	0.	0000000	E 08	9 0	. 0000000	= 60)-W	. 32033000	. 6T	. e	. 00000000	. 00	. מ	. 00000000 8000000F	เดด	0	9099999E	99	0.		
Ø.	0000000	E 00	0.	00000000		3 0	. 80000000	E 191		, eesõeset	. 00	, - e	. 1000000L	. O.	, o	. ООВЕССЕ	. 00	0	. 0000000E	. 00	. 0		
0.	0000000	E 00	1 0.	9899999	E 0	3 6	. 0000000			. ********	: 00 : 00		, 6900000± 10000000	. 00		. DA TODOS	- 00	- . В	ANNANNA	90	9 0		
9. 9	. 0 000000 . 0000000	E 00	0.	. 0000000 . 0000000	E 01	9 6). 00000000). 00000000	E 01	9 6). 0000000GE	. 00	9 6). 00000000E	90	ð	. 00000000	90	ı–Ø	. 3203900E	01	•		

*** KS STIFFNESS MATRIX *** (TWO LINES PER A ROW)

Ø. Ø.	00000 00	90E	00 00	Ø. 1 Ø. 1	0000000E	99	Ø. Ø.	00000000E	98 99	Ø. Ø.	1966830E 0000000E	95 99	0. 0.	00000000E	00 00	Ø. Ø.	00000000E	00 00	Ø. Ø.	1966830E 0000000E	05 00	Ø.	0000000E	99
Ø. Ø.	00000 0	90E	00 00	0. I 0. I	000000088	99 99	Ø. Ø.	0000000E	00 00	0. 0.	0000000E	00 00	0. 0.	59984 10 E 60000005E	97 99	Ø 0.	00000000E 0000000E	00 00	0 . 0.	00000000E	99 90	Ø.	5998410E	07
Ø. Ø.	000000 655720	90E	00 03	9. i 9. i	00000001 00000001	99	Ø. Ø.	0000000E 0000000E	00 08	Ø Ø.	0000000E	00 00	0. 0.	00000000E 00000000E	00 00	Ø. Ø.	6557200E 0000000E	00 03	0. 0.	00000000E	99 99	Ø,	0000000E	00
Ø. Ø.	000000 000000	90E	00 00	0. 0. :	00000000 1841400	00 04	Ø. Ø.	0000000E	00- 00	-Q. Ø.	1966830E 0000000E	95 99	0. 0.	0000000E	00 00	Ø. Ø.	00000000E	9 0 99	0. 0.	00000000E	99 90	9.	9999999E	90
Ø. Ø.	000000 000000	30E	00 00	Ø. Ø.	00000000 0000000	00	Ø. Ø.	0000000E 7024030E	00 06	Ø. Ø.	0000000E 0000000E	00- 00	-Ø. Ø.	5998410E 0000000E	07 00	Ø. Ø.	9600000E	00 00	Ø. Ø.	80000000E 80000000E	99 90	0.	0000000E	00
0. 0.	000000	90E 90E	00 00	Ø. Ø.	00000001 00000001	E 00	0. 0.	0000000E	00 00	Ø. Ø.	0000 000E 8954900E	00 02	Ø. Ø.	00000000E 00000000E	00- 00	-0. 0.	6557200E 0000000E	00 80	Ø. Ø.	0000000E 0000000E	99 99	Ø,	9999999E	00
Ø. Ø.	000000 000000	30E	99 99	Ø. Ø.	00000001 00000001	E 00	Ø. 1 Ø.	0000000E	99 99	0. 0.	0000000E	99 90	Ø. Ø.	0000000E 1841400E	00 04	Ø. Ø.	00000000E 00000000E	00 00	-0. 0.	1966830E 0000000E	05 00	0.	0000000E	00
Ø.	000000	30E	ØØ	0.	0000000	E 00	0.	0000000E	99	0.	08008BRF	พพ	ъ.	ORROGORE	99	Ю.	(6546765	60	٠.	9099990C	ಛಲ			
~Ø.	655720	98E	93	0.	0000000	E 00	0.	0000000E	99	0.	GGGGGGGF	ผผ	6.	9999999	99	Ю.	0666666E	99	Θ,	0204269E	O.C.			
0.	000000	30E	90-	Ø.	1841400	E 04	0.	0000000E	99	0.	QQQQQQQE	ียย	И.	กดกดดอดธ	เล	Ø,	ดดอดดอดอดต	CO	€.	0000000	-00			
0.	000000	30E	60	0.	0000000	= 04	JU.	0000000E 7024030E	ÑР	Ю.	00000000	66	О.		99	Ο.	90000000		₩.	0000000				
Ø.	00000	90E	90	0.	0000000	E 00	9	. 0000000E . 0000000E	00	-0.	8954900E	62	Ю.	30000000	טט	Ø.	00000000	65	٠,,	9000000L	ÓΩ			
0.	00000	00E	00	0.	0000000	E 00	9 0	. 00000000E . 00000000E	กก	И.	имиминин	מט.	-0.	. 18414666	94	Ø,	. 66666990	50	w.	00000000				
0.	00000	00E	00	0.	0000000	E 09	9 0	. 00000000E . 0000000E	90	Ю.		טט.	Ю.	. മരവവദെട	60	-o.	, 10270	00	٥.		~~			
Ø. Ø.	00000	00E 00E	98 99	0. 0.	0000000 0000000	E 00	3 Ø	. 000 000 00E . 00000000E	99 99	0.	. 000 00000E . 00000000E	99	Ø. Ø.	. 00000000E . 00000000E	00 00	Ø. Ø.	. 0000000E . 0000000E	99 99	0. -0.	0000000E 8954900E	00 02	0.	0000000E	00

*** A11 PART OF A -THE PLANT MATRIX (ROWS=1,13 ; COLS=1,15) *** (TWO LINES PER A ROW)

~ 0.0000000E 00 0.0000000E 00 0.000000E 00 0.1280899E-02 0.0000000E 00-0.5771543E-12 0.1280899E-02 0.0000000E 00 -0.5771543E-12-0.6926712E-03 0.0000000E 00 0.000000E 00-0.6926707E-03 0.0000000E 00 0.0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00 0,1000111E-02 0,0000000E 00 0,0000000E 00 0,1000111E-02 0.000000E 00 0.000000E 00-0.1348562E-02 0.000000E 00 0.000000E 00-0.1348562E-02 0.000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.7501572E-04 0.000000E 00 0.1336089E-04 0.7501571E-04 0.0000000E 00 0,1336089E-04 0,4367963E-03 0,0000000E 00 0,0000000E 00-0,4367961E-03 0,0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00-0,2962485E-02 0.0000000E 00 0.7431766E-05-0.1354121E-02 0.0000000E 00 0.7431766E-05 0.1767937E-01 0.0000000E 00 0.0000000E 00 0.4263467E-03 0.0000000E 00 0.0000000E 00 0, 0000000E 00 0, 0000000E 00 0, 0000000E 00 0, 0000000E 00-0, 1118445E-01 0, 0000000E 00 0, 0000000E 00-0, 9886064E-03 0,000000E 00 0,000000E 00 0,2963305E 00 0.000000E 00 0.000000E 00-0.1739376E-03 0.000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.7501571E-04 0.0000000E 00-0.4751936E-02-0.7501572E-04 0.0000000E 00 -0.1336089E-04-0.4367963E-03 0.0000000E 00 0.4231419E-02 0.4367961E-03 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.1354121E-02 0.0000000E 00-0.7431767E-05-0.2962486E-02 0.0000000E 00 -0.7431767E-05.0.4263471E-03.0.000000E 00.0.000000E 00.0.1767937E-01.0.000000E 00.0.000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.9886064E-03 0.0000000E 00 0.0000000E 00-0.1118445E-01 0 0000000E 00 0 0000000E 00 0 1739395E-03 0 0000000E 00 0 0000000E 00 0 2963274E 00 0 0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.7501571E-04 0.0000000E 00-0.1336089E-04-0.7501572E-04 0.0000000E 00 -0,4751936E-02-0,4367963E-03 0.0000000E 00 0.0000000E 00 0.4367961E-03 0.0000000E 00 0.4231419E-02 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.4130814E-02 0.0000000E 00-0.1011085E-04 0.9961669E-04 0.0000000E 00 -0.1011085E-04-0.5660854E-01 0.0000000E 00 0.0000000E 00 0.3623310E-03 0.0000000E 00 0.0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00 0.2520601E-01 0.0000000E 00 0.0000000E 00-0.1479540E-04 0.0000000E 00 0.0000000E 00-0.9839008E 00 0.0000000E 00 0.0000000E 00 0.1957956E-02 0.0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00 0,0000000E 00 0.0000000E 00 0.4738573E-02 0.0000000E 00 0.0000000E 00 9, 99999999E 99 9, 9999999E 99 9, 9999999E 99-9, 8462839E-92 9, 9999999E 99 9, 9999999E 99 9, 9999999E 99 9, 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.9961659E-04 0.0000000E 00 0.1011084E-04 0.4130814E-02 0.0000000E 00 0.1011034E-04 0.3623313E-03 0.0000000E 00 0.0000000E 00-0.5660854E-01 0.0000000E 00 0.0000000E 00 · 0,0000000E 00 0.000000E 00 0.000000E 00 0.000000E 00-0.1479524E-04 0.000000E 00 0.000000E 00 0.2520575E-01 0. 0000000E 00 0. 0000000E 00 0. 1957956E-02 0. 0000000E 00 0. 0000000E 00-0. 9838948E 00 0. 0000000E 00 **9. 0000000E 30 0. 0000000E 00 0. 0000000E** 0,4738573E-02 0,0000000E 00 0,0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.8462839E-02

*** A12 PART OF A -THE PLANT MATRIX (ROWS=1,15 ;COLS=16,30) *** (TWO LINES PER A ROW)

0.0000000E 00 0.0000000E 00 0.0000000E 00 0.6956348E 00 0.0000000E 00-0.1054800E-09 0.6956348E 00 0.0000000E 00 -0.1054800E-09-0.8228935E-02 0.000000E 00 0.000000E 00-0.8228928E-02 0.000000E 00 0.000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0 2240359E 02 0.0000000E 00 0.0000000E 00 0.2240359E 02 0. 0000000E 00 0. 0000000E 00-0. 3008974E 00 0. 0000000E 00 0. 00000000E 00-0. 3008974E 00 0. 0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.4073977E-01 0.0000000E 00 0.2441819E-02 0.4073976E-01 0.0000000E 00 8.2441819E-02 0.5189139E-02 0.0000000E 00 0.0000000E 00-0.5189139E-02 0.000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.1608875E 01 0.0000000E 00 0.1358220E-02-0.7354001E 00 0.0000000E 00 0, 1358220E-02 0, 2100309E 00 0, 0000000E 00 0, 0000000E 00 0, 5064998E-02 0, 0000000E 00 0, 0000000E 00 9, 0000000E 00 0, 0000000E 00 0, 0000000E 00 0, 0000000E 00-0, 2505439E 03 0, 0000000E 00 0, 0000000E 00-0, 2214587E 02 0.0000000E 00 0.0000000E 00 0:6611862E 02 0.0000000E 00 0.0000000E 00-0.3880975E-01 0.0000000E 00 0.000000E 00 0.000000E 00 0.000000E 00 0.4073977E-01 0.000000E 00-0.8684571E 00-0.4073976E-01 0.000000E 00 -0.2441819E-02-0.5189139E-02 0.0000000E 00 0.1182682E 00 0.5189139E-02 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.7354001E 00 0.0000000E 00-0.1358220E-02-0.1608876E 01 0.0000000E 00 -0.1358220E-02.0.5055005E-02.0.0000000E 00.0.0000000E 00.0.2100309E 00.0.000000E 00.0.000000E 00. 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00-0.2214587E 02 0.0000000E 00 0.0000000E 00-0.2505439E 03 0.000000E 00 0.000000E 00-0.3881019E-01 0.0000000E 00 0.000000E 00 0.6611795E 02 0.000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.4073977E-01 0.0000000E 00-0.2441819E-02-0.4073976E-01 0.0000000E 00 -0.8684571E 00-0.5189139E-02 0.0000000E 00 0.0000000E 00 0.5189139E-02 0.0000000E 00 0.1182682E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.2243375E 01 0.0000000E 00-0.1847846E-02 0.5410015E-01 0.0000000E 00 -0.1847846E-02-0.6725094E 00 0.0000000E 00 0.0000000E 00 0.4304495E-02 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.5646426E 03 0.0000000E 00 0.0000000E 00-0.3314323E 00 8. 0000000E 00 0. 0000000E 00-0. 2195325E 03 0. 0000000E 00 0. 0000000E 00 0. 4368683E 00 0. 0000000E 00 0. 8660153E 00 0. 0000000E 00-0. 2365364E 00 0. 0000000E 00 0. 0000000E 00 0,0000000E 00 0.0000000E 00 0.0000000E 00 0.5410010E-01 0.0000000E 00 0.1847845E-02 0.2243375E 01 0.0000000E 00 0. 1847845E-02 0. 4304495E-02 0. 0000000E 00 0. 0000000E 00-0. 6725094E 00 0. 0000000E 00 0. 0000000E 00 0,0000000E 00 0.000000E 00 0.000000E 00 0.000000E 00-0.3314285E 00 0.0000000E 00 0.0000000E 00 0.5646367E 03 0.0000000E 00 0.000000E 00 0.4368683E 00 0.000000E 00 0.000000E 00-0.2195312E 03 0.000000E 00 0. 0000000E 00 0. 0.8660153E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.0000000E 00 0.2365364E 00

A-7

BENDIX RESEARCH LABORATORIES

*** B ARRAY (CONTROL MATRIX) FIRST 15 ROWS ***

0. 3283360E-04 0. 0000000E 00-0. 1608613E-12-0. 3284731E-05 0. 0000000E 00 0. 0. 000000

*** ROWS 16 THRU 30 ARE ALL ZEROS ***

BENDIX RESEARCH LABORATORIES

***** SPACE BASE, CONFIGURATION 1(5BODY) *****

		4	
CD	MSN1	KXSM1	KXSVB
1	0.5109602E 03	0. 5125000E 01	Ø 2991702E 02
CD	MHM1	KYSM1	KYSNB
CD	0.5124204E 03	0.4816702E 01	0. 3091702E 02
CD	NDM1	KZSM1	KZSWB
	0.1748300E 03	0. 4816702 <u>F</u> 01	0. 7566702E 01
CD	MTA1	KXSWA	KXTA1
4	0. 2020201E 02	0.2991702E 02	0. 3091702E 01
CD	MSWA	KYSWA	KYTA1
5	0. 2644902E 02	0.3091702E 02	0.3625000E 01
CD	MSWB	KZSWA	KZTA1
6	0. 2644902E 02	0.7566702E 01	0. 3625000E 01
CD	DTA1	LDM1	LHM1
?	0.8750000E 01	0.1080000E 02	0.2600000E 02
8	LSM1	LTA1	1XDM1
CD	0.1100000E 02.	0.1100000E 02	, 0. 3972300E 04
CD	IXHM1	IYDM1.	14HM1
	0.1345900E 05	0.3686000E 04	0.3558500E 05
CD	IZDM1.	IZHM1	WSWA
10	0. 3686000E 04	0. 3558500E 05	0: 2600000E 02
CD	MSNB	XDM1	YDM1
11	0. 2600000E 02	-0.3141698E 02	0. 0000000E 00
CD	.ZDM1	XSWA	YSWA
12	Ø. 000000E 00:	0. 1650000E 02	0. 0000000E 00
CD	ZSNA	XHM1.	YHM1
13	8. 5958301E 82	-8. 1300000E 02	.0. 0000000E. 00
CD	ZHM1 _	XSNB	YSMB
14	0. 0000000 00	0. 1650000E 02	0. 0000000E 00
ČD	ZSWB	XSM1	YSM1.
15	-0. 5958299E 02	0.550000E 01	9: 0000000E 00
CĎ	25M1	XTA1	YTA1
16	0. 0000000E 00	0. 1650000E 02	0.0000000E 00
CD	ZTA1	K512X	KS12Y
17	0.000000E 00	0.1966830E 05	0. 5998410E 07
CD	KS12Ž	C512X	CS12Y
18	0. 6557202E 03	0.3621600E 02	0. 2677732E 03

A-10

CD	CS12Z	KS13X	KS13Y
19	0.3587900E 01	0. 1966830E 05	0. 5998410E 07
ĆD	KS1.3Z	CS13X	CS13Y
20	0. 6557202E 03	0. 3621600E 02	0. 2677732E 03
CD	CS13Z	KS24X	KS24Y
21	0.3587900E 01	0. 1841490E 04	0. 7024030E 06
CD	KS24Z	CS24X	CS24Y
22	0.8954901E 02	0. 1550000E 03	0. 3148030E 04
CD 23	CS24Z Ø. 3203900E Ø1	K535X 0.1841400E 04	KS35Y 0. 7024030E 06
CD 24	KS35Ź 0. 8954901E 02	C535X 0.1550000E 03	CS35Y 0. 3148030E 04
ČD	CS35Z	XLSWA	XLSNB
25	0.3203900E 01	0. 1040000E 03	0. 1040000E 03
CD	RE1X	RE1Y	RE1Z
26	0.000000E 00	0.0000000E 00	0.000000E 00
CD· `	RA1X	RA1Y	RA1Z
27	0.000000E 00	9. 9099998E 99	0.000000E 00
CD 28	RE2X 0.000000E 00	- REŻY · 8. 0000000E 00	RE2Z 0. 0000000E 00
CD	RÁ2X	RA2Y -	RA2Z
29	Ø. ØØ9ØØSŠE ØØ	Ø. Ø86ØØØE OØ	0. 0000000E 00
CD	ŘĚ3X	RE3Y	RE3Z
30	0. 000000ěe 00	0. 0000000E 00	0.000000E 00
CD -	ŘÁ3X	ŘÁ3Y	RA3Z
31 ·	6. 0000000E 00	Ø. 000000E 00	Ø. 0000000E 00
CD	RE4X	RE4Y	RE4Z
32	0.000000E 00	0.0000000E 00	Ø. ØØØØØØE ØØ.
CD	RA4X	RA4Y	RA4Z
33	9. 0999000E 00	0.000000E 00	0. 0000000E 00
CD	RE5X 0. 0000000É 00	RÉSY	RE5Z
34		0. 0000000E 00	0. 0000000E 00
- CD 35 -	0MG1X 0. 0000000E 00	0MG1.Y 0. 0000000E 00	0MG1Z 0.000000E 00
CD	OMG2X	OMG2Y	0MG2Z
36	0, 0000000E .00	0. 0000000E 00	0 0000000E 00
CD -	011Ġ3X 0. 000000ĠE 1981	0. 0000000E 00 '	、 いからさ え

BENDIX RESEARCH LABORATORIES

CD	OMG4X	0MG4Y	0MG4Z
38	8. 8008888 80	0.0000000E 00	0.0000000E 00
CD	0MG5X	0MG5Y	0MG52
39	0. 0000000E 00	0. 0000000E 00	0.0000000E 00
CD	DPH124	DTHT24	DPSI24
40	0.000000E 00	0. 0000000E 00	0.000000E 00
CD	DPHI35	DTHT35	DPSI35
41	0.000000E 00	0.0000000E 00	0.0009000E 00
CD	DPHI12	DTHT12	DPSI12
42	8. 0000000E 00	0.000000E 00	0.0000000E 00
CD	DPHI13	DTHT13	DPSI13
43	0.000000E 00	0.0000000E 00	0.000000E 00
CD	PHI1	THT1	PSI1
44	0.000000E 00	0.0000000E 00	0. 2000000E-01
CD	. RDT1X	RDT1Y	RDT1Z
45	0.000000E 00	0. 0000000E 00	0. 0000000E 00
CD	R1X	R1Y	81Z
46	0.000000E 00	0.0000000E 00	0.0000000E 00
CD	DT	IPRT	TEND
47	0. 5000000E-01	0. 200000E 02	0. 5000000E 02

APPENDIX B

TRANSFER FUNCTIONS FOR SYMMETRIC Z-AXIS WITH STATE VECTOR

$$\mathbf{X}^{\mathrm{T}}(\mathsf{t}) = \begin{bmatrix} \boldsymbol{\omega}_1, \ \boldsymbol{\omega}_{21}, \ \boldsymbol{\omega}_{42}, \ \boldsymbol{\psi}_{21}, \ \boldsymbol{\psi}_{42} \end{bmatrix}$$

Space Construction Base,
 Configuration 1

```
ORIGINAL PAGE IS
OF POOR QUALITY
```

	0.37244E-05 0.00000 0.41150E-05 0.14901E-07
NUMBER OF CONTROLLED STATES ? 5	0.38339E-06
NUMBER OF CONTROLS AND OUTPUTS ? 2,5	DENOMINATOR COEFFICIENTS
LIST INPUT MATRICES ? (NO) YES	0.13228E-01 1.1050 0.42524E-02 0.10295
ENTER INPUT MATRICES DATA FILE. *2AXIS2	9.00000
LIST CALCULATED NUM. & DENOM. PAIRS ? (NO) YES	
NAME OF GENERATED TRANSFER FUNCTION FILE ? *222	**************************
•	OUTPUT 1 INPUT 2
INPUT MATRIX A	NUMERATOR COEFFICIENTS
0.0000E+00 0.0000E+00 0.0000E+00 0.0000E+00	9.0000E+00
0.0000E+00 -0.4765E-02 0.4231E-02 -0.8685E+00	0.1183E+00 0.00000
0.0000E+00 0.4739E-02 -0.2463E-02 0.8660E+00	-0.2365E+00 DENOMINATOR COEFFICIENTS
0.0000E+00 0.1000E+01 0.0000E+00 0.0000E+00	0.0000E+00 0.1322BE-01 1.1050 0.42524E-02 0.10295
0.0000E+00 0.0000E+00 0.1000E+01 0.0000E+00	0.0000E+00 0.00000
INPUT MATPIX E *	************
0.3724E-05 0.0000E+00	- OUTPUT 2 INPUT 1
-0.3724E-05 0.1321E-02	**************************************
0.0000E+00 -0.1321E-02	-0.37244E-05-0.29802E-07-0.88073E-06 0.00000
0.0000E+00 0.0000E+00	0.00000
0.0000E+00 0.0000E+00	DENOMINATOR COEFFICIENTS
·	0.13228E-01 1.1050 0.42524E-02 0.10295
INPUT MATRIX C =	0.0000
0.1000E+01 0.0000E+00 0.0000E+00 0.0000E+00	0.0000E+00
0.0000E+00 0.1000E+01 0.0000E+00 0.0000E+00	0.0000E+00 *******************************
0.0000E+00 0.0000E+00 0.1000E+01 0.0000E+00	0.0000E+00
4 5000E-00	A 0000C+00
0.0000E+00	9.0000E+00

******* NUMERATOR COEFFICIENTS *******

OUTPUT 1 INPUT 1

	S TUPTUO	INPUT	a
*******	** NUMERATOR	COEFFICIENT	5 ******
0.13210E	-02 0.55879E-	05 0.15614E	-03 0.00000
0.00000	Ŧ		
****	DENOMINATO	R COEFFICIE	NTS ********
0.13553E	-01 1.1050	0.42524E	-02 0.10295
0.00009			;
			`
*******	******	******	*****
	OUTPUT 3	INPUT	1
******	NUMERATOR	COEFFICIENT	
0.00000	0.00000	-0.32250E	-05 0.00000
0.00000			
*******	DEMOMINATO	R COEFFICIE	NTS *****
0.1322SE	-01 1.1050	0.42524E	-02 0.10295
0.00000			
******	*****	*******	*****
	OUTPUT 3	INPUT	2
*******	• • NUMERATOR	COEFFICIENT	5
-0.13210E	-02-0.59605E-	07-0.33026E	-05 0.00000
0.00000			
	DENOMINATO	R COEFFICIE	NTS
0.13258E	-01 1.1050	0.42524E	-02 0.10295
0.00000			
*****	**********	*********	******
•	OUTPUT 4	INPUT	1
*******	** NUMERATOR	COEFFICIENT	S ========
0.00000	A STÉRAR	AE-A 2440AE	-07-0.53073E-06
	-0.3/C53E-	.03_0.21430£	-01-0.550135-06
9. 90999	-9.3/C53E-	-03-0.314 <i>90</i> E	-01-06-36-06

```
******************************
        OUTPUT 4
                     INPUT
                            2
******* NUMERATOR COEFFICIENTS ********
-0.18626E-08 0.13210E-02 0.55854E-05 0.15614E-03
 0.00000
----- DENOMINATOR COEFFICIENTS
 0.13228E-01 1.1050
                    0.42524E-02 0.10295
 0.00000
******************************
        OUTPUT 5
                     INPUT 1
******* NUMERATOR COEFFICIENTS ********
. 0.00000 0.00000
                   -0.18626E-07-0:32250E-05
 0.00000
****** DENOMINATOR COEFFICIENTS ********
 0.13228E-01 1.1050
                    0.42524E-02 0.10295
 0.00000
****************
        OUTPUT 5
                     INPUT 2
 ****** NUMERATOR COEFFICIENTS *******
 0.00000 -0.13210E-02-0.35623E-07-0.33024E-05
 0.00000
======= DENOMINATOR COEFFICIENTS ==
```

0.42524E-02 0.10295

0.13228E-01 1.1050

0.00000

APPENDIX C

DERIVATION AND ANALYSIS OF MINIMUM (TRACE $\mathbf{E}_{\mathbf{C}}^{\mathbf{T}}\mathbf{E}_{\mathbf{C}}$) $^{\frac{1}{2}}$ SOLUTION FOR STATE CONTROLLER GAIN MATRIX C

The problem, minimize $|C\underline{x}_j - \underline{y}_j|^2$ with respect to \underline{x} where \underline{x}_j is the jth column of G and \underline{y}_j is the jth column of $A_p + \frac{1}{T}I$, is equivalent to the problem, minimize (trace $E_c^TE_c$) with respect to G where:

$$E_{c} \triangleq A_{c} + \frac{1}{T} I$$

I $\underline{\underline{\Delta}}$ identity matrix of dimension n

Expanding $|c\underline{x}_j-\underline{y}_j|^2$, we have

$$\underline{\mathbf{x}}_{\mathbf{j}}^{\mathrm{T}}\mathbf{C}^{\mathrm{T}}\mathbf{C}\underline{\mathbf{x}}_{\mathbf{j}} - 2\underline{\mathbf{y}}_{\mathbf{j}}\mathbf{C}\underline{\mathbf{x}}_{\mathbf{j}} + \underline{\mathbf{y}}_{\mathbf{j}}^{\mathrm{T}}\underline{\mathbf{y}}_{\mathbf{j}}$$

Taking the gradient with respect to \underline{x}_J , setting equal to zero for a critical value and solving for \underline{x}_j , we obtain

$$\underline{\mathbf{x}}_{\mathbf{j}} = \mathbf{C}^* \underline{\mathbf{y}}_{\mathbf{j}} \tag{C-1}$$

where

$$C^{*\underline{\Lambda}}(C^{T}C)^{-1}C^{T} \tag{C-2}$$

Therefore:

$$G = C^*(A_p + \frac{1}{T} I)$$
 (C-3)

Substituting equation (C-3) into equation (7-23) yields:

$$\underline{x}_{p} = A_{c}\underline{x}_{p} + D\underline{w}$$
 (7-22)

where:

$$A_c = A_p - CC^* (A_p + \frac{1}{T}I)$$
 (C-4)

It was desired that all of the eigenvalues of the controlled plant matrix, A_c , be $-\frac{1}{\overline{T}}$. The c linearly independent columns of C, that is, the vectors $C\underline{\delta}_i$; i=1 to c.

where:

$$\underline{\delta}_{i} = (\delta_{i1}, \ \delta_{i2}, \dots, \delta_{ic})^{T}$$
 (C-5)

 δ_{ij} =the Kronecker delta

are eigenvalues of A_{C}^{T} corresponding to the eigenvalue, -1/T; since

$$A_{c}^{T} C\underline{\delta}_{i} = -\frac{1}{T} C\underline{\delta}_{i} \qquad (C-6)$$

Therefore, at least c of the eigenvalues of $A_{\rm C}$ are -1/T since the number of linearly independent eigenvectors corresponding to a given eigenvalue is not greater than the multiplicity of the eigenvalue and the transpose of a matrix has the same eigenvalues as the matrix.

The rank of the sum of two matrices is equal to or less than the sum of the ranks of the matrices. Furthermore, the rank of a nonzero scalar times a matrix is equal to the rank of the matrix. Hence, we have:

 $\operatorname{rank} A_{\mathbf{C}} \leq \operatorname{rank} \mathbf{R} + \operatorname{rank} \mathbf{CC}^*$

where:

$$R = (I - CC^*)A_p$$
 (C-7)

If M_1 and M_2 are pxr and rxq matrices, respectively, and each is of rank r, then M_1M_2 is of rank r. Hence, the matrix CC* has rank c. If the rank of a square matrix of dimension n is r, then at least n-r of the eigenvalues of the matrix are zero. Furthermore, a necessary condition for linear control system asymptotic stability, that is, for no disturbance, $\underline{x} + 0$ as $\underline{t} + \underline{\phi}$. $\forall \underline{x}(0)$, is that all of the eigenvalues of the controlled plant matrix have negative real parts. Therefore, a necessary condition for R is:

 $rank R \ge n-c$

The rank of the product of two matrices can be no greater . than the rank of either matrix. Thus, if r_{ℓ} of the : columns of A_p are linearly independent and $r_{\ell} \leq n-c$, then the rank of R is less than or equal to n-c. If the jth column of A_{p} is in the range of C, that is, if $\underline{\underline{A}}_{p_i} = \underline{\underline{C}}_{\underline{c}}$ where $\underline{\underline{A}}_{p_i}$ is the jth column of $\underline{\underline{A}}_p$ and $\underline{\underline{c}}$ is a c component constant vector, then the jth column of R is Thus, if r of the columns of A_{D} are linearly independent and r > n-c, then r+c-n of the columns of R will be zero and n-r will be zero or linearly dependent, that is, the rank of R will be n-c. Therefore, for the minimum (tr $E_c^T E_{\vec{c}}$) $^{\frac{1}{2}}$ solution for G to be asymptotically stable, it is necessary that the rank of R be n-c, that is, that n-c columns of the plant matrix must be linearly independent from the columns of C.

APPENDIX D

Algorithm for Generating Optimum State Controller or Estimator Gain Matrix

1. Compute
$$K = C*(A_p + \frac{I}{T}I)$$
 or
$$= (A + \frac{20}{T}I) B^T (B_p B_p^T)^{-1}$$

2. Set
$$\underline{e}_k = n^{-\frac{1}{2}} (1, 1, ----, 1)^T$$

3. Set
$$\lambda_k = 0$$

4. Go to subroutine.

5. Set
$$\underline{e} = \underline{e}_{k+1} / |\underline{e}_{k+1}|$$

6. Set
$$\lambda = \lambda_{k+1}$$

7. Compute
$$\delta = 0.01 \text{ largest} | k_{ij} |$$

9. Set
$$j = 1$$

10. Set
$$k_{ij} = k_{ij} + \delta$$

11. Set
$$\underline{e}_k = \underline{e}$$

12. Set
$$\lambda_k = \lambda$$

13. Go to subroutine.

- 14. Compute $\delta_{ij} = \lambda_{k+1} \lambda$
- 15. Set $k_{ij} = k_{ij} \delta$
- 16. If j = n(m), go to step 19.
- 17. Set j = j+1
- 18. Go to step 10.
- 19. If i = c (dimension of \underline{x}), go to step 22.
- 20. Set i = i+1
- 21. Go to step 9.
- 22. Compute Δ = largest | δ_{ij} |
- 23. Set $K = K \frac{\delta}{\Delta} \left[\delta_{i,j} \right]$
- 24. Set $\underline{e}_k = \underline{e}$
- 25. Set $\lambda_k = \lambda$
- 26. Go to subroutine.
- 27. If $|\lambda_{k+1} \lambda|/\lambda_{k+1} > 0.01$, go to step 5.
- 28. Set G or H = K

SUBROUTINE

1. Compute
$$E = W_c \left(A_p - \frac{1}{T}I\right)W_c^*$$
 or
$$= W_e \left(A - KB + \frac{20}{T}I\right)W_e^*$$

- 2. Compute $\underline{e}_{k+1} = \underline{E}^T \underline{E} \underline{e}_k$
- 3. Compute $\underline{\lambda}_{k+1} = |\underline{e}_{k+1}|$
- 4. If $\lambda_{k+1} \leq 0$, go to step 6.
- 5. If $|\lambda_{k+1} \lambda_k|/\lambda_{k+1} < 0.01$, return.
- 6. Set $\underline{e}_k = \underline{e}_{k+1} / | \underline{e}_{k+1}$
- 7. Set $\lambda_k = \lambda_{k+1}$
- 8. Go to step 2.

APPENDIX E

Derivation and Analysis of Minimum (trace $\mathbf{E_e}^T\mathbf{E_e})^{\frac{1}{2}}$ Solution for State Estimation Gain Matrix H

The problem, minimize $|\mathbf{B}^{T}\underline{\mathbf{x}}_{\mathbf{i}} - \underline{\mathbf{y}}_{\mathbf{i}}|^{2}$ with respect to $\underline{\mathbf{x}}_{\mathbf{i}}$ where:

$$\underline{\underline{x}}_{i}^{T} = ith row of H$$

$$\underline{y}_1^T = \text{ith row of A} + \frac{20}{T}I$$
,

is equivalent to the problem, minimize $(\text{tr E}_e^T E_e)^{\frac{1}{2}}$ with respect to H where:

$$E_{e} = A - HB + \frac{20}{T}I$$

I = identity matrix of dimension A

Expanding $\left| \mathbf{B}^{T} \underline{\mathbf{x}}_{i} - \underline{\mathbf{y}}_{i} \right|^{2}$ yields:

$$\underline{\mathbf{x}}_{\mathbf{i}}^{\mathrm{T}} \mathbf{B} \mathbf{B}^{\mathrm{T}} \underline{\mathbf{x}}_{\mathbf{i}} - 2 \underline{\mathbf{y}}_{\mathbf{i}}^{\mathrm{T}} \mathbf{B}^{\mathrm{T}} \underline{\mathbf{x}}_{\mathbf{i}} + \underline{\mathbf{y}}_{\mathbf{i}}^{\mathrm{T}} \underline{\mathbf{y}}_{\mathbf{i}}$$

Taking the gradient with respect to \underline{x}_i , setting equal to zero for a critical value and solving for \underline{x}_i^T , we have

$$\underline{\mathbf{x}}_{i}^{\mathrm{T}} = \underline{\mathbf{y}}_{i}^{\mathrm{T}} \mathbf{B}^{\mathrm{T}} (\mathbf{B} \mathbf{B}^{\mathrm{T}})^{-1}$$
 (E-1)

where:

$$B = \begin{bmatrix} B_p & 0 & 0 \end{bmatrix}$$
 (7-44)

Therefore:

$$H = (A + \frac{20}{T}I) B^{T} (BpBp^{T})^{-1}$$
 (E-2)

Substitution of (E-2) into equation (7-42) yields:

$$\underline{\dot{\mathbf{x}}}_{e} = \begin{bmatrix}
A_{c}^{-H_{1}B_{p}} & 0 & DB_{w} \\
0 & A_{v} & 0 \\
---- & 0 & A_{w}
\end{bmatrix}
\underline{\mathbf{x}}_{e} + \begin{bmatrix}
D \\
--- \\
0 \\
--- & 0
\end{bmatrix}
\underline{\mathbf{w}}_{k} + \begin{bmatrix}
H_{\dot{1}} \\
--- \\
0 \\
--- & 0
\end{bmatrix}
\underline{\mathbf{y}}$$

where: (E-3)

$$H_1 = (A_C + \frac{20}{T} I) B_p^T (B_p B_p^T)^{-1}.$$
 (E-4)

Since

$$\underline{\mathbf{x}}_{\mathbf{e}} (0) = \left[\underline{\mathbf{y}}^{\mathbf{T}}(0) (\mathbf{B}_{\mathbf{p}} \mathbf{B}_{\mathbf{p}}^{\mathbf{T}})^{-1} \mathbf{B}_{\mathbf{p}} \right] \underline{\mathbf{0}} \left[\underline{\mathbf{0}} \right]^{\mathbf{T}}, \quad (E-5)$$

the estimates for \underline{x}_v and \underline{x}_w and thus the estimates for the unknown part of the control and plant disturbances are zero for all time.

APPENDIX F

EQUATIONS FOR THE FULL BEAM

AND SPLIT-BEAM

EQUATIONS FOR THE FULL BEAM AND SPLIT-BEAM

F.1 Translational equations for the full beam

(i)
$$m\ddot{\mu}_1 + (K+K_1)\mu_1 - K_1\mu_2 - K\mu_3 - (K_{\phi} + K_{\phi_1})\beta_1 - K_{\phi_1}\beta_2 - K_{\phi}\beta_3 = F_{e_1}$$

(ii)
$$m\ddot{\mu}_2 + (K+K_1)\mu_2 - K_1\mu_1 - K\mu_4 - (K_0 - K_0)\beta_2 + K_0\beta_1 - K_0\beta_4 = F_{e_2}$$

(iii)
$$\ddot{\mu_{i}} + (2K+K_{1})\mu_{i} - K\mu_{i-2} - K_{1}\mu_{i+1} - K\mu_{i+2} - K_{0}\mu_{1}$$
 β_{i} $+K_{0}\beta_{i-2} - K_{0}\beta_{1}$ $\beta_{i+1} - K_{0}\beta_{i+2} = F_{e_{i}}$ $\beta_{i} = 3,5,\ldots,2n-3$

(iv)
$$m_{i}^{\mu} + (2K + K_{1})\mu_{i} - K\mu_{i-2} - K_{1}\mu_{i-1} - K\mu_{i+2} + K_{0}^{\beta}i$$

 $+ K_{0}^{\beta}i - 2 + K_{0}^{\beta}i - 1 - K_{0}^{\beta}i + 2 = F_{e_{i}}^{'}i$
 $i = 4, 6, \dots, 2n-2$

(v)
$$\tilde{\mu}_{2n-1}^{\mu_{2n-1}-K_1} \mu_{2n-1}^{\mu_{2n-1}-K_1} \mu_{2n-3}^{\mu_{2n-3}-(K_{\emptyset_1}-K_{\emptyset})\beta_{2n-1}-K_{\emptyset_1}} \mu_{2n-1}^{\mu_{2n-1}-K_{\emptyset}} \mu_{2n-3}^{\mu_{2n-1}-K_{\emptyset_1}} \mu_{2n-1}^{\mu_{2n-1}-K_{\emptyset_1}} \mu_{2n-1$$

(vi)
$$^{m\ddot{\mu}_{2n} + (K+K_1)\mu_{2n} - K_1\mu_{2n-1} - K\mu_{2n-2} + (K_{\emptyset_1} + K_{\emptyset})\beta_{2n} + K_{\emptyset_1}\beta_{2n-1} + K_{\emptyset}\beta_{2n-2}}$$

$$= F_{e_{2n}}'$$

where
$$\mathbf{F}_{\mathbf{e}_{\underline{\mathbf{i}}}}^{'} = \mathbf{F}_{\mathbf{e}_{\underline{\mathbf{i}}}} - \frac{\mathbf{m}}{\mathbf{M}_{\mathbf{T}}} \mathbf{F}_{\mathbf{e}} + \mathbf{m} \mathbf{r}_{\underline{\mathbf{i}}} \mathbf{\omega}_{\mathbf{0}}$$

F.2 Rotational equations for the full beam

(i)
$$J_{\beta_1}^{\beta_1} + K_a \beta_1 + K_b \beta_2 + K_b \beta_3 + (K_{\emptyset} + K_{\emptyset})^{\mu_1 - K_{\emptyset}} \mu_2 - K_{\emptyset}^{\mu_3} = T_{e_1}^{\mu_1}$$

(ii)
$$J_{a_2}^{\beta_2} + K_{a_2}^{\beta_2} + K_{b_1}^{\beta_1} + K_{b_2}^{\beta_4} + (K_{\phi}^{-K_{\phi_1}})^{\mu_2} + K_{\phi_1}^{\mu_1} - K_{\phi}^{\mu_4} = T_{e_2}^{\mu_1}$$

(iii)
$$J_{\beta_{i}}^{\mu_{i}+K_{d}} \beta_{i}^{\mu_{i}+K_{b}} \beta_{i-2}^{\mu_{i}+K_{b}} \beta_{i+1}^{\mu_{i}+K_{b}} \beta_{i+2}^{\mu_{i}+K_{b}} \beta_{i+2}^{\mu_{i}+K_{b}} \beta_{i-2}^{\mu_{i}+K_{b}} \beta_{i+2}^{\mu_{i}+K_{b}} \beta_{i+2}^{\mu_{i}$$

(iv)
$$J_{\beta_{i}}^{\beta_{i}+K_{d}}\beta_{i}^{\beta_{i}+K_{b}}\beta_{i-2}^{\beta_{i}-2}^{+K_{b}}\beta_{i-1}^{\beta_{i}-1}^{+K_{b}}\beta_{i+2}^{\beta_{i}+2}^{-K}\phi_{1}^{\mu_{i}^{i}+K}\phi^{\mu_{i-2}}$$

$$+K_{\phi_{1}}^{\mu_{i}-1}^{-K_{\phi}}\beta_{i+2}^{\mu_{i}+2}^{\mu_{i}+2}^{-K_{\phi}}\beta_{i}^{\mu_{i}^{i}+2}^{-K_{\phi}}\beta_{i}^{\mu_{i}^{i}+2}^{-K_{\phi}}\beta_{i}^{\mu_{i}^{i}+2}^{-K_{\phi}}\beta_{i}^{\mu_{i}^{i}+2}^{-K_{\phi}}\beta_{i}^{\mu_{i}^{i}+2}^{-K_{\phi}}\beta_{i}^{\mu_{i}^{i}+2}^{-K_{\phi}^{i}}\beta_{i}^{\mu_{i}^{i}+2}^{$$

$$(v) J_{2n-1}^{+K} a^{\beta} 2n^{-1} b_{1}^{+K} b_{1}^{\beta} 2n^{+K} b^{\beta} 2n^{-3} (K_{\emptyset_{1}}^{-K} \phi)^{\mu} 2n^{-1} A_{\emptyset_{1}}^{\mu} 2n^{+K} \phi^{\mu} 2n^{-3}$$

$$= T_{e_{2n-1}}^{'}$$

$$(vi) \quad J^{\beta}_{2n} + K_{a}^{\beta}_{2n} + K_{b_{1}}^{\beta}_{2n-1} + K_{b}^{\beta}_{2n-2} - (K_{\emptyset_{1}} + K_{\emptyset})^{\mu}_{2n} + K_{\emptyset_{1}}^{\mu}_{2n-1} + K_{\emptyset}^{\mu}_{2n-2}$$

$$= T_{e_{2n}}^{'}$$

where
$$K_a = K_{\theta} + K_{\theta_1} + K_{\psi} + K_{\psi_1}$$

$$K_d = K_{\theta} + K_{\psi} + K_a$$

$$K_b = K_{\psi} - K_{\theta}$$

$$K_{b_1} = K_{\psi_1} - K_{\theta_1}$$

$$T'_{e_i} = T_{e_i} + \gamma_i F_{e_i} - J_{\phi_0}$$

- F.3 Translational equations for the bodies involved in the connection of half-beams
 - $\begin{array}{lll} \text{(i)} & & \text{m}\ddot{\mu}_{n-1} + \text{m}\overset{\circ}{\epsilon}_{n-1}\ddot{\beta}_{n-1} 0.5K\mu_{n+3} 0.5K_{1}\mu_{n+2} + 0.5(K+K_{1})\mu_{n+1} \\ & & -0.5K_{1}\mu_{n} + 0.5(K+K_{1})\mu_{n-1} 0.5K\mu_{n-3} 0.5(K_{\emptyset} + K_{\emptyset_{1}})\beta_{n+1} \\ & & -0.5K_{\emptyset_{1}}\beta_{n} 0.5(K_{\emptyset_{1}} K_{\emptyset})\beta_{n-1} + 0.5K_{\emptyset}\beta_{n-3} 0.5K_{\emptyset}\beta_{n+3} 0.5K_{\emptyset_{1}}\beta_{n+2} \\ & & = & F^{'}_{e_{n-1}} \end{array}$

(ii)
$$\begin{split} & \text{m}\ddot{\mu}_{n} + \text{m}\overset{\circ}{\epsilon}_{n} \ddot{\beta}_{n} - 0.5 \text{K} \mu_{n+4} + 0.5 (\text{K} + \text{K}_{1}) \mu_{n+2} - 0.5 \text{K}_{1} \mu_{n+1} \\ & + 0.5 (\text{K} + \text{K}_{1}) \mu_{n} - 0.5 \text{K}_{1} \mu_{n-1} - 0.5 \text{K} \mu_{n-2} + 0.5 \text{K} \phi_{1} \beta_{n+1} \\ & + 0.5 (\text{K}_{\phi} + \text{K}_{\phi_{1}}) \beta_{n} + 0.5 \text{K} \phi_{1} \beta_{n-1} + 0.5 \text{K} \phi_{n-2} \\ & + 0.5 (\text{K}_{\phi} + \text{K}_{\phi_{1}}) \beta_{n} + 0.5 (\text{K}_{\phi} - \text{K}_{\phi_{1}}) \beta_{n+2} = \overset{\circ}{\text{F}} \overset{\circ}{e}_{n} \end{split}$$

(iii)
$$\begin{split} \text{m}\ddot{\mu}_{n+1} + \text{m}\ddot{\varepsilon}_{n+1}\ddot{\beta}_{n+1} &-0.5 \text{K} \mu_{n+3} - 0.5 \text{K}_1 \mu_{n+2} + 0.5 (\text{K} + \text{K}_1) \mu_{n+1} - 0.5 \text{K}_1 \mu_{n} \\ &+ 0.5 (\text{K} + \text{K}_1) \mu_{n-1} - 0.5 \text{K} \mu_{n-3} - 0.5 (\text{K}_0 + \text{K}_{0_1}) \beta_{n+1} - 0.5 \text{K}_{0_1}\beta_{n} \\ &+ 0.5 (\text{K}_0 - \text{K}_{0_1}) \beta_{n-1} + 0.5 \text{K}_0 \beta_{n-3} - 0.5 \text{K}_{0_1}\beta_{n-2} - 0.5 \text{K}_0 \beta_{n+3} &= \text{F}_{e_{n+1}}' \end{aligned}$$

F.4 Rotational equations for the bodies involved in the connection of half-beams

(ii)
$$J_{\beta_n} - J_{\beta_{n+2}} = J_{\omega_{02}} - J_{\omega_{01}}$$

(iii)
$$J_{\beta_{n+1}} - J_{\beta_{n-1}} = J_{\omega_{0_1}} - J_{\omega_{0_2}}$$

where

$$J_{1}^{*} = J_{2}^{*} = m \stackrel{\sim}{d}_{13} \stackrel{\sim}{\epsilon}_{n-1}$$

$$d_{1}^{*} = -d_{4}^{*} = \frac{1}{2} (\stackrel{\sim}{d}_{12} - \stackrel{\sim}{d}_{31})$$

$$d_{2}^{*} = -d_{3}^{*} = \frac{1}{2} (\stackrel{\sim}{d}_{12} - \stackrel{\sim}{d}_{13})$$

$$K_{\psi_{11}} = -d_{1}^{*} \quad K_{1} \quad \stackrel{\sim}{d}_{12} = K_{\psi_{14}}$$

$$K_{\psi_{12}} = -d_{2}^{*} \quad K_{1} \quad \stackrel{\sim}{d}_{12} = K_{\psi_{13}}$$

APPENDIX G

MODE SHAPES OF THE NATURAL FREQUENCIES FOR THE ORIGINAL BEAM

M. 1.74	
3	
5	
Š.	
÷	
×	

		NA LURA	L FREDUENC	.582178	E+U2							
TX	1 K Ihag	IY Real	TY . Imag	TZ REAL '	T Z E MAG	RX REAL	RX IHAG	RY	L SAPI	REAL_	RZ IMAG	·
33024E+0J	0.06000	.23506E-12	0.00000	.44892C~12	0.00000	.17900E-13	0.00000	19128É-1Ž	0.00000 ¯	-, 97421E-0	<u>i</u> o o o o o	00
330245+00	0.00000	.1d507E-12	0.00000	.430096-12	0.00000	12107E-14	0.00000	19146E_12 _	~ 000 0 0	<u>-</u> ,97421E-(0.000	00
13612E+00	J.00000	.19979E-12	0.00000	.41581E-12	0.00000	254466-13	0.00000	14710E-12	0.00000	928006-0	i0.000	<u>0</u> 0
13612E+00	ŭ.00000	-21906E-12	0.00000	.425166-12	0.00000	11676E-13	0.00000	16659E-12	0.00000	92806E-0	j0.000	<u>ດດີ [</u>
-40347E-01	0.00000	.22347L-12	0.00000	.4260>E-12	0.00000	231426-13	0.00000	15103E-12	0.00100	7aîl6əL-0	i_ o.ooo	จัด 📜
.403478-61	0.00000	+222198-12	0.00000	.424565-12	0.00000	108906-13	0.00000	16981E-12	0.00000	-,78165£-0	1_ 0.000	33, _
.176025+00	0.00000	.2554912	0.00000	.388716-12	0.00000	15673E-13	0.00000	97336E-13	0.00000	524946-0	1 0.003	စ္စင့္ ု
-17602E+UO	0.00000	.1808dr-12	0.00000	. 193164-12	0.00000	21793E-13	0.00000	10153E-12	u_00000 ¯	524946-0	1. 0.000	อง_ี_ี
.24998t+00	0.00000	-27174E-12	0.00000	J17086-12	0.00000	~41159£-13"	0,0000	[-11]1196-12	0.00000	- <u>,</u> 185196-0	o cg.o i	<u> </u>
.24998E+0J	0.00000	.183651-12	00000.0	:320136-12	0.00000	43248E-13	0.00000	11533E-12_	0.00000	16519E-0	ir " 0•00'0	ôο [
24998E+00	0.03000	.2d040E-12	0.00000	~.20839E-12	0.00,000	=.64140E-13	0.00000	11087E-12_	0.00000	•1971èE-0	10.000	00
.24998E+00	0.00000	.17390L-12	0.00000	.20150E- <u>12</u>	0.00000	04916E-13	j.00000	107616-12	0.00360	.185198-0	าั <u>้</u> อ.งดอ	00_
176026+00	0.00000	-30439E-12	0.00000	.69439E-15	6.00000	72611£-13	_0.00000	~.11264E-12	0.00000	52494E-C	<u>r _ o</u> _000	ō <u>o</u>
-17602E+00	0.00000	.15919L-12	0.00000	•65218E-13	,0.00000	762976-13	0.00000	10572E-12 ~	ŭ. 00000 <u>0</u>	52494E-(<u>ir0*0000</u>	<u>0</u> 2
-40347E-01	0.00000	.30699E-12	0.00000	-,ïooooe-12	0.00000	73817E-13	0.00000	003254-13	£.00000	.7dlb5E-0	ji j ožóbo:	o๋ก <u>ั</u>
-40347E-01	0.00000	.14783L-12	0.00000	983666-13	~0.00000	744898-13	0.00000	927616-13_	v.00500¯	761656-0	<u>ir] 0.0</u> 000	90
136128+60	0.00000	.313576-12	0.00000	26887E-12	0.00000	78/78E-i3	0.00000	~.90483E-13	0.00000	,9230ot-0	11 0,000	ัง <u>ขั</u>
13615E+00	0.00000	,1>218E-12,	_0.00000	4.50803F-TS	0.00000	8123oE-13.	0.00000	93835E-13_	0.00000	*a\$\$0e£;-0	10.000	<u>jo[]</u>
330248+00	0.00000	.307781-12	0.00000	43672£-12	.0.00000	799d8E-13	0.60000	773684E-13	0.00000	.974Z1L-(1 0.000	02
330248.00	0.00000	.15372E-12	0.00000	439076-12	0.00000	815891-13	-0.00000	67896E-13	0.00000	. 47.42 LE-0	ກ້. ລະບວລ	òōŢ

" NATURAL	FÁEGULNCY*	-102354E+03
-----------	------------	-------------

TX TY	TY TZ	TZ TZ	RX RX RX	REAL	KY RZ	RZ IHAG
31516E-12 0.00000 .76616E-						
10627E-Li _0.0000078616E-	01 0.00000 .316/8E	[000000]	847748-01 0.00000	67659E-12	0.00000 .62450E-1	0.00000
31959E-12 0.00000 .73579E-	01 0.06000	00 0.00000	d3511E-01 "0.00000"	60407E-12	0.00000 .11193E-L	3 0.00000
85837E-120.0000073599E-	01 0.00000 1.13696L		835116-01, 0.00000	58525E-12	0.000091650F-J	3 0.0000
25727E-12 0.0000061146E-	Q1` 0.00000 <u>-</u> .35149E-	-0î0.00009,	72074E-01 0.00000	~.47129E-12	0.0000038747E-1	3_0.0000
-69870E-12 0.0000061146E-	01 0.6000035149E-	-31 0.00000	72074-01 _0.00000	462746-12	v.00000	2 0.00000
63464E-13 0.00000 .40736E-	01 0.00000 171546	•uo 'o.ooòoo" =:	.490802-01 0.00000	30735E-12]	0.00000 921236-1	3 0 - 0 0 0 0 0
	01 0.0000017154E	•au	49080E-01 0.0000	31459E-12	0.00000 .51963E-1	3 0.00000
	01 0.00000 - 24704E	00 _0.00000	1/422E-01 0.00000	88757E-13	0.0000011787c-1	2 0.00000
.38924E-12 0.0000014314L-	01 0.0000024704E	+00 0.00000	.1/4226-01 0.00000	1033/1-12	0.00000469532-1	3o.oonoo_
	01 0.00000 <u>-</u> .24704E	•00.00000	174228-01 0.00000	1,22096-1,2	0.00000 81230E-1	3 0.00005
	01 0.0000024704E	00 0.00000 .	174226-01 0.0000	10819E-12	0.00000 .854736-1	3 0.00000
-61793E-12 0.0000040736L-	-01 0.0000017154E	. 00000.0 0 00	.49030E-01 0.00000	-34900E-12	0.00000 <u>-44726</u> £-1	3 0.0000
56045E-13 0.00000 .40/36E-	01 0.00000171548	+00 0.00000 ,	.49080E-01 0.00000	.33856E-12	0.00000968018-1	
69625E-12 0.0000061146E-	-01 0.000 <u>0035149E</u>	-01_0.00000	.72074E-01, 0.00000	49157E-12	0.0000024159E-1	4 0.00000
	·01 0.00000 35149E				0, 00000 - 95940 <u>-</u> 1	
	-01 0.00000 .13696Ē	• <u>0</u> 0 0.00000 .	.835116-01 ^0.00000	-63042E-12	0.0000047046E-	3 0.0000
58170E-12 0.00000 .73599E-	-01 0.00000 .1369bE	+00 0.00000	.83511L-01 0.00000	.62428E-12	0.0000010791=-	2 0.00000
-52179E-12 0.0000078616E-	-01, 0.00000 .31678E	+00 0.00000	.84774E-01 0.00000	.691678-12	0.0000091322E-	30•00000
78664E-12 0.00000 .78016E-	-01 0.00000 .316786	•00 0.00000 .c	.84774L-01 0.00000	67920E-12	0.00,00098,788=_	30.000000

	,NATUR	T EKFÖNFÄCK*	.125539E+03					
TX TX TX	TY KEAL	TY """ "	TZ TŽ REAL JHAG,	KEAL KEAL	RX H IHAG RE	RÝ RÝ	RZ KEAL I	HAG
22354E+00 0.00000	18766E-12	0.000007	5533E-12 0.0000	0 -12264E-12			737/0E-02 0	00000
.22354E+00 0.00000	100718-12	0.000007	7460Ê-12] j. 0000	0 129282-12	0.00000 -219	74 E 00 7 0. 0000	73770E-02 0.	<u>.0000</u>
19912E+00 0.00000	15666c-12	0.000004	8719Ë-12° 0.0000	0 •1449ob-12	0.00000 L96	642-00 0.0000	ว ู้ =ั•นั่รวิช36= <u>์ดิ</u> นไ ดูโ	00.050_
,19912E+00 `0.00000	.84086£-13	0.000004	93446-15, 0.0000	0 .16226E-12	0.00000196	64E+00 0.00090	. 15383F-010	• ດດວ່ນກຸ້
15772E+00 0.00000	13927L-12	0.000001	66211-12 0.0000	0 .16836E-12	0.00000155	59E+00 0.00 <u>0</u> 00	18413E-01 0	.00000_
15772E+00 0.00000	.73263E-13	0.000001	6674 <u>È-12</u> 0.,0000	0137436-12	~0.00000 ~	59E•00° 0,00000)	•ំ ០១ ០០ ក្
10123E+00 0.00000	10343E-12	0.00000 7 -1	e oʻqiE−15 ′n•0oʻoʻo	0 .121796-12	0.00000998	000E-01 _0°0000	7 =.23107E-01 0.	.03500_
10123E+00 0.00000	.986346-13	ο•οοοόα ˙•T	4691E-12 0.0000	0 .123276-12	0.00000998	1001-01 <u>0</u> .0000	231078-01 0	00000
34880E-01 0.00000	686508-13	6.000000	8778E-12 -0.000	0 .79764E-13	0.00000 143	379E-01] 0.0000	025603E-010	00000
34889E-01 _ 0.00000]-358426-13	0.000003	8865 <u>E-12</u> 0.0000	0 .86219E-13	0.00000343	3798-010,00000		03000
-34880E-01 0.00000	66851E-15	0.00000	8409E-12~~0.0000	0 .79123E-14	0.00000 .343	798-01 0.0000		00000
-34880E-01 0.00000	11260E-13	[0.000004	84236-12 [0.0000	038149E-14	0.00000 343	179E-07. 0*00000	25603E-01 0.	00000
010123E+00 0.00000	33282E-13	0.00000	<u>09</u> 26E <u>∓</u> 12 <u>. 0</u> .0000	078530E-13	0.00000 77.998	ιοόε=οί <u>τ΄ ο"</u> οοδό <u>ς</u>	23107E-01 0.	.00000
10123E+00 0.00000	547446-13	0.00000 .4	0942E-12 U.0000	0 407776-13	0.00000 77 .998	100È-01 *0.00000	23107E-01 0.	
	111866-12	_ 0 • 0 ō 0 0 0 0 · T	<u>8</u> ģ29 <u>E-1</u> 20.0000	0132146-12	0.00000 .155	238400 0 0 00000	1d413e-01 0.	.00000
15772E+00 U.00000	116496-12	0.000001	7932E-12 0.0000	0138651-12	0.00000 1.155	59E+00 0.0000	.18413£-01 0	.000000
19912E+00 U.00000	.15016b-12	`0.00000ì	63946-12 0.000 <i>0</i>	016729E-12	0.000001196	646,00 0.0000	123d3E_010	• ი ი პ ი ი ়
19912E+00 0.00000	154636-12	0.000001	6328E-12 0.0000	015780E-12	~0.00000 . ,196	64E+00 0.0000	. 12383E-01 <u>-0</u>	00000
2,2,354E+00 .0.00009	. 151900-12	0.000005	38326-12 _0.0000	0017>18E-12		74£ +00 0.00000	73/70E-02 0.	00000
22354E+00 0.00000	15791E-12	0.000005	38208-12 0.0000	01/531E-12	0.00000 .214	774E+00 0.00000	.73770E-02 0.	00000

NA THRAI	FREQUENCY=	.151409E+03
TANIONAL	LVE AOF NO! -	47374017.03

		NA TURA	L FREQUEN	CY=151409	PE+03	+					
TX REAL	XT DAM1	T Y	TY IHAG	TZ REAL	TZ 1mag	KX Real	RK IHAG	RY PEAL	IHAG	RZ REAL	RŽ LIHAĢ
25021E+00	0.00000	41304E-13	0.00000	12909E-12	0.00000	87225L-14	0.00000 _	57051E-12	0.00000	.15155£÷00,	_0.00000
25021E+00	0.00000	78432E-14	0.00000	113608-12	0.00000	12384E-13	0.00000	58822E-12	_ 0.00000	15155£ 00	0.00000
45077E-01	0.00000	171114-13	0.00000	11016E-12	0.00000	.31d22t~14			0.00000	-	
45077E-01	u.00000	11525L-13	0.00000	108716-12	0.00000	.367488-13	0.00000	44250E-12	0.00000	•15380E+00	0.00000
23879E+00	0.00000	340426-13	0.00000	62174E-13	0.00000	.42619L-13	0.30000	→.24055E-12	_ ŭ. 00 0 0 0	•232695==01	0.00000
23879E+00	`v.òòooo	72684E-14	0.0000g	63381E-13	_0.00000	. +19044E-13,	0.00000	23783E- <u>1</u> 2	_ 0.00000	.53569E-01.	
25604E+00											
25664E+00	0.00000	.15392 E -13	[6106000]	26950E-14	0.00000	.21538L-13	_0.00000	810276-13			0.00000
10818E+00	0.00000	135796-13	្តីច•្នុំ១១១១ភ្ជុំ	67801E-13	0.00000	~22367E-13	0.00000	.30240Ē-13	0.000000	. 9530(5 <u>F</u> -01	0.00000
10818E+00	.0.00000	,12076±+13	_0.00000		~ 0.0000à	~~.24485É-13	0.00000	-41292E-13	0.00000	.92302E-01	0.00000
0818E+00	0.00000		_0.00000	115416-12	0.00000	-11550t-13	0.00000_	140484-12		923028-01	0.00000
10818E+00	0.00000	.104386-13	0+63808		0.00000	.85977E-14	0.00000	13238E-12		• 35 105F - 0T	0.00000
-25664E+00	0.00000	.205575-13	0.00000			72863E-14	0.00000	17142E-12		· 33033E-01	0.0000
-256a4E+00	0.00000	-•15f8aF-j1 <u>ÿ</u>	្នំ០ • ឃុំ០០០ថ្ងំ	11587E=12	0.00000	90409E-14	0.00000	17711E-12	_0.00000	_33033E_0,t	0.00000
23879E+00	0.00000	36234E-13	0.00000		0.00000	33719E-13	[0.00000 "	18109E-12		.53568E-01	0.0000 <u>0</u>
23879E+00	0.00000	16520E-13	0.00000	67429E-13	0.00000	352748-13		i7793E-12	0.00000	.53568E-01	_0.00000
45077E-01	0.00000	-352641-13	0,00000	17475E-13	0.00000	4 10596-13	0.00000	14074E-12	0.00600 [12380E+00	0.00000
45077E-01	0.00300	24594E-13	៦ • ១ ១ ១ ១ ភ្លួ	1 <u>7</u> 39 <u>9</u> E- <u>1</u> 3	_ 0.00000	,494416-13	_0.00000	.15701E-1		i2380E+00	0.00000
25021E+U0	0.00000	.51266E-13	0.00000	119386-12	0.00000	,45/53L-13	0.00000	10222E-i	o.joo	151554+00	0.00000
25021E+00	. 0.00900	34450L-13	0.00000	11934É-12	_ 3.00000	45136t- <u>1</u> 3	o•00000	87843E~1.	0.00000	.15155e+00	0.00000

```
TZ TZ RX RX IHAG REAL IHAG
73557E-13 0.00000 -.10536£+00 0.00000 -.22456E+00 0.00000 .12476£+00 0.00000 .72586E-13 0.00000 .232606-13 0.00000
                     10536E+00 0.00000 -.22956E+00 0.00000 .12496E+00 0.00000 .11061E-12 0.00000 .12916E-13 0.00000
---99821E-13 0.00000
                    -.86253E-01 0.00000 .44973E-01 0.00000
                                                           .10898E+00 0.00000 .31877E-13 0.00000 .27681E-14 0.00000
--.90368E-14 0.00000
                     -862531-01 0.00000 .44973E-01 0.00000
                                                           .10498E+00 0.00000 .26037E-13 0.00000 -.14777E-13 0.00000
--- 50689E-13 0.00000
-74290E-13 0.00000 -.47082E-Ci 0.00000 .23930E+00 0.00000 .52710E-01 0.00000 .76948E-16 0.00000 .37080E-13 0.00000
                    _.4708ZE-01_0.00000__.23930E+00_0.00000 .52710E-01_0.00000, .46746E-14_0.00000 _-.22046E-13 _0.000000
---92464E-13 0.00000
--.13750E-12 0.00000 --.14401E-02 0.00000 -.26101E+00 0.00000 --.21327E-01 0.00000 --.44402E-13 0.00000 -.26490E-13 0.00000
                    .14401E-02 0.00000 .26101E+00 0.00000 -.21327E-01 0.00000 -.51447E-13 0.00000 -.3041E-14 0.00000
--18732E-13 0.00000
                     .29239L-01 0.00000 .11078L+00 0.00000 -.73073E-01 0.00000 -.67392E-13 0.00000 1.15801E-13 0.00000
-.55179E-14 0.00000 -.29239E-01 0.00000 11078E+00 0.00000 -.73073E-01 0.00000 11362E-12 0.00000 1349E-14 0.0000
                     .29239E-01 0.00000 -.11078E+00 0.00000 -.73073E-01 0.00000 -.95848E-13 0.00000 -.33960c-13 0.00000
---14487E-12 0.00000
-.6531as-13 0.00000 -.27239E-01 0.00000 -.11078E+00 0.00000 -.71073E-01 0.00000 -.97707E-13 0.00000 -.30778E-13 0.00000
-.23899E-13 0.00000 -.14401E-02 0.00000 -.26101E+00 0.00000 -.21327E-01 0.00000 -.37505E-13 0.00000 -.33131E-13 0.00000
69840E-13 0.00000 144016-02 0.00000 261018-00 0.00000 -21327E-01 0.00000 244819E-13 0.00000 26797E-13 0.00000
                                                                               .27954E-13 0.00000 -.45212E-15 0.00000
 .43022E-13 0.00000 --.47082E-01 0.00000 -.23930E+00 0.00000
                                                           .52710E-01 0.00000
                                                           .52710E-01 0.00000 .26759E-13 0.00000 .63708E-13 0.00000
--11795E-13 0.00000 .47082E-01 0.00000 --23930E+00 0.00000
-34253E-13 0.00000 -.86253E-01 0.00000 -.44973E-01 0.00000
                                                           .108986+00 0.00000 .714526-13 0.00000 .205256-13 0.00000
_-.15086E-12 0.00000
                                                                                .64051E-13 0.00000 .90780E-13 0.00000
                     .862536-01 0.00000 --44973E-01 0.00000
                                                             -13498E+00 0.00000
                                                                                .97716E-13 0.00000 .27731E-13 0.00000
.23973E-13 0.00000 -.10536E+60 0.00000
                                                             -12496E+00 0.00000
                                         .22956E+00 0.00000
                                                             .12496E+00 0.00000 .98913E-13 0.00000 .44522E-13 0.00000
 --25547L-12 0.00000
                     .10536r+00 0.00000
                                         .22956E+00 0.00000
```

" NATURAL FREQUENCY= -225557E+03

TX REAL	TX IHAG 7	TY "	TY THAG	TZ REAL	TZ IHAG	KX	AX	REAL	YA	KEAL _	RZ I HAG
•22113E+0ō	0.00000	369420-13	0.00000	13567E-12	~0.00000	462514-13	0.00000	~20756E+00	0.00000	~29047E=01	0.00000
22113E+00	0.00000	74210E-13	0.00000	-,144888-12	0.00000	.506566-13	_ 0.00000	~20756E+00	0.00000	29049E_01	0.0000
£12808E+03	0.00000	109076-13	0.00000	71271E-13	0.00000	.502665-13	0.00000	+12300E+00	0.00000	~ .43154t-01	0.00000
12808E+00	0.00000	.24951E-13	0.00000	43642t-13	0.00000	544336-13	0.00000	.12J00E+U0	0.00000	43154E-01	
36490E-02	0.00000	.57650E-14	0.00000	.48886E-14		791098-14	0.00000	29158E-02_	0.00000	\$0.103E-01	
<u>_</u> 36490E-02	0.00000	-23870E-13	0.00000	43226E-14	၁ - ဝဂုပ်ဝဝ	19484E-13	_0.00000	29158E-02	0.00000	-,501,09E-01	0*00000
±-13300E+00	0.00000	192714-13	0.00000		<u></u>	661346-14	o• <u>`</u> 00000	12604E+00	0.00000	40095E_01	0.00000
13300£+00	_o.ooooo_	.233906-13	0.00000	. 3 79948-13	0.00000	.50052E-15	0.00000	12604E+00	្តី ០. ឲ្យ១០០	40095E-01	_ 0 • 0 ๋n ơ ơ ở Ž ¯
21257E+00	0.00000	39011e- <u>1</u> 5	0.00000	27128E-13	0.00000	43 1486-14	0.00000	Z0161E+00	ີ່ ປຸດດວດດີ	.15271E-01	0.00000
21257E+00	_0.00000 _	7&350E_14,	0.00000	2983AE-13	_0,00000	110176-14	0.00000	20161E+00	0.00000	15271E-01	
212576+03	0.00000	60060E-14	ຼືດ.ດວດວວີ	11563E-1J	_0.00000	12105E-13	0.00000	-120161E+00	ີ ປ. 000 00	15271E-01	0.00007
-21257E+00		74996E-14	0.00000	<u>-,11434£-1</u> 3	0.00000	1 <u>407</u> 12-13	0.00000	20161E+00	0.00000	.15271E-01	
13300£+00	0.00000	21942E-13	0.00000.	=-41146L-13	0.00000	1,1414L-13	0.00000	12604E+00	0.00000	40095E-01	0.00000
								12604E+00			
36490E-02	0.00000	21579c-13	0.00000	41963Ê-13	0.00000	10385L-13	. 0.00000	29158E-02	0.00000	50109£_01	0.00000
.36490E-02	0.00000	154846-13	0.0000	41368E-13	0.00000	-80864E-14	0.00000	29158E-02	0.00000	•50109E-0	0.0000
•12808E+00	0.00000	47996E-13	0.00000	11672E-13	0.00000	. 12407E-13	0.00000	+12300E+00	0.00000	431546=0	
##12808E+00	3.00000	157936-14	_0.00000	~.117226-13	0.00000	i3802E-13	0.00000	•12300£+00	6.000,00	43154 <u>E</u> -0	เ "จะจือออ๋อ๋
.22113E+00	0.00000	425116-13	0.00000		0.00000	.20842E-13	``ō.oʻoooo	~\$20756E+00	_0.00000		0.00000
22113E+00	0.00000	33967E-14	0.00000	37014E-13	0.00000	.20690E-13	_ 0,00000		_0.00000	24047 <u>6</u> -0	0.00000

NATURAL FREQUENCY= .2755545+03

TX REAL	TX TY TY HAG KEAL	TY TZ TZ	KĒĀL .	RX RY RY IMAG REAL	RZ RZ IHAG KEAL IHAG
		0.00000			0.00000 <u>1.13</u> 034 <u>5.00 0.03030</u>
		0.00000 . 156028-12 0.00000		0.0000030011E-12	0.00000 .14048F+00 0.00000
16829E+G0		0.00000 -#3018E-13 0.00000		0.0000015557E-12	0.00000 .11037c+00 0.00000
16829E+03		0.00000553018-13 0.00000		0.0000012216E-12	0.00000 1110376+00 0.00000 1
		0.0000042213E-130.00000		0.0000068313E-13	0.0000040052E-01 0.00000
241916+00		0.0000037223E-13 0.00000		0.00000 -572216-13	0.00000400524-01 3.00005
145758-01	0.00000 .200816-13	0.00000411876-13 0.00000	12179=-13	\$1-34441. 00000.0.	0.0000012673E±00 0.00000
14575E-01	U.0000023425L-13	0.00009 .316276-13 0.00000	10934E-13	0.00000 .10476E-12	0.0000012673:+00 0.00000
-24400E+00					0.0000067446E-01 0.00000
-2440GE+00	0.0000027227E-L3	0.00000 .18625E-13 0.00000	435875-14	0.00000 .131658-12	0.00.0067446E-01 0.00000
-24400E+00	0.0000019324E-14	0.00000 7.717626-14 0.00000	16751E-13	0.00000 .56015E-13	0.00000 .67446E-01 0.00005
-24400E+00	0.0000012863E-14	0.00000789716-14 _0.00000	11977£-13	~ 0.0000064820E-13 _	0.00000 .67446 -01 0.0000
14575E-01	0.00000 .182116-13	23102E-140.0000) 39400L-14	.0.00000 10257E-13	0.00000 126732+00 0.00000
14575E-01	0.00000 .45114E-14	0.00000 22863E-14 0.0000	5749lC-14	0.0000068127E-14	0.00000 .126735.00 0.00000
24191E+00	0.00000 .22756E-13	~ 0.00000 ~89446Ē-Ī4 J.0000	.54082E-14	0.00000313876-13	0.00000 [.40052E_01 0.00000
241918+00	0.00000 " .69393E-14	0.0000092608E-1-1 0.0000	0 .47604E-14	0.00000316011-13_	0.00000 .40052E-01 0.00000
168292+00	0.00000 .289178-14	0.0000024765E-14 0.0000	0 "540476-14	0.0000038464E-13	0.00000110376+00 0.00000
16829E+00	0.0000031753L_13	_0.0000024499E_140.0300	064565 <u></u> =-14	_ 0.0000029961E-13_	0.00000110376+00 0.00000
1807JE+G0	0.00000 .175731-13	0.00000 .10604E-13 0.0000	.72935E-14	0.00000 .45128E-13	0.00000190985.00 0.00000
18078E+00	0.00000 .196315-13	0.0000010947E-13 v.0000	068888E-14	0.0000026366E-13_	[0.00000+14038F+000.00000_

N.A	THIDAL	FREQUENCY=	-291931E+03
	FOVAL	- KT AOCUCL -	*4AFA31F#A3

TX	TX TY REAL	TY TZ TZ	. KEAL	RX RY IHAG REAL	RY RZ RZ IHAG REAL IHAG
		0.00000 .92622E-13 0.00	000 .113266-12	0.00000 -43073E-13	0.00000 55990E-13 0.00000
26233E-13	0.00000 315331-00	0.0000078986E-13 0.00	u0011849E_15		0.00000 .59738E-13 0.00000
38200E-13	0.00000201761+00	0.00000 .305200-12 0.00	000 +36647E-13	0.00000 -402966-13	0.005u0 30845E-13 0.00000
84762E-13	0-0000024176-+00	0.00000 3.30048E-12 0.00	000 .715636-13	0.00000 .326451-13	0.00000 33452E-13 0.00000
12229E-12	0.0000022361E+00	0.0000026404E-12 -0.00	000645H0E-13	0.00000 .21874E-13	0.0000089906E-14 0.00000
147836-12	0.0000022361E+00	0.00000 [.25896E-12 0.00	00055067£-13	0.00000 79022E-15	0.0000063130E-14 0.00000
~•24597E-13	0.00000143562+00	0.00000 86709E-13 0.00	00011a55E-12	0.00000 .25774E-13	0.0000042029E-13 0.00000 "
67176E-13	0.0000014356E+00	0.0000085345E-13 0.00	00013086E-12	0.00000 .72138E-14	0.00000520645-13 0.00000
11057E-12	0.00000 - 494676-01	0.00000 - 44617E-12 0.00	000 <u> </u>	_0.0000045773E-13	0.0000058469E-13 0.00000
.21337E-13	0.00000494598-01	0.00000433736-12 0.00	U0040109L-13	0.00000 .64022E-13	0.0000043468E-13 0.60000
-195568-12	0.00000 .49469E-01	0.0000U32671E-12 0.00	000 .13177E-12	0.00000 .682106-13	0.00000 27696E-13 0.00000
53362E-13	0:00000 43494F-01	0.00000 29492E-12 0.00	000 13004E-12	0.00000 73932E-13	0.00000 .18177E-14 0.00000
+47057E-13	0.00000 T. 14356E+00	0.0000022309E-12 0.00	000 -14742E-12	0.00000 ~ .2563JE-13	0.00000 .10257E-12 0.0000
64273E-13	0.00000 .14356L+00	0.00000 .19367E-12 0.00	000 -16778L-12	0.00000 .267508-13	0.00000 [.27942E-13 0.00000
180516-12		0.00000536036-12 _ 0.00	000949128-14	0.0000033954E-13	0.00000 .557886-13 0.30000
86254E-13	0-0000055191E+00,	0.0000055405E-12 0.00	000 44380E-14	0.0000036861E-13	0.0000013069E-13 0.00000
19441E-12	U.00000,2d176E+00,	0.0000032509E-12 0.00	00023950E-iz	0.00000 959086-13	0.0000034608E-13 0.00000
_=.11817E-13	0.000000 .281766+00	0.00000 31917É-12 u.00	00025379E-12	0.0000097033E-13	0.00000 -1102276-12 0.00000
68973E-13	0.00000 *31533E+00	0.0000040688E-15_0.000	J0035549t-12	0.0000014737E-12	0.0000036354E-13 0.00000
-21170L-12	J-00000 -31233£+00	0.000004222LL-12 0.000	21-368448- 000	0.00000155418-12	J.0000094203E-13 0.00000 -

NATURAL FREQUENCY= .363684E+U3

TX , REAL	TX IMAG.	TY _ keal	TY, 1HAG	REAL	TZ I HAG	RX REAL [RX	RY - REAL	RY RZ RZ RZ IMAG IMAG
92605E-13	0.00000	-12219E+00	0.00000	.16307E+00	0.00000	15552E+00	0.00000	72452E-13	0.0000016384E-13 0.00000
*13025E-12	0.00000	12219E+00	0.00000	16307E+00	_0.00000	15552Ê +00	0.00000	11424E-12	0.00000 1.17527E-13 0.00000
17055E-13	0.00000	.81601E-01	0.00000	167436+00	0.00000	1009ZE+00	0.00000	77627E-14	0.00000551746-13 0.00000
-11260E-13	0.00000	816011-01	0.00000	16743E+00	0.00000	10092E+00	0.00000	159676-13	0.00000 .44691E-13 0.00000
.164658-12	0.00000	.16438E-01	0.00000	243781+00	0.00000	.21670E-01	0.00000	.12478E-12	0.00J0065964E-13 0.60000
-+59330E-13	0.00000	104380-01	0.00000	∠437dC+00	0.00000	-21670F-01	0.00000	•93624E-13	0.0000042827E-13 _0.00000
26124E-12	_0.00000	260356-01	0.00000	10780E-01	0.00000	.972586-01	0400000	.15967E-12	0.0000037006E-13 0.00000
923726-13	0.00000	.26035E-01	0.00000	10700E-01	0.00000	.97258E-01	0.00000	.15685E-12	_U.OUJOQ84861E-14_[0.000000
.66056E-13	0.00000	17480E-01	0.00000	25892E+00	0.00000	. •53414E-01	0.00000	.56871E-13	0.00000 .10371E-12 .0.000 <u>00</u>
60506E-13	0.00000	.174808-01	0.00000	~25892E+00	0.00000	.53414E-01	0.00000	.723528-13	0.00000 930796-14 [0.00000
20320E-12	0.00000	.17480E-01	0.00000		0.00000	53414E-01	0.00000	~.65644E-13	0.00000 .621236-13 0.00000
2571eE-13	0.00000	17480E-01	0.00000	25892E+00	ັນ	5J414L-Ö1	0.00000	7100dE-13	0.0000013292E-13 0.00000
18682E-12	0.00000	-20035t-01	_0•00000	107806-01	0.00000	97258E-01	0.00000	11757E-12	0.0000063798E-13 0.00000
•61155E-13	[0.00000]	26035E01	0.0000	10780E-01	0.00000	97258£-01	0.00000	<u>11040E-12</u>	0.0000057322E-13 0.00000
13328E-13	[u.00000°]	164381-01	~o.oooo	24378E +00	.ö.00000	21670E-01	, 0 ° 0 0 0 0 0 ,	61472E-13	0.0000085340E-13_0.00000
-16640E-12	0.00000	[-1643&E-01	0.00000	=-24378E+00	0000000	21670E-01	~o,.00000	58305E-13	0.00000191146-13 0.00000
-14557E-12	0.00000	81601E-01	0.00000	16743E+00	0.00000	.10002E+00	0.00000	.28795E-13	0.00000216656-14 0.00000
99077E-13	0.00000	, 10-31001E.		16743E+00	ō•00000	.10002E+00	0.00000	-30527E-13	0.00000 .46551e-13 0.0000
.10614E-12	0.00000	12219E+00	0.00000	.16307E+00	0.00000		0.0000,0	-1263dC-12	0.00000 .40913E-13 0.00000
7-17543E-L2	_0.00g0o	.,.12513F+00	០* ០ភិ០០០	16jv7E+0j	¯o•oōōod	15552E+ <u>00</u> _	0.00000	13148E-12.	0.00000 -88263E-13 0.00003

NATURAL FREQUENCY = 3727826+03

YX REAL _	TX TY REAL	TY TATE TO THE TEAL TO THE TEA	TZ RX THAG KEAL	RA RY	L THAC TO	RZ RZ REAL IMAG
- <u>•2</u> 1112E+00	0.00000 .33415E-14	0.00000 T.25331E-13	0.00000242586	-i3 0.00000 1860	4E + 00 00,000 00 6	2371E-01-0.00000
21112E+00	0.00000550406-13	0.00000 .12475E-13	_0.0000076174E-	-14 0.000001860	4E+00 0.00000	2371E-01 0.00000
22244E-01	0.00000156551-13	0.00000 .37297E-13	_0.0000086833E	-14 0.000002323	4E-01] 0.000007	46856-01 0.00000
	0.00000143046-13	0.0000044444-13	_0.000007a386E-	-14 0.000002323	4E-01	4685E-01 0.00000
16489E+00	0.00000 .278466-13	0.0000 <u>0</u> 64460E-13	_0.00000 ~-84840E-	-14 [0.00000 .1477	2E+00 0.000004	79036-01-0,00000-
16489E+00	0.00000452156-13	0.0000063479E-13	0.00000450646-	-14 0.00000 .1477	20+00 -0.00000	79036-01 _0+00000
e21900E+00	0.00000 .207466-14	0.0000022753E-13	0.0000030936E	-13 .0.000001975	OF+00 (0*00000 ""*;	13029E-01_0.00000
21900E+00	0.0000030605E-13	0.00000 .19595E-13	0.0000029377E	-13 0.00,000 .1975	0E+00 <u>0</u> .00000 1.,	13059F-01 0.00000
99257E-01	9.00000 -71066E-14	.0.0000039228E-13	0.0000025849E	-13 0.00000 .8959	1E-01 0.00000	3186E-01 0.00000
99257E-01	0.00000255636-13	0.0000039252E-13		-13 0.00000 .8959	16-01 . 0.00000	93[46F-01, 0'0000ñ]
99257E-01	0.0000052354E-14	0.0000049011E-13	0.00000 .62533E	-14 T0.00000 T.8959	iE-01 0.00000	3186E-01 0.00000
.99257E-01	0.00000 - 460146-14	0.0000048997E-13	_0.00000 .84328	14 0.00,000 ,8959	16-01 0.00000	3189F-01 0.00000
Z1900E+00	0.0000054363E-14	_0.0000018036E-14	0.0000017802E	-13, 0.000001975	08+00 [0.00000	3029E-01_0.00000
.21900E+00	0.0000018632£-14	0.0000018721E-14	0.00000 .16382E-	-13 0.000001975	0E+00 0.00000:	3027E-01 0.00000 _
16489E+0U	0.00000 .13233E-13	0.0000047200E-13	0.00000303026	-14 _0.000001477	28+00 0.00000	77036-01 0.00000
.164892+00	0.00000 100336-13	0.00000 7 .47749E-13	0.00000 .14378E	-14 0.000001477	2E+00 0.00000	7903=-01_0.00000
-22244E-01	0.00900 .386976-13	0.00000 .36941E-13	U.0000010818E	-13 0.00000 .2323	4E-01 0.00000	74685E-01 0.00000
22244E-01	0.00000119088-13	0.00000. 36957E-13	0.00000147598	-13 0.00000 .2323	4E-01 [0.00000] .	4685E-01 0.00000
	0.0000040528E-13			•	·	2371E-01_0.00000
21112E+00	0.0000046273E-14	0.00000271686-13	0.00000329466	-13 0.00000 1.1860	4E+00 0.00000	23716-01 0.00000

ŧ
7
7
٤
, res
ž

	NATU	·····							
_ TX _ REAL	TX TY TY	TY TZ	TZ I HAG	xX REAL	RK THAG	RY PEAL .	KY	KÉAL	RZ IHAG
-11954E+00	0.00000 .82508E-1	4 0.0000050010	E-14 0.00000	214588-13	0,00000	160116-12	0.00000	51405 <u>F_+</u> 00	
-11954E+0d	0.00000419716-1	3 0.00000138250	-i4 <u></u> 0.00000	24620E-13	0.00000 =.	15566E-12	0.00000	•21902 <u>+00</u>	0.00000
-,23122E+00	0.0600021100E-1	3 0.00000 .852901	-14 0.00000	2d039E-13	0.00000	7Ò825E-13		~5y140e-01	0.00000
*+23122E+03	0.00000126854-1	4 _0.0000044846	-15 0.00000	.16375t-13	0.00000	686118-13.	0.00000	.591,40£-0,1	_0.60000
93326E-01	0.00000 .225386-1	4 0.00000150121		55014E-14	0.00000	142225-12	0.00000	-129216+00	0.00000
93326E-01	0.0000025576E-1	3 0.00000 .16924	E-13 0.000u0	.806551-14	0.00000	14605E-12		-,12921E+00	0.00005
23541E+00	0.00000186318-1	4 0.00000227751	i-ii. v.00000	149858-13	0.00000	Ž4262E-13	_0.00000]	75020=-01	
	0.0000039056L-1								
•	0.00000 ~24730L-1								
	0.00000181246-1								
17756E+ut		5 0.0000021989							
177562+0	0.00000246116-1	3 0.0000022255	E-13 0.00000	.217975-14	~`0.00000´~	15372E-12	0.00000	11441E+00	0.00000
	0.00000 19667E-1								
	0.00000126216-1				0.00000				
.9332aE−01		4 0.00600 .14376			0.00000	39223E-12	0.00000	12921E+00	
•93326E-0		.3 0.00000 .13083							
-23122E+00		- '							
•23122E+0		4 0.00000 .19924							
11954E+6		3 0.0000054704							
	0.00000188302-1								

•			•							
. TX REAL	IHAG	TY .	TY TZ	TZ IHAG	KEAL	RX IMAG	RY REAL	THAG	RZ KEAL	IMAG
.18918E+00	ó*00000	41291E-11	0.00000153140-11	L 0.00000	.45775E-11	0.00000	.15570E+00	0.00000	•1009aE+00	0.0000
÷18919E+0ú	0.00000	.41075E-11	0.0000015398E-1	L _ 0.0000ō.	.45833E-11	0.00000	15570E+00	0.00000	10098E+00	0.00000
92025E-01	0.00000	261528-11	0.00006597788-11	L 0.00000	•16467E-11	0.00000	74324E-01	0.00000	.85806E-01	0.00000
~92025E - 01	0.00000	.25857E-11	0.0000059988E-11	0.00000	.16293E-11	0.00000	74324E-01	0.00000	85806E-01	0.00000
22194E+00	9.00000	112316-11	0.00000 .20071E-11	L 0.00000	18271E-11	0.00000	18945£+00	0.00000	72055E-02	0.00000
+22194E+00	0.00000	.10655E-11	0.00000 .20001E-11	0.00000	1d362E-11	.0.00000	18945E+00	0.00000	_•72055E-02	0.00000
57420E-01	0.00000	115636-11	0.0000060931E-11	0.00000	/o936E-12	0.00000	49098E-01	0.00000	84289E-01	0.00000
-57420E-01	0.00000	.11044E-11	0.0000060890E-11	0.00000	77078t-12	0.00000	49098E-01	0.00000	84289E-01	0.00000
.18221E+00	0.00000	21430E-11	0.0000044459E-1	i_ 5.00000 j	.27263b-11	0.00000	.15718E+00	0.00000	49977E-01	0.00000
182216+00	0.00000	.21021E-11	0.00000444536-11	0.00000	.272248-11	0.00000	15718E+00	0.00000	-49977E-01	0.00000
18221E+00	_0.00000	21421E-11	0.00000 -44678E-1	0.00000	27107E-11	0.00000	.15718E+00		49977E-01	0.00000
182216+00	0.00000	.20955E-11	0.00000 -44670E-11	L 0.00000	.270526-11	0.00000	1571dE+Q0_	0.000,00		0.0000
₹.57420E-01	0.00000		0.00000 .60668E-11		78605E-12	0.00000	49098E-01_		.842898-01	0.00000
7-57420E-01	0,00000	.11265E-1I	0.00000 . 60624E-1	<u> </u>	78jžo5-12		49 <u>09</u> 8E-01		84 <u>2</u> 849E-01	0.0000
=-22194E+00	_0.00000_	10687E-T1	0.00000204696-11	0.00000	18134E-11	<u>_0.00000</u>	18945E+00	0.00000		0.00000
22194E+00	0.00000	.10880E-11	0.00000 20477E-1	L 0,00000]	181386-11	0.00000	18945E+00	0.00000	72055E- <u>02</u>	0.00000
92025E-01	0.00000	26229E-11	0.00000599936-11	i 0.00000	-10402E-11	0.00000	74324E-01	0.00000	85806E-01	0.00000
92025E-01	.ô.00000	. 56660 <u>C</u> - <u>1</u> 1	[0.00000]59990E_[]	i <u> </u>	_[.lo499E+1]			0.00000		0.0000
_			0.0000015932E-13						•	
=.18914E+00	0.00000	.41558E-11	0.00000 .15923E-1	0.00000	-40048E-11	0.00000	.15570E+00	[0.00000]	-100984-00	0.00000
		-		•-		-				= +a++

When the second is present the

NATURAL	FRE OULNCY=	.495598E+03

NATURAL FREDUÉNCY = 1 495598E+03
TX TX TY TY TZ TZ RX RX RY RY RZ RZ RZ REAL IHAG REAL IHAG REAL IHAG REAL IHAG REAL IHAG
-69314E-11 0.0000016056E.00 0.0000061141E-01 0.00000 .17935E-00 0.0000056768E-11 0.00000 -37218E-11 0.00000
69111E-11 0.00000 -16056c+60 0.0000061141E-01 0.00000 -17935E+00 0.00000 .57047E-11 0.0000036610E-11 0.00000
33953E-11 0.0000010255E+00 0.0000023406E+00 0.00000 .63659E-01 0.0000027461E-11 0.00000 [.31565E-11 0.0000]
=-91909E-11 0.0000042019E-01 0.00000 .79057E-01 0.0000071042E-01 0.0000069431E-11 0.0000025827E-12 0.00000
20997E-11 0.0000044061E-01_0.0000023732E+00 0.0000030226E-01 0.0000017913E-11 0.0000031663E-11 0.00000
.210516-11 0.00000 .440616-01 0.0000023732E+00 0.0000030226L-01 0.0000017868E-11 0.00000 .305726-11 0.00000
-67996E-11 0.0000082771E-01 0.0000017405E+00 0.00000 .10601E+00 0.00000 .57586E-11 0.0000014330E-11 0.00000
66ZB9E-11 0.00000 .82771E-01 0.0000017405E+00 0.00000 .10601E+00 0.00000 .576Z9E-11 0.00000 .1d393E-11 0.00000
7.66700E-11 0.0000082771E-01 0.00000 17.17405E+00 0.00000 10601E+00 0.00000 57553E-11 0.00000 18925E-11 0.00000
66572E-11 0.00000 .82771E-01 0.00000 .17405E+00 0.00000 .10601E+00 0.00000 .57595E-11 0.000018121E-11 0.00000
21794E-11 0.0000044061E-01 0.00000 -23732E+00 0.0000030226E-01 0.0000018172L-11 0.00000 -30917E-11 0.00000
813656-11 0.0000042019E-01 0.0000079057E-01 0.0000071042E-01 0.0000069674E-11 0.00000 -26126E-12 0.00000
-81444E-11 0.00000 420196-01 0.00000790576-01 0.0000071042E-01 0.0000069743E-11 6.0000028948E-12 0.00000
33652E-11 0.00000 =.10285E+00 0.0000023406E+00 0.00000 .63659E-01 0.000002727dE-11 0.0000031434E-11 0.00000
34139E-11 0.00000 10265[+00 0.0000023406E+00 0.00000 .63659E-01 0.0000027350E-11 0.00000 132028E-11 0.00000
to a contract of the contract

NATURAL FALGULNCY
TX TX TY TY TY TZ RX RX RY RY RZ RZ RZ REAL IMAG REAL IMAG REAL IMAG REAL IMAG REAL IMAG REAL IMAG
-66049E-01 0.0000075792E-13 0.00000 .80913E-14 0.00060 .17149E-13 0.00000 .11085E-12 0.0000023699E+00 0.00000
-66049E-01 0.0000018360c-13 0.0000014487E-13 0.00000 -95541E-15 0.00000 -11938E-12 0.0000023699E+00 0.00000
-23248E+00 0.0000030219E-13 0.0000030825E-13 0.0000013245E-13 0.0000014074E-12 0.00000 -12711E-01 0.00000
-232486+00 0.0000010647E-13 0.0000025075E-13 0.0000086196E-14 0.0000013651E-12 0.00000 [.12711C-01 0.0000]
10642E+00 0.00000 =-33819L=13 0.0000055445L-13 0.00000 -41618E-13 0.0000014174E-12 0.00000 .14168E-00 0.00000
10842E+00 0.00000 .54817L-13 0.0000064517E-13 0.00000 .13983E-13 0.000001273dE-12 0.00000 .14108E-00 0.00000
-22921E+U9 0.00000 .79019E-15 0.00000 -53867E-14 0.00000 .24705E-13 0.00000 .78784E-13 0.0000085515E-01 0.00000
22921E+00 0.00000 .75707E-13 0.0000021932E-15 0.00000 .30541E-13 0.00000 .84808E-13 0.0000085515E-01 0.00000
.17120E+00 0.00000 .422926-13 0.00000 .66158E-13 0.00000 .12763E-13 0.00000 .13556E-12 0.0000012243E+00 0.00000
.17120E+00 0.00000 .64154E-13 0.00000 .58088E-13 0.00000 .10338E-13 0.00000 .12633E-12 0.00000 .62443E+00 0.00000
-17120c+03 0.00000 .46983E-13 0.0000023333E-14 0.0000014270E-13 0.0000033471E-13 0.0000012243c+00 0.00000
-17120E+00 0.00000 -41758E-13 0.00000 -46509E-16 0.0000018062E-13 0.0000031288E-13 0.00000 -12243E+00 0.00000
229Z1E+O) 0.00000 .19574L-13 0.0000065698E-13 0.0000093640E-14 0.0000013301E-12 0.0000085515E-01 0.00000
22921E+00 0.00000 .33765E-13 0.0000066713E-13 0.0000010206E-13 0.0000013355E-12 0.0000045515E-01 0.00000 -
-108422+03 0.0000028790g-13 0.0000015388E-13 0.00000 .21206E-13 0.00000 .68054E-13 0.0000014104E-00 0.00000
10842E+00 0.0000015160E-13 0.0000013952E-13 0.00000 .15738L-13 0.00000 .6909LE-13 0.0000014108E+00 0.00000
-23248E+00 0.000001/603E-13 0.00000 39843E-13 0.00000 .12698E-14 0.00000 .10932E-12 0.0000012711E-01 0.00000
.23248E+00 0.0000066447E-13 0.00000 .45332È-13 0.00000 .14195E-13 0.00000 .11447E-12 0.0000012711E-01 0.00000
66049E-01 0.0000051584E-13 0.0000024372E-14 0.0000031818E-13 0.0000010381E-12 0.00000 .23699E+00 0.00000
66044E-01 0.0000088338E+13 0.00000210715-14 0.0060031471E-13 0.0000010033E-12 0.00360 .23699E+00 0.00000

WAR STRAIGHT ISTANT

NATURAL	FKLOULNCY=	.5/6674E+03	
---------	------------	-------------	--

TX REAL	TX IHAG	- ~ TY - kłal	TY IHAG	TZ REAL	'TZ I MAG	RX Real	RX IHAG	RY Real	RY	REAL THAG
35001E-13	0.00000	30075E+00	0.60006	-40480E-14	0.00000	17502c-13	0.00000	37113E-13	0.00000	~78438E-13~0.0000 <u>~</u>
- 	0.00000	30075£+00	0.00000	-1115396-13	0.00000	1d918E-13	0.00000	516928-13	0.00000	70821E-14 0.00000
.64270E-13	0.00000	18587E+00	0.00000	344868-13	0.00000	933146-14	0.00000	.20870E-13	. 0. 00 000	.895056-15 0.00000
10950E-13	0.00000	18587E+00	0.00000	19273E-13	0.00000	.19919E-13	0.00000	.20573E-13	0.00000	.369941-13 0.00000
33014E-13	0.00000	834306-13	0.00000	.10914E-12	0.00000	.49780E-13	0.00000	.16442E-13	0.00000	.173546-13_ 0.00000
55507E-13	0.00000	66813t-13	0.00000		0.00000	362396-13	0.00000	-10716E-13	_0.00000	
12292E-13	0.00000	.1d587E+00	0.00000	.14707E-12	0.00000	428001-13	_0.00000	29337E-13	. 0.00000	20384E-13 0.0000J
-25658E-13	0.00000	.10587E+00	0.00000	15299E-12	0.00000	135991-13	0.00000	,45216E-13	0.00000	33356E-13 _0.00003_
.32326E-14	0.00000	.30075E+00	0.00000	`33061E-Ĩ3	0.00000	48457E-13	0.00000	18358E-13	. 0. 00000	.33959E-13 0.00000
.23939E-13	0.00000	.30075E+00	0.00000	56084E-13	0.00000	7>340E-13	0.00000	.24779E-14	_ o* ooo oo	1.0343E-13 0.00000
-49469E-14	`a.ooooo	300758+00	0.00000	14479E-12	_ 0.00000	-25655€-13	0.00000	.247110-13	0.00000	58949E-14 0.00003
152076-13	u.00000	.30075++00	0.00000	14583E-12	0.00000	171786-14	0.00000		<u>_</u> 0.00000	27421E-14 0.00000
_88490E-14	ŏ.00,00	18587E+00	0.00000	40050E-13	_0.00000		_0200000 <u>_</u>		0.00000	- 22806E-13 0.00000
28467E-13	0.00000	18587L+00	0.00000	61118E-13	<u></u>	.34701E- <u>1</u> 3	0.00000	68843E-14	0.00000	.27044E-14 0.00000
45297E-13	_0.00000	73154E=[3]	0.00000	.55174E-13	000000	710021-14		I2357E-13	_ 0.00000	.74681E-14 0.00000
55255E-14	`0.00000	280326-JJ	_ 0•ñooà.	. 862246-13	00000		0.00000	72056E- <u>L</u> 4	0.00000	36640E-13 0.00000
F-14125E-13	. [၁• გიეიიი	14587E+00	_ 0 - 00 000	774325-13	0.00000	- -377736-13		3226JE-i3	0.00000	97273E-14 0.00000
-68442E-13	0.0000 0	·18587£+00	0.00000	3575E- <u>1</u> 3		31479E13	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	34164E-13		21040 <u>E</u> -13 0.00000
2556dE-14	j.00000	30075E+00	_ 0.0000g	17445Ë-1J	0.00000	541076-13	0.00,000	14145E-13	0.00000	.41191E-13 0.00000
==35764E-13	_0.00000	-,30075E+00	0.00000	11392 <u>6-13</u>	<u>_0</u> .000000	61166E-13	0.00000	70580E-14		.79891E-13 0.00000
	•								-	

		NATURA	L FKEOULN	CY= +617710	£+03						
TA REAL	TX Imag	TY KEAL	TY I MAG	T.Z Real	TZ 1mag	KΧ ₹EAL	RX Imag	. KY Real	I 4 V C 4 A	RZ KEAL	QZ THAG
.79738E-12	0.00000	214106+00	0.00060	.47452E-01	0.00000	.18049E+00	0.00000	•61259E-12 [°]	0.00000	.72338E-12	0.00000
.716161-12	0.00000	.21410L+00	0.00000	.47452E-01	0.00000	.18049E+00	0.00000	~56489E-12	0.00000	605391-12	0.00000
.955382-12	0.00000	142486+00	0.00000	.18305E+00	0.00000	.140361-01	0.00000	68442E-12	0.00000	•34517E-12	
.83059E-12	0.60000	.14248£+00	0.00000	.18305E+00	0.00000	.140361-01	0.00000	72377E-12	0.00000	310226-12	ຶ່ງ•ວຍວວຍຸ້
.70926E-12	0.00000	906674-01	0.00000	14614E+00	0.00000	415276-01	0.00000	55002E-12	_0.00000_	42120E=12	
.69079E-12	0.00000	.900671-01	0.00000	14614E+00	0.00000	41527t-01	0.00000	58605E-12	0.00000	<u>334426_12</u>	_0.00000_
,93341E-12	0.00000	864376-01	0.00000	21237E+00	0.00000	.87174E-01	0.00000	.71887E-12	_o•ooooi	-, 333334-12	0•āòoo <u>ō</u>
.749412-12	0.0000	.8u4d7t-01	0.00000	212376+00	0.00000	.871746-01	0.00000	.72053£-12	jő.00000	.339,226-12	0.000000
,768178-12	0.00000	43949E-0 <u>1</u>	0.00000	.128016+00	0,00000	.83439E-01	` à. 00 ò oo		_0.00000		0.00000
.8655#E-12	0.00000	.43949L-01	0.00000	.12801L+00	0.00000	.83439t-01	0.00000	-6524/E-12	00000	~~31855E-12	0.00000
.89214E-12	~~	.43949L-01	0.00000	-12801E+00	`0-00000	83437E-01	0.00000	67020E-12			0.00000
				. 1280 [E+00		•		67887E-12			
							0100000	-,75727E-12	0.00000	39635E-12	0.00000
			•	21237E+00				~~~77086E-12			
.77897E-12	0.00000	.90657L-01	0.00000	-14614E+00	0.00000	.41527E-01	<u> </u>	.587236-12	0.00000	354o5E-12	_0.0000
								-56253E-12			
.86747E-12		.14248E+00						.78887E-12			
-103325-11		14248E+00"		-	•		•				
.774odE-12		•	-					"59320E-12			
1871036-12								62859E-12			

3	ŧ.
1	Ļ
100	
1	į
	ŧ
	•

	. 4	ATURAL FREQUEN	CY=' .618714	E+03						
TX REAL	TX - TY		•		KX Real	RX -	RY REAL	THAC .	RZ REAL	RZ IHAG
.15589E+00		E-12 0.00000			74862E-12	0.00000	11979E+00	0.00000	-413635E+00	0.00000
	0.0000073242				75270E-12	0.00000	11979E+00	0.00000	13635E+00	0.00000
.18084E+Ó0		==12 0.00000			801998-13	0.00000	.14421E+00	0.00000	651666-01	. 0.00000
-18084E+00		L-12 0.00000			80340E-13	0.00000	.14421E+00	0.00000	.65160E-01_	0.00000
_13570E+00		C-12 0.00000			.32557E-12	0.00000	.11062E+00	0.00000	.701506-01	[0.0000 <u>0</u>
•13570E+00	0.0030010920	£-12 0.0000	4410/E-12	0.00000	.33360£-12	0.00000			78150E-01	
.16947E+00						0.00000	14233E+ŎO	်စ•စစ္ခံစစ္	.644806-01	_0.00000_
•16947E+00	0.0000062025	E-13 0.00000 <u>-</u>	.10157E-11	0.00000	1d733t-12	0.00000	142336+00			
.15327E+00	0.000003738	ī∈_13 _0.00000_	37818E-12	`ò.00000	29172E-12	0.00000	-1,2823E+00	0.00000	72016E-01	0.00000
•15327E+00	g.000g012438	E-12 0.00000	38350E-15	_0.00000	28862E-12	0.60000	128236+00	0.00000	. •72016e-01	_0.00000_
.153276+00	0.000004425	E-12 0.00000	66026E-12		.34586E-12	0.00000	.12823E+00	0.00000	72016E-01	0.00000
.15327E+00	0.00000 77.49289	L-12 0 00000	65800E-12	000000	**.34445E-12	0,000,00	12823E+00	0.00000	.72016c-01	0.00000
16947E+00	0.00000 -59729	3E-12 0.0000	./8741E-12	ຼື ລູ້. ດວຸນຸດດີ	.53265E-12	. ō, 0000ò	14231E+00	0.00000	.64480E-01	0.00000
-16947E+00	_0.05000	E-12 0.00000	78484E-12	00000.		0.00000	142338700	0.00000	64440E-01	0.00coj -
-13570E+00	0.000006424	LE-12 0.00000	.743386-12		52782E-13	0.00000	11095E+00	0.00000	74150E-01	0.03000
•13570E+00		3E-12 0.00000	74451ETZ	<u></u>	4954ZE-13	0.00000	11065 <u>£+00</u>	<u></u>	78150E-01	0.00000
-18084E+00	0.0000082180	o <u>E</u> -120.00000	74563E-12	0.00000	823036-13	0.00000	14421E+00	_`o•bezoo	65166E-01	0*00000
180846.00	ກີ່ ປຸດບັດຄວີ່-793ນີ້	sĒ-12 0.00000	74526E-12	0.000,00		_ 0.00000	14421E+00	0_000000_	.65166E-01	0.00000
.1556 JE+0.	0.000001126	86-11 0.0000E	411 <u>5</u> 86-12	_0.00000		0.00000	11979E+00	0_•00000 <u>_</u> _	13635E+00	0.00000
-15589E+00	0.00000 .1045	7E-11 0.0000	411358-12	0.0000	79875E-12	<u>0</u> 0000 <u>0</u> 0	11979E+00	0.00000	13635E+00	0.00000

NATURAL	FREQUÊNCY=	.623158E+03
		44544444

TX TX TY TY LEAL	TY TEAL	TZ RX IMAG REAL	RX RY	RY RZ RZ IHAG THAG
.934172-13 0.0000013091E+00	0.00000 .168641+00	0.00000 .177586-01	0.0000012560E-12	0.00000195324-13 0.00000
.13391E-12 0.00000 1.13091E+00	0.00000 .16864E+00	0.00000 -17758E-01	0.00000 [94406E-13	0.00000 .15451E-12_0.00000
-94634E-13 0.0000014730€+00	0.00000179936-01	0.00000 .32249E-02	0.00000 " 91766E-13	0.0000034162E-13 0.00000
.18968E-12 0.00000 .14730E+00	0.0000037993É-Ö1 "	0.00000 -32249E-02	0.00000 -13262L-12	6.00000 .44313E-13 0.00000
-11369E-12 0.0000019322E+00	0,0000011049E+00]	0.00000 .10062E+00	0.00000826666_13	0.00000 .47474E-13 0.00000
.65344E-13 0.00000 .19322L+00	0.00000110496+00	0.00000 .100621.00	0.00000 .10040E-12	@.0000080901E-13 _0.00000
-61672E-13 0.0000021416E+00	0.00000 .893658-01	0.00000 .126456+00	0.00000 10477E-12	0.0000049897E-13 0.00000
.15815E-12 0.00000 .21416E+00	0.0000à89365E_g1	0.0000012645E+00	_0.0000074514É-13	0.00000603622-14 0.00000
-13407E-12 0.0000019755E+00	0.00000 .107080.00	0.00000 .39098E-01	0.0000090419E-13	0.00000345256-13 0.00000
.37838E-13 0.00000 .14755E+00	0.0000010708E+00	0.0000034048F-01	. 0.0000092101E-13	0.00000 .825066-13 0.00000
-89731E-13 0.0000019755E+00	0.0000010708E+00	0.0000039098E-01	0.00000 -9123uE-13	0.0000041370E-13 0.00000
.12264E-12 0.00000 .19755E+00	0.0000010708E+00	0.00000 .39098E-01	0.00000 -855348-13	0.00000157156-130.00000
-94413E-13 0:0000021416E-00	0.0000089365E-01	J.00000' ".12645E+0Ò	ó.00000	. 0.00000 25611F-13 0.00000
-32894E-13 0.00000 .21416E+00	0.0000089365E01	0.0000012645E+00	_0.0000066409E-13	
-75970E-13 0.000001932ZE+00	0.00000 111049E+001	0.00000 .10062£+00	j0.0000000839F-i7	0.00000 .848038-13 0.00000
-95946E-13 0.00000 :193226+00	0.00000li04}E+00 _	u.0000010062E+00	0.0000054536E-13	0.0000019425E-13 0.00000
-12907E-12 0.0000014730E+00	.0.00000 -37993E-01	_0,00000 <u>0</u> 32249E02		0.0000057860E-13 0.00000
_66777E-13 0.00000 .14730E+00		0.0000000000000000000000000000000000000	0.0000073626E-13	0.00000 52711E-13 0.00000
-11562E-12 0.90000130711+00	0.00000 168642 90	0.00000 .177581-01	0.0000086095E-13	_0.00000 ~12651E-120.40000_
-6583cE-13 0.00000 -13091E+00	0.0000016864E+00	0.00000 .177586-01	0.00000 .992516-13	. 0.00000Z6977E-13 _ 0.00000

		NATURA	L FKEJUEN	CY= •71 <u>)</u> 2 77	E+03_					
TX TX	TX THAG .	KEAL .	TY	T4 REAL	YZ IHAG	RX REAL	RX IMAG	RY REAL	" RY IMAG	RZ RZ REAL THAG
	0.00000	.77156E-14	0.00000	899388-13	0.00000	-14d00c-13	0.00000	3605 JE-1 J	. o. o. o. o	.24607E +00 0.00000
192306-01	0.00000	47786F-L3_	6.00000	63083E-13_	0.00000	.34904E-13	0,00000	25252E-13	<u>_0</u> • 00000	.24607£+00 0.00000
18076E+00	0.00000	.10420E-13	0.00000	.806176-13	0.00000	749388-14	0.00000	55058E-13	_ 0.000,00	80657E-01_0.00000_
18076E+00	0.00000	198516-15	0.00005	.767948-13	0.00000	.49004E-13	0.00000	835981-13	0.00000	80657E-01 0.00000
248215+00	0.00000	.24465E-13	0.00000	-40622E-13	0.00000	45912E-13	0.00000	-6163/E-13	0.00000	57847c_OLO.00000
-24821E+00	0.00000	22227E-13	0.00000	.31707E-13	.0.00000	50290E-14	0.00000	.173248-14	0.00000	578476-01 0.00000
16962E-01	0.00000	.18525E-13	0.000000	69876E-13	_0.00000	.79298E-14	0.00000	.77559E-13	_o.cooqo	.16715E+00 0.00000
16962E-01	0.00000	.4uð5lC-13	6.00000	78184E-13	0.00000	32578E-14	0.00000	.56123E-13	_o. oonoo_	• 16715E • 00 0 00000
-,22418E+00	0.00000	86136E-14	0.00000	16382E-1J	0000000	.3/304E-13.	00000.0.	64071E-13	0.00000	85 300c-01 0.00000
22418E+00	0.00000	.100454-12	. ó•o~~~ooo_	_+.11945E-13_	0.00060	46097E-13	0.00000	62227E-13	0.00000	85300c-01_0.00000_
	0.00000	.119998-13	0.00005	.54398E-13	0.00000	185906-13	0.00000	-+62127E-14	~ ō. 00000	82300E-01_0.00000_
22418E+U0	0.00000	.96971E-13_	0.00000	.47589E-13	_0•\00000	-90740E-14	0.00000	40718E-14	_0.00000	85300E-01-0.00000
169028-01	0.00000	1/6221-13	0.00000	229406-13	0.00000	12489L-13	0.00000	•71103E-13	0.00000	.16715c+00 0.00000
16962E-01	0.00000	94807E-13[0,00000	20365E-13	0.00000	14261E-14	0.00000	80844E-13	~0.0000ō	167156-00
24821E+00	0.03000	48554L-13	_0,00000	13136E-13	_0.00000	.33782E-13	0.00000	16309E-13	0.00000	57847E-01 _0.00000
24821£+00	0.00000	31014E-13	_0.00000	7.22405E-13	~ ō.ooooō	~~29559E-13	0.00000	19819E-13	0.00000	57847E-01 0.00000
-18076E+00	0.00000	704926-13	0.00000		0.00000	·20128E-13	0.00000	52292E-13	0.00000	80657E-01 0.00000
i8076E+00	_ U. 00000	14168E-ļ3_	0.00000	~35236E-13_	.000000	104416-15	0.00000	62804E-13	0.00000	80657E-01 0.00000
19230E-01	0.00000	769j09E-13	0.00000	-:34628E-13	0.00000	~19468E-13	0.00000	49783E-13		.24607L+00 0.00000
19230E-01	. p. 00000	<u></u> 429856-13	_0.00000	33196E-13	0•00 <u>00</u> 0	16454E-13_	o.oōōōo	.5055JE- <u>1</u>]	<u>0• 005ño</u>	-24607E+00 0.0000J

	NATURAL	FREQUENCY=	.735407E+03
--	---------	------------	-------------

					4					
TX REAL	TX - "	KEAL	TY -	TZ. REAL	TZ IHAG.	RX REAL	RX THAG	REAL	RY" IHAÇ	RZ RZ
10152E-12	0.00000	.14640E+00	0.00000	,19551E+00	0.00000	.24985E-01	0.00,000	~~.47968Ë-13		18962E-12 0.00000
.10914E-12	0.00000	14640t+00	0.00000	19551E+00	_0.00000		0.00000	65144E-13	_0.00000	124326-12 0.000 <u>00</u>
-23744E-12	0.00000	-1713dc+00	0.00000	-17738E+00	0.00000	23611E-01	0.00000	.15908E-12	0.00000	597878-16 0.03000
180578-12	.0.00000	171388+00_	0.00000,	177386+00	0.00000	23611E-01	0.00000	.17536E-12	0.00000	.306521-13 0.00000
717408-13	0.00000	.18756E.+00	$0.00000\vec{0}$	35832E-01	0.00000	1>2025+00	0.00000	-+32940E-Ī3	_0.00000	97522E-13 _0.00000
216928-13	000000	14756L+00	0.00000	.35832E-01	0.00000	15202E+00	0.00000	16231E_[3		97425E-13 0.00000
19921E-12	0.00000	•11072E •00	0.00000	171376+00	_0,00000	219168-01	0.00000	7-18100E-12	0.00000	75963E-13 0.00000
.22292E-12	0.0000	110721.+00.	0.00000	17i37E+00	0.00000	219161-01	0.00000	15701E-12	ັບ. 0ວນບດ	20705E-14 0.00000
-172006-12	. 0.00000		0.00000	15367E+00	0.00000	.5809ZE-01	0.00000	.90916E-1 <u>.1</u>	_ o. ooooo	80338E-13 0.00000
63646E-13	0.00000	237931-01	0.00000	.153678+00	0.00000	.58092L-01	0.00000	.12154Ļ-12	6- 60906	
-141646-12	0.00000	237736-01	0.00000	. 153670+00	_0.00000	580928-01	.0.00000	•10327E-12	0.00000	-64006E-13 0.00000
17966E-12	0.00000	`~.23793E-01	0.00065	.153678+00	0.00000	~.50092E-01	0.00000	.12102E-12	_0.00000	661786-13 0.00000
21207E-12	. 0.00000	110726+00	0,000000	17137E+00	0.00000	. 21916E-01	_0.00000_	-, 17425E-1,2		-25646E-13 0.00000
-20783E-12	0.00000	-11072E+00	0.00000	17137E+00	0.00000	.21916E-01	,0.00000	-,166748-12		65913E-13 0.00000
23693E-14	0.00000	18756b+00	0.00000		00000	+1020Že+00		56138E-13		114348-12 0.00000
-64279E-13	" oʻ• ១០៤០o		0.00000		0.00000	152026+00	0.0000	44831E-13	0.0000	-11040E-12 0.00000
-21876E-12	0.00000	171386+00	0.00000	.1773dE+00	0.00000	.23o11E-01	0.00000	-19133E-12	_ 0.0,0000	.24213E-13 0.00000
225246-12	3 *00000	17138E+00.	0.00000	17738E+00	_0.00000		0.0000	.19272E-12	_0.00000	12444E-13 0.00000
124336-12	0.00000	14640L+00	0.00000	19551E+00	0.00000	20985E-01		94302E-13	e• ōō ō ō ō ō	-17726E-12 "0.00000"
.14840E-12	0.00000	•14640E •00	0.00000	19551É+00	0.0000	28985E-01	0.00000	88158E-13	. 0 • 00000	18581E-12 0.00000

and the missings form, the 27

NATURAL FREQUENCY= .741646E+03
TX TX TY TY TY TZ TZ RX RX RY RY RZ RZ REAL IHAG REAL IHAG REAL IHAG REAL IHAG REAL IHAG
11658E+00 0.0000040279E-13 0.00000 -10037E-12 0.0000027944E-13 0.0000082744E-01 0.0000016122E+00 0.00000
.11658E+00 0.00000 .87697E-13 0.00000 .10754E-12 0.0000012711E-13 0.0000082744E-01 0.00000 .16122E+00 0.00000
-21957E+00 0.0000066647E-13 0.0000090432E-13 0.00000 .60836E-14 0.00000 .17337E+00 0.0000019733E-01 0.00000
21957E+00 0.00000 .10596E-12 0.0000013547E-12 0.00000 .18385E-13 0.00000 .17337E+00 0.00000 .19733E-01 0.00000
36200E-01 0.0000071109L-13 0.0000077551E-14 0.00000 -11297E-12 0.0000034077E-01 0.00000 -10342E+00 0.00000
204466+00 0.00000448032-13 0.00000104416-12 0.00000 .269306-17 0.00000170766+00 0.00000424566-01 0.00000
20440E+00 0.00000 .344836-13 0.00000 .13957E-12 0.00000352676-14 0.0000017076E+00 0.00300 .42456E-01 0.00000
-13775E+00 0.0000011934E-14 0.0000012600E-12 0.0000068873E-13 0.0000011421E+00 0.0000083481E-01 0.00000
13775E+UO 0.0030016587E-13 0.0000013074E-12 3.0030036212E-13 0.00000 -11421E+00 0.00000 .83481E-01 0.00000
-13775E+00 0.00000 .19276E-13 0.0000011639E-12 0.00000 .64424E-13 0.00000 .11421E+00 0.00000 5.83481E-01 0.00000
-13775E+00 6.0000047963E-13 0.0000012303E-12 0.00000 39573E-13 0.00000 .11421E+00 0.0000083481E-01 0.00000
20446E+00 0.0700040029E-13 0.00000 18341E-12 0.0000027459E-13 0.0000017076E+00 0.0000042456E-01 0.00000
36280E-01 0.00000 1.122135-12 0.00000 1.57430E-14 0.0000012138E-12 0.0000034077E-01 0.0000010342E+00 0.00000
36280E-01 0.00000138202-12 0.0000086044E-14 0.0000011520E-12 0.0000034077E-01 0.00000 -10342E-00 0.00000
-21957E+00 0.00000 -31055E-13 0.00000 -17493E-12 0.00000 -13451L-13 0.00000 -17337E+00 0.00000 -19733E-01 0.00000
11658c+00 0.0000058594E-13 0.00000 .13798E-12 0.00000 .6484E-13 0.0000082744E-01 0.00000 0.16122E+00 0.00000
.11650e+09 0.0000061367E-13 0.00000 .13149E-12 0.00000 .64307e-13 0.0000082744E-01 0.0000016122E+00 0.00000

NATURAL	FREQUENCY	

TX REAL	TX IHAG -	. TY REAL	TY "	. TZ REAL	TZ I MAG	KK KEAL	RX I HAG	RY REAL	YY	RZ	RZ IHAG
•37231E-15	0.00000	•173556+00	0.00000	16049E-01	0.00000	17357E+00	0.00000			•35310E-14	
47587E-13	0.00000	17355E+00	0.00000	16049E-01	0.00000	1/3576+00	0.00000	17392E-13	_0.00000	.312005-13	ō • <u>'ōʻ</u> ōʻoʻòʻò'.
.337728-14	0.00000	-52174E-01	0.00000	12018E÷00	0.00000	-35478E-01	0.00006	.79004E-14	0.00000 [0.00000
68795E-14	0.00000	52174E-01	0.00000	120186+00	0.00000	.3>478E-01	0.00000	-22730E-14	0.000'00	27414 <u>k-</u> 13	0.00000
.11049E-13	0.00000	47755E-01	0.00000	.25282E+00	0.00000	.49242E-01	0.00000	23366E-13	0.00000 ;-	11975 <u>4-</u> 14	0.00000
-85051E-14	0.00000	.47755E-01	0.00000_	· 252d2E+00	0.00000	.492428-01	0.00000	61997E-14	0.00000	.85687E-14	0.0000
-4202bE-13	0.00000	113318+00_	0.00000			,44104E-01	_0.00000		0.00000		0.00000
-345188-15	ò*000 0 0	11331E+00	0.00000	.11230E-01	00000.0	44104E-01	0.00000	10806E-13	0.00000	.64181E-14 _	<u>0.0000</u>
.90786E-14	0.00000	~20366±+00		17848E÷00		-12488E+00	0.00000	83861Ê-14		. 18335E-14	0.00000
-15624E-14	0.00000	_:20366E:00_	์ถ∗ดดงดีวั	1784 <u>86+00</u>	o•òoooo	.12488E+00	0.00000	32791E-13	0.00000	:16010k-14	0.00000
		20366E+00									
24989E-13	ò•00ō0ō.	•20366E ÷00	0.00000	1784dC+00	0.00000	-12488E+00	0.00000	18403E-13	0.00000	27318E-14 "	0.00000
533716-14	ngoboóō	11331E+00'	0.00000_	11530E-01	~0.0000°	44104L-01	0.00000	10649E-13_		34070:-14	0.00000
		.11331£+00									
44021E-14	0.00000	4/755E-01	70.00000	25282E+00	0.00000	.44242E-01	0.00000		- 0-00000	-1859628-14	0.00000
44009E-13	0.00000	.47755L~01	0.00000	.T. 25282E+00	0.00000	-49242E-01	_0.000000	29833E-13	_0.00000	16864E-13	
		52174E-01									
-29100E-14	0.00000	52174E-01	_0.00,000_	12018E+00,	0.00000	.354786-01	0.00000	1993 <u>ZE-1</u> 3	0.00000	255036-13 "	0.00000
		•173556+00									
15699E-13	0.000,00	1/355E+00	_ดั∙ดดัดอกั <u>_</u>		0.00000	,1,735 (E+00_	_0.00000	23732E-13	0.00000	.23951E-13_	<u>0.00</u> 090]

NATURAL FREQUENCY= .847218E+03

TX REAL	TX Inag	TY REAL	TY IHAG	TZ. Real	LT LHAG	RX KEAL	RX I hag	RY Keal	YR DAM1	RZ RŽ REAL IMAG
58404E-13	0.00000	28176E+00	0.00000	.17532E-12	0.00000	.48835E-13	0.00000	.72002E-15	0.00000	27545E-12 0.00000
57561E-13	0.00000	281762+00	0.00000	1,6634E-12	0.00000	.675761-13	0.00000	±.81667£-13		82556±-13_0.000005
-17954E-12	0.00000	494636-01	0.00000	131478-12	0.00000	.20622£-13	0.00000	•12365E-12	0.00000	-11720c-12 0.00000
518836-13	0.00000	49467E-01	0.00000	13585E-12	0.00000	.29838E-13	0.00000	.8105dE-13	_ 0.00000	.106316-12_0.00000
3209>E-12	0.00000	-22361E+00	0.00000	61859E-13	0.00000	.49720E-13	0.00000	68374E-13	0.00000	39097E-13_0.00000
83612E-13	0.00000	.22361E+00°	0.00000	[421d3E-13	0.00000	-62121E-13 _.	0.00000	881226-13	0.00000	
•16400E-12	0.00000	•31233 <u>#</u> +00	0.00000	27503E-13	0.00000	55451=-13	0-00000	71960E-14	0.00000	10454E-12 0.0000J
.201186-12	0.00000	31233E+00	0.00000	-42527E-13	_n•00000	17901E-13	0.00000	776748-13	0.00000	33759E-140.00000_
17898E-15	0.00000	.14356E+00	0.00000		0.00000	77793E_13	0.00000	14719E-12	0.000000	.139146-12 0.00000
21283E-12	0.00000	•14356 <u>E</u> +00	0.00000	68196E-13	0.00000	668926-13	0.00000	.798588-13	_ 0.00300	
18878E-12	0.00000	14356£+00	0.00000	-16743E-13	0,00000	50452t-13	0.00000	~.54565E-13	0.00000	
.353608-13	0-00000	14356E+00_	0.00000	1585 <u>3E-11</u> 3	0.00000	67676E-13	0.00000	14125E-12	0-000000	16785E-12 0.00000
-18870E-12	.0.00000	31233E+00_	0.00000	48470E-[13]	0.00000	-,38073E-13	0.00000	"35578E-13		16454E-13 0.000000
19979E-12	0.00000	31233E+00	0.00000	.30308E-13	0.00000	44736b-13	0.00000	65230E- <u>1</u> 3	~0.00000	-112886-12 0.00000
10330E-12	0.00000	-12:361 <u>E</u> +00	0.00000	io1826-12	.0.00000	13519E-13	0.00000	12795E-12	0.00000	-80735E-13 0.00000
29832E-12	0.00000	22361E+00	0.00000	48210E-13	9.00000	169121-13	0.00000	.49000E-13	_0.00000	11335c-13 0.30000
23384E-13	0.00000	.49469E-01	0.00000	- 43721E-13	0.00000	.60189=-14	0.00000	12.39009E-13	0.05000	8150LE-13 0.00000
-18285E-12	0.00000	.49469E-01	0.00000	_,.36422E-13	0.00000	.6J006E-14	0.00000	939166-13	0.00000	14806E-12 0.00000
30668E-13	0.00000	_24176E+00	0.00000	86800E-13	0.00000	.76941E-13	0.00000	.26176E-13	0.00000	.86584E-13_0.03000°
318826-13	0.00000	.201766+00	0.00000	9932dE-13	0.00000	.77074E-13	0.00000	24609E-13	6.00100	.311106-12 0.50000

-	=	NATURA	L FREQUENC	Y=" .859770	E+03						
. T.K . REA!	. IK	TY	TY	TZ	TZ IMAĞ	REAL	RX IHAG	RY .	RY	RZ REAL	RZ
77737E-01				•		74564E-13			-		
.77737E-01	0.00000			.307276-13						-17062 <u>E</u> +00	
-20367E+00	0.00000			228426-13					•	.28791E-01	
20367E+00	0.00300			12949E~13	•	1/3261-14				207916-01	•••
-*18399E+0J	0.00000	29870£-13	0.00000	356526-13	0.00000	.92918E-14	0.00000	16191E+00	0.00000	.58341E-01	0.00000
*18344E+00	0.00000	58727E-13	0.00000	29154E-13	0.00000	.51758E-14	0.00000	16191E+00	. 0. 00000	583416-01	0.00000
103698-01	0.00000	60617E-13	0.00000	58047E-15	0.00000	.128878-14	0.00000	10325E-01	0.00000	104005+00	0.00000
.10309E-01	0.00000	,13784E-12	0.00000 _	.10720E-13	0.00000	.50439E-14	0.00000	103256-01	_0.00000_	104001+00	0.0000
					0.00000	_*55865£=jj3	0.00000	_ •167376+0ŏ	0.000_00_	.50995E-01	0.00000
		976976-13	0.00000	.40189L-13	0.00000	146491-13	0.00000	.1673/E+00	0.00900	50995E-01	0.00000
19724E+0J						32619E-13					
						25780E-13_			0.00000	50995E-01	0.0000
-10309E-01						.82444E-14				10400€+00	
10-360001						-87465E-14			-		
						192656-14 975616-15					
						47761E-13					
77737E-u1				43940E-13							
						1307032 13		#11000C*UL		***************************************	

ATILIALIS ROOF TAINEIRO

 		MA (URAI	L FREQUEN	1CY=' '_+'862306	E+03							
TX REAL	TX IHAG .	TY REAL :	TY Imag	T Z Real	TZ IMAG	RX KEAL	RK I HAG	RY REAL	KY Imag	RZT REAL	ا	RZ
21346E-01	0.00000	125104-12	0.00000	.427466-13	0.00000	.39084E-13	0.00000	381216-12	_0.00000	24655E	¥ 00 ~ (<u></u>
21346E-01	0.00000	131116-13	0.00000	.37974E-14	0.00000	77780E-14	0.00000	.37243E-12	្ត្រី _• ្តី១១១១១	24655E	• <u>0</u> 0 0 (o <u>ʻ c</u> oʻ <u>oʻj</u>
92837E-01	0.00000	734826-13	0.00000	327256-13	0.00000	.37425E-13	0.00000	128396-11	0.00000	119895	+`00 <u> </u>	o•noooo
92837E-01	0.00000	-139206-13	0.00000	50104E-13	0.00000	.23168E-14	0.00,000	-,1265ŽE-1ļ	o• oʻo oʻo o	11989E	<u>+</u> 00 -0)•000 <u>0</u> 0
-25646E+00	0.00000	.813406-14	0.00000	.61490E-13,	0.00000	.299826-13	0.00000	.13193E-11	0.00000	65701E	-01 (0.0000
25646E+00	0.00000	-21612 _E -13	0.00000	.51997E-Í3	0.00000	-15668E-13	.0.00000	.12570E-11	0.00000		-01 _[0	**00007_
24404E+00	0.00000	.934638-13	0.00000	_'19101F-13_	_0.00000	509558 <u>-</u> 13_	0.00000	122 <u>\$</u> 9E+12	0-00000	67100E	-01	o`*0000 <u> </u>
24404E+U0	0.00000	-12311E-13	0.00000	.296855-14	0.00000	487348-13	0.00000	76110E- <u>13</u>	_ o • o o o o o	-67100Ē	-01 0	
-10177E+00	0.00000	.1001 H -12	0.00000	7.177586-13	0.00000	18948E-13	_0.00000	13277E-L1	0.00000	1499 <u>0</u> ±	÷00 0	0.0000
-10177E+00;	0.00000	11437E-13	0.00000	53943L-13	0.00000	134986-13	0.00000	~.13156E-11	ŏ• öoòōo	7-14990E	• 00 T	0.0000
-10177E+00	0.00000	797366-13	0-00000		_0*00000	15209E-13	_0.00000	-13225t-11	0.00000	14990E	+00_0	
.10177E+U0~	0.00000	487546-13	′d.00000	.611u6E-13	_0.00000_	28790E-13	[0.00000 <u>]</u>	13446E-11	_a_0 <u>00</u> 00	14990E	• <u>00 </u>	1.00000
24404E+00	0.00000	.275952-13	0.00000	38071E-14	0.00000	255488-13_	0.00000	13946E-12	0.00000	6 <u>7</u> 100£	-010	ō•00 <u>0</u> 7_
24404E+00	0.00000	-+52713E-13	0.00000	55266E-14	0.00000	28097E-13_	0.00000	11984E-12	ୂର୍ଣ୍ଟ ପଦ ନ୍ତର୍	6710ÓĻ	-010	0.0000
•25646E+00	0.00000	34175E-13	,0.00000	24190Ê-1J	0.00000	. 34762E-13	0.00000	12250E-11	₫ <u>* 000</u> 000		- <u>0</u> 1 0	•00000
.25646E+00	0.00000	250566-13	0.00000	20124È-13	0.00000	•15320E-13	0.00000	12109E-11	0.00000	65701E	-01 0	<u>0</u> 0000 <u>0</u>
92837E-01	0.00000	55191E-13	0.00000	.362278-13	0.00000	.17249E-13	0.00000	.12098E-11	0.00000	1194?E	+00 0	00000
92837E-01	0.00000	-24709E-13	0.00000	.46408E-13	0.00000	-32557E-13		-12279E-11	0.00000	.1 <u>1</u> 989jž	• 000	<u>. </u>
213466-01	0.00000	-2720796-13	0.00000	15550E-13	0.00000	.39923=-14	0.00000	349726-12	0.00000	-, 24gb <u>5</u> E	+0 <u>0 </u>	j•00300
21346E-01	0.00000	-614872-13	0,00000	28107E-13,	0.00000	•14541E-13	0.00000	34784E-12	0.00000	24655E	∓00 <u></u> 0	040000

NATURAL FREQUENCY= .873360E+03 ΤX TΧ TZ REAL TZ REAL κX RХ IHAG KE AL IHAG REAL REAL IMAG IHAG -35419E-13 0.00000 -.18443E+00 0.00000 -16319E+00 0-00000 --10008E-01 0-00000 --95999E-13 0.00000 .26005E-12 0.00000 .16314E+00 0.00060 -.10008E-01 0.00000 .10108E-12 0.00000 .29668E-15 0.00005 -.49980E-13 G.00000 .184431+00 0.00000 --13985E-12 0.00000 --15136E+00 0.00000 --22855E+00 0.00000 .50910E-01 0.00000 -.16943E-12 0.00000 -.72727E-13 0.00005 -75475E-13 0.00000 -15135L+00 0.00000 --22855E+00 0.00000 .509106-01 0.00000 -.19452E-13 0.00000 -.51409E-13 0.00000 -22353E-12 0.00000 -.52076E-01 0.00000 .76219E-01 0.00000 .805d6L-01 0.30000 .6514bE-13 0.00000 .23956E-14 0.00003 -27456E-13 0.00000 .52076E-01 0.00000 .76219E-01 0.00000 .80586E-01 0.00000 .14277E-12 0.00000 .73133E-13 0.00000 -.12165E-12 0.00000 .11168E+00 0.00000 .10367E-01 0.00000 -.11764L+00 0.00000 .36427E-13 0.00000 .61709E-13 0.00000 -13353E-12 0.00000 -.11168E+00 0.00000 .10367E-01 0.00000 -.11764E+00 0.00000 .27843E-13 0.00000 -.31409E-13 0.00000 -22116E-13 0.00000 -173656+00 0.00000 --20079E+00 0.00000 -37230E-01 0.00000 -70524E-13 0.00000 -82093E-13 0.00000 -194876-12 0.00000 -.17365E+00 0.00000 --20079E+00 0.00000 -.37230E-01 0.00000 -.11320E-12 0.00000 .62390E-15 0.00000 \$13930E-12 0.00000 17365E+00 0.00000 2.20079E+00 0.00000 -.37230E-01 0.00000 17906E-12 0.00000 1.59585E-13 0.00000 -13803E-12 0.00000 -17365E+00 0.00000 .20079E+06 0.00000 -37230E-01 0.00000 .58337E-13 0.00000 _.56768E-13 0.00000 -11759E-12 0.00000 -11168E+00 0.00000 -10367E-01 0.00000 -11764E+00 0.00000 -16042E-16 0.00000 -1241E-13 0.0000 -55889E-14 0.00000 -.11168E+00 0.00000 -.10367E-01 0.00000 -.11764E+00 0.00000 -.13569E-12 0.00000 -.11249E-12 0.00000 -16493E-13 0.00000 -.52076E-01 0.00000 -.76219E-01 0.00000 .80586E-01 0.00000 .1683LE-13 0.00000 -.62382E-13 0.00000 .52076E-01 0.00000 -.76219E-01 0.00000 *13069E-12 0.000J0 .80586E-01 0.00000 -.98529E-13 0.00000 -.43938E-13 0.0000 -58261E-13 0.00000 --15136E+00 0.00000 .22855E+00 0.00000 .50910b-01 0.00000 .11065E-12 0.00000 .41911E-13 0.00000 -12938E-12 0.0G000 -15136E+00 0.0000J .22855E+00 0.00000 .50910E-01 0.00000 .24008E-13 0.00000 .37317E-13 0.00000 -.39083E-13 0.00000 --18443E+00 8.0000J -.16319E+00 0.00000 -.10008L-01 0.00000 .12549E-14 0.00000 -.45893E-13 0.00000 -14602E-13 0.00000 -18443E+00 0.00000 -.16319E+00 0.00000 -.10008E-01 0.00000 -.56138E-13 0.00000 -.12513E-12 0.00000

MATURAL FREQUENCY= .933079E+03

TX TX TY TY TY		TZ IMAG	KEAL RX	RK THAG	REAL	KĄ	KĒAL_	RZ IMAG
				0.00000_	22301E+00	0.00000	41851E-1	3 0.00000
64350E-14 [0.00000] .19857E-11 0.0	000012178E-11	0.00000	.49806E-11	0.00000	.22361E+00		76943 <u>E-</u> 1	3 0.00000
23986E-14 0.00000 .1d949E-11 0.0	0000 .44259E-11	0.00000	291451-11	0.00000	22361E+00	_0.00000	.50877E-1	3 0.00000
37338E-13 0.0000019047e-11 0.0	.43797E-11	0.00000	290246-11	0.00000	.22361£+00	0.00000	48596E-1	4 _0. <u>0</u> 0000
	90059E-11	0.00000	78777t-12	0.00000	22361E+00	_0.00m00	-4d675E-1	4 <u>0.00097</u>
64472E-13 0-0000032803E-11 0:0	9999999706E-11	0.00000	T-79520L-12	0.00000	-22361E+00	0.00000	31148£1	3 0.00000
.25899E-13 0.00000 .33591E-11 0.0	00000 .802508-11	0.00000	.158956-12	0.00000	22361E+00	0.00000	.22153c-1	.3. 0.000001.
	. 11-319£080000	0.00000	. 150904-12	0.0000	22361E+00	_0.00000	,39492 <u>E</u> -1	3 0.00000
31306E-11 0.00000 .20832E-11 0.0								
52327E-13 0.0000018793E-11 0.0	000020471E-11	0.00000	358572-11	0.00000	.22361E+00	0.00000	.1617/ <u>e-1</u>	4 0.00000
-57270E-13 0.0000023956E-11 0.0	00000 232778-11	0.00000	.36696£-11	0.0000	22361E+00	_0.00000	318576-1	3 0.00000
.679268-13 0.00000 .218986-11 0.0	.11-3£93E-11	0.00000	.36655L-11	0.00000	.22361E+00	_ 0.00'190,	21664E-1	3 0.00005
37133E-13 0.0000035372E-11 0.0	0000080354E-LL	0.00000	.706325-15	0.00000	22361E+00		455 <u>a</u> 96_1	4 0.0000
25077E-11 3.00000 .32333E-11 0.0	11-35126. 00000	0.00000	.Z>889L-13	0.00000	.22361E+00	0.00000	•4050le=1	4 0.0000 <u>0</u>
	00000 V0204E-11	0.00000	67178E-12	0.00000	_=.22361E+00	_0.00000_	27,75,0E-1	<u> </u>
.40260E-14 0.00000 .32287E-11 0.	0000090312E-11	0.00000	.67177E-12	0.00000	22361E+00	J.00J00	27930 <u>L</u> -1	13 _0.00000
51567E-14 0.0000016656E-11 0.	0000040932E-11	0.00000	.20357L-11	0.00000	2236 1E+00	0.00000	.20251E-1	13 [0.0000]
.3695dE-13 0.00000 .16798E-11 0.	00000	0.00000	-28544E-11	0.00000	.22361E+00	0.00000	17284c-1	13 [0.000002]
29856f-13 0.00000 .25816E-11 0.	00000 93050E-12	_0.00000	49850b-11	0.00000	223618+00			
94B00E-15 0.0000023214E-11 0.	0000093835E-12	0.00000	49849E-11	0.00000	.22361E+00	0.00000	~26941E-1	13 0.00000

NATHDAL.	ER DIR NCY=	-9345325+03

TX	TXIMAG	TY	TY IMAG	TZ REAL	T Z T AG	KX Real	RA -	- RY	` RY	REAL	RZ IHAG
_•32656E- <u>1</u> 3	0.00000	•72543E-01	_0.00000_	,33451E-01	0.00000	15719E+00	0.00000	- <u>.</u> 68167E-11	ñ•00000	.35537t-13	`o*ñoòo <u>o</u> o_
=.55539E-13	0.00000	725438-01		7.33451E-01	~~o.ooooo	=.15719E+00	0.00000	-67657E-11	`0.0000 <u>0</u>	-, 14632£-13	0.00000
33680E-14	_0•00noo	561,70E-01	_0.00000_	13428E+00	0.00000	.910026-01	0.00000	67807E-11	0.00000	201356- <u>1</u> 3_	0.00000
-56340E-14	0.00000	56170L-01	0.00000	13428E+06	0.00000	.9100ZE-01	_0.00000	.675218-11	u. 000 coʻʻ	30461E-14_	0.00002
2610LE-13	~ő•ooooo	105528+00	0.00000	.28571E+00	_ 0.00000	.229291-01	ó.0000v	67785E-11	0.00000	37012±-14	
47925E-13	0.00000	.10552£+00	0.00000_	285716+00	0.00000	22929£-01	0.00000	68209E-11	0,00000	15208E-13	
23875E-13	0.00000	10360L+00	~a.òoooo	2545LE+00	` ó.00000	192501-02	0.00000	70048E-11	0.00000	550836-14	0.00000
17751E-L3	0.003.00	10360 <u>F</u> +00	_0.000001	25451E+00		19250L-02	0.00000		_0.000.00	56986E-14	0.00000
33449E-13	3.00000	675061-01	0.00000	.6962>E-01	0.00000	.114711.+00	0.00000	71425E-11		[1]14ZoE-13	0.00000
2764dE-13	0.000,00	.67506E-01	0.00000	•69625E-01	_0.00000	.11471L+00	0.00000	71662E-11			0.00000
7.39244E-14	0.00000		0.00000	10-3<5040.	0.00000	11471E+00	0.00000	73915E-11	_0.00000	85060E-14	0.00000
57318E-13	0.00000	67506E-01	_ 0.00000_	. 696256-01	0.00000	11471E+0 <u>0</u>	0.00000	739746-11	0.00000	12739E-13	0.0000
.49443E-14	0.00000	.10350£+00	0.00000	25451E+00	~~	.14520E-02	0.00000	76020E-11	_ 0.000000	727246-14	0.00000
-48450E-13	0.00000	103608+00	_ 0.00000[25451E+00	0.00000	19250E-02	0.00000	~ 75449E-LL	`@. 000,00	10238±-15]	_0.00000_
-20404E-13	0.00000	-1u552E+00	0.00000	.28571E+00	0.00000	229296-01	~°0.00000	~.77352E-11	06000.0	81691E-14	0.00000
66278E-13	0,00000	10552E+Q0	0.00000	.28571E+00	0`.00000	22929E-01	0.00000	-77879E-11	0.00000	1 <u>7</u> 246 <u>-1</u> 3	_0.00000
32617E-13	0.00000	.56170E-01	_0.00000	13428E+00	0.00000	91002E-01	0 .000000	78657E-11	_ 0• <u>0</u> 00000_	.25535t-13	.0.00000
29465E-13	0.00000	501708-01	0.00000	-+13428E+00	0.00000	910026-01	0.00000	.78576E-11	0.00000	~25160E-13	~0.00000
.29164E-13	0.00000	72543E-01	0.00000	.33451E-01	0.00000	.15719E+00	0.00000	78923E-11	0.00000	.3939dE-13	0.00000
_+14403E-13	0.00000	•72543L-01	0.00000	.334518-01	_0.00000	15719E+00	0.00000	. •79154E-11	<u>ō</u> .000000	83384E-13	0.00000

		_ HATURA	ř Ł×rαnfμÇ.X≃¨	.9482588	+03 -						
TX REAL	TX .	. TY . REAL .	TY Imag " "	TZ REAL	TZ IMAG	RX Real	RX Imag	- RY REAL	RY. T	RZ RZ REAL IMAG	
93832E-14	0.00000	Ž47236-12	0.000001	0822E-12	0.00000	.54d85E-12	0.00000	• 31233E+00	0.000000)_
31455E-15	0.00000	_,299971-12	0.00000	5530E-13	0.00000	.50914#-12]	0.00000	31233E.+00	<u> </u>		<u> </u>
	0.00000	.17550i-12	0.00000 .4	28758-12	0.00000	255176-12	0.00000 -	.28176E+00	0.00000	~44627E-14 0.0000)
60995E-13	0.00500	144408-12	0.00000 .4	3263E-12	0.00000	33238E-12	0.00000 "	2817bE+00	~ 000000°	31047E-13 0.00000) _
33829E-14	0.00000	.29987E-12	0.00009	51-13866	0.00000	-,507928-13	0.00000	+223616+00	0.00000	.34070e-14 0.00000)
.70796E-13	0.00000	368936-12	0.000009	7169 <u>F</u> -12	0.00000	73683L-13	0.00000	22361E+00	0.00000	404276-15 0.0000) <u> </u>
-207551-13	0.00000	•30654L-12	0.00000 [.8	65551-12	0.00000	70394E-14	0.00000	14356E+0 <u>u</u> _	0.00000	-10370b-13 0.00000	三
827046-13	0.00000	428498-12	0.00000 ·q	6265 <u>E</u> _12_	0.00000	645226-14_	0.00000	14356E+00	_ 0.00000	-10000 <u>0</u> 000 <u>0</u> 0	<u>-</u>
14671E-13	0.00000	.220046-12	9.00000 2	4975Ē-Ī2 [—]	0.00000	38227=-12	0.00000	49469E-01	0.00000	~~.93979E-14_~0.00000	j
.43945E-13	0.00000	30409E-12	0.000002	2344E-12 _.	0.00000	425448-12	0.00000	49469E-01	0.00000	100595-13 0.0000	<u>)</u> _
576476-14	0.00000	18789E-12	0.00000 2	47176-12-	0.00000	+ 37 3034 -12	0.00000 1	49464E-01	0.00000	37224E-14-0.00000	<i>τ</i> .
570248-13	0.00000	.212578-12	0.000002	4785Ē-12	0.00000	.374556-12	0.00000	.49469E-01	0.00000	.15989E-13 <u>.0</u> .0000	<u>,</u>
-14907E-13	0.00000	292371-12	0.00000 .8	7319E-12	0.00000	.205141-14	0.0000	14356E+00	0.00010	.22959c-13 0.00000)_
-9238¤E-14	0.00000	.40783E-12	0.00000 .6	8700E−12	0.00000	350868-14	0.00000]	.14356E+00	0.00000	157926-13 0.00000	5]
33095E-13	0.00000	~_305006-12	_0.00000,9	6344E-12	0.00000	.76234E-13	0.00000	22361E+00	0.00000	468 <u>28</u> E-14 0.00000	<u>)</u>
.13479E-13	0.00000	.426241-12	0.000009	5729E-12	0.00000	.81636E-13	0.00000	.22361E+00	0.05000	415 î Î E-Î 4 - 0.090 9	ם –
-15481E-13	0.00000	20988E-12	0.00000 4	78076-12	0.00000	.12402L-12	0.00000 _	28176E+00	0.00000	~12823E-13 0.00000	ຼ
40264E-13	0.00000	.21442L-12	0.00000 .4	7614E-12	0.00000	·3J444E-12	0.00000	.281768+00	0.00000	.14170E-13 0.0000	ງຼັ
-304685-13	0.00000	-156628-12	0.00000 i	4005E-12	0.00000	51091E-12	0.00000	31233E+00	0.00000	.81694E-13 "0.0000) ".
89735E-14	0.00000	26007E-12	0.000001	4019E-12	0.00000	52207E-12	0.00000	+31233E+00	0.00000	27957E-130.6000	o

		HATURAL	. FREQUENC	Y <u></u> . 484469	£+03						
TX REAL 1	тx	<u></u>	TY	12	TZ	RX.	RX	RY -	KY "	RZ	RZ
-44950E-01 (0.00000 _	37695£-13	0.00000	• 41226E-13	_0.00000		0.00000	10040F-01	_0.00000		0.0000
44950E-01 (0.00000.	64469£-13	0.00000	.16949E-13		54636E-13	0.00000	16696E-01		- <u>. 1</u> 6035 <u>E+0</u> 0	0.00000
14844E+00 (o. 00 v o o	85907E-14 [*]]	0.00000 "	68832E-14		84117E-14	0.00000	120iu£+00	0*003.00	55926E-01	0.00000
.14844E+00	0.00000	31957E-13	0+00000	230508-13	_0.00000	278926-13	0.00000	12010E+00	0.00000	.55926E-01	0.0000
226118+00	0.00000	29900L-14	0.00000	• 30307E-13	0.00000	.42798E-14	0.00000	*\$10f2E+00	0.00000	16322E-01	[0.000000]
226112+09	0.00000	.208788-13	ó.00000 <u>.</u>	46 <u>8</u> 77E-13_	. 0.00000	13260E-15	0.00000	21015E+00		16,3226-01	0.00000
=•20095£+05 °	a.60000 ⁻	.78628E=14	0.00000	=-81672E-14	0.00000	25576E-13_	_0.00000	17748E+00	0.00000	.45817E-01	0.0000
_20095E+00 (o. 00000 <u>.</u>	. 480261-13	0.00000	68905E-14	0.00000	24043E-13	`0.00000	-,17740E+00	0.00000	458176-01	0.00001
.78343E-01	0.00000	.165966-13	0.00000_	56204E-13	0.00000	92314E-14_	0.00000	70821E-01	0.000000	B6603E-01	0.00000
78343E-01 1	0.00000	396526-13	0.00000	5,8331E-13		10598E-13	0.00000	708Z1É,-01	[0.000000]		0.00000
78343E-01 (00000.0		~0.000°	-20045E-13	<u>ื้อำจึจ็อออ่</u>	12355É-13			0.00000	10-3c0381	0.00000
78343E-01	0.00000	30d0dE-13	0.00000	213506-13	0.00000	~.96368E-14	0.00000	70821E-0i	[0.06300]	86603E-01	0.0000
-+20095E+00	0.00000	.18139E-13	0.00000	-482798-14	0.00000	34148E-13	0.00000	17748E+00	0.00000	45al7c-01	0.00000
20095E+00	0.00000	75530E-13.	_0.00000	.77249E-14	0.00000	13871E-13	0.00000.	17748E+00	0.00000	.458176-01	_0.00000_
.22611E+00	0.00000	.26679L-13	.0.00000	-, 14624£-15	0.00000	25382t-13	0.00000	-210158+00	0.00000	16322£-01	0.00000
22611E+00	0.0000	~~70932É-13	0.00005	10651E-13	0.00000	36345E-13	0.00000	_210158+00	_0:00000	-163 <u>2</u> 52 <u>-</u> 01	0.00000
14844E+00	0.00000	.359098-13	0.00000	36795E-i3	0.00000	83402t-14	0.00000	12018L÷00	0• ó00,00 _	.55926E-01	0.0000_
.14844E+00	0.00000	331466-13	0.00000	395068-13	0.00000	12321E-13	0.00000	12018E+00		55926£-01	0.000 <u>00</u>
-44950E-01	0.00000	.563826-13	0.00000	41916E-13	0.00000	.20765E-13	0.00000	.16696E-01	ío•ooooō ''	160358+00	0.00000
44950E-01	0.00000	.254186-13	`o.oooo, ~	.37948E-13	_0.00000	.183786-13	0.00000	.16696E-01	0.00000	.16035É.00	

NATURAL FALUULNCY=	.989d14E+UJ		
--------------------	-------------	--	--

TX REAL	TX Enag	. FY	TY IHAG	TZ . REAL	TZ IHAG	RX KEAL	RA I HAG	RY REAL	RY RZ RZ IMAG KEAL IMAG
.53495E-01	0.00000	63788E-13	0.00000	.30964E-13	0.00000	21353E-13	0.00000	- 26372E-11	0.0000023210E+00 0.00000
53495E-01	0.00000	.56287L-13	0.00000	.231426-13	_0.00000	.304681-13	0.00000	24801E-11	_0.0000023210E+00 0.00000
6326>E-02	0.00000	157176-13	0.00000	56168E-13	0.00000	47705E-14	0.00000	10757E-11	0.00000 .10972E+00 0.00000
-+632o5E-02	0.00000		0.00000	599d2E-13	0.00000	.373726-13	0.00000	-19496E-11	_ 0.00000 L0972E . 00 _ 0.0000
14137E+00	0.00000	~	0.00000		u.:00000	462868-14	0.00000	62277E-12	0.00000135335.00 0.00000
14137E+0J	0.00000	272976-13	0.00000	.3973jE-1j	0.00000	-,484075-15	0.00000	87430E-12	_0.00000[3533F.±00 0.000000
.23175E+00	0.00500	311070-13_	0.00000	~.35741E-L3	0.00000	289611-13] 0.000000	2325161 <u>T</u>	_0.0000083041E-01_0.00000
23175E+00	0.00000"	69960E-13	_0.00000_	46713Ê-13"	,0.00000	264706-13	0.00000	11139E-11	0.00000 -83041c-01 0.00000
28783E+00	ō•00000	.452348-14.	0.00000	.22528F-13	0.00000	.25703t-14	0.00000		0.0000031877g-01 0.00000
28788E+00	0.00000	470048-13	0.00000	+21444E-13	0,00000	782316-14	0.00000	27964E-11	0.00000 31879E-01 0.00000
28788E+00`	0.00000°	104586-13	0. องุ้ออบ	.47802E-13_	_0,00000	,-+45977E-14	0.00000	~22372E-1Į	0.0000031879E-01 0.00000
-28763£+00	0.00000	11424E-14	0.00000	-28131E-13	0.00000	13571É-13	0.00000	297978-11	0.0000031879E-01 0.00000
23175E+00	0.00000	122556-14	0.00000	640638-13	0.00000	.30782E-13	0.00000	.23066E-11	0.0000083041E-01 [0.00000]
23175E+00	0.00000	.58745E-L3	0.00000	514396-13	<u>_0</u> •00000				0.00000 .3304IE-01 0.00000
-14137E+00	0.00000	361201-13	0.0000	.23743E-13	0.00000	.28464E-13	0.00000	83054£-12	0.00000 13533=+00 -0.00000
-14137E+03	0.00000			31822E-13					0.0000013533E+00 _0.00000
-63265E-02	0.00000	13279E-13	_0.00000	25010E-13					0.00000 .104726+00 0.00000
•63265E±02	0.00000	.21950L-13	0.00000	.143058-13	0.00000	.20098E-14	0.00000	-20308E-11	0.00000 10972£.00 0.00000
53495E-01	3.90400	28104E-13	0.00000	23195E,-13	0.00000	19137è-13	0.00000	26468E-11	0.00000232102+00 _ 0.00003
534956-01	0.00.00	366722-13	0.00000	25529E-13	_0.00000	191196-13	0.00000	-25853E-11	0.00000232106+00 0.00000

NATURAL FREQUENCY= .790744E+03 TX IY TY TZ TZ RX RX RY KY RZ RZ IHAG REAL IHAG REAL IHAG REAL IHAG REAL IHAG REAL IHAG 37130E-12 0,00000 .20/214-13 0.00000 -.51634E-14 0.00000 .13146L-14 0.00000 .30075E+00 0.00000 -.15725E-11 0.000000 .37613E-12 0.00000 -.20263E-13 0.00000 .17545E-13 0.00000 -.45727E-13 0.00000 -.30075E 100 0.00000 -.15526E-11 0.00000 =-10649E-12 [0.00000]-.26347E-13 0.00000 .39127E-14 0.00000].10734E-13 0.00000]-18587E+00 0.00000] 72721E-12 0.00000 -.80308E-13 0.00000 -.31264E-13 0.00000 -.12262E-13 0.00000 -.13191E-13 0.00000 -.18587E+00 0.00000 -.74529E-12 0.00000 --89034E-12 0.00000 -.55855E-13 0.00000 .37214E-13 0.00000 .36195L-13 0.00000 .33747E-12 0.00000 -.67636E-12 0.00000 --93421E-12 0.00000 .37531E-13 0.00000 2.26013E-13 0.00000 0.00000 -.24701E-12 0.0000 -.92429E-12 0.00000 -14926E-11 0.00000 -.35365E-14 0.00000 .73287E-14 0.00000 -.90515E-14 0.00000 -.18587E+00 0.00000 .57163E-12 0.00000 -15561E-11 0.00000 .29284E-13 0.00000 .5864>E-14 0.00000 -.14539E-13 0.00000 .18587E+00 0.00000 .572ddE-12 0.00000 --18900E-11 .0.00000 -27665L-13 0.00000 -.58687E-13 0.00000 -.20168E-14 0.00000 -.30075E+00 0.00000 -.24208E-12 0.00000 -.19151E-11 0.00000 .31437E-14 0.00000 -.55641E-13 0.00000 -.21812E-13 0.00000 .30075E+00 0.00000 -.20752E-12 0.00000 -19148E-11 0.00000 -.44000E-13 0.00000 -.12022E-13 0.00000 -42853E-15 0.00000 -.3007>E+00 0.00000 -.1980@E-12 0.00000 .18794E-11 0.00000 -.52493E-13 0.00000 .41203E-14 0.00000 -.41192E-14 0.00000 .30075E+00 0.00000 -.20167E-12 0.00000 --15514E-11 0.00000 .44346E-13 0.00000 .27182E-13 0.00000 --20050E-13 0.00000 --18587E+00 0.00000 .57717E-12 0.00000 #.15102E-11 0.00000 -.61126E-13 0.00000 .28263E-13 0.00000 -.7/287E-13 0.00000 .18587E+00 0.00000 .56456E-12 0.00000 -94481E-12 0.00000 --32159E-14 0.00000 --67270E-13 0.00000 -43161E-13 0.00000 --24456E-12 0.00000 --88832E-12 0.00000 .92605E-12 0.00000 .12256E-13 0.00000 -.68437E-13 0.00000 .10978E-13 0.00000 .26906E-12 0.00000 -.88017E-12 0.00000 _47928E-13 0.00000 _-.54131E-13_ 0.00000 __.11242E-12 0.00000 .36595E-13_ 0.00000 _.18587E+00_0.00000 _.71347E-12_0.00000 .56482E-13 0.00000 _ .49177E-13 0.00000 .13794E-12 _ 0.00000 .31414E-13 0.00000 _ -.18587E+00 _ 0.00000 _ .74925E-12 _ 0.00000 --34314E-12 0.00000 --71548E-13 0.00000 --51355E-13 0.00000 --57912L-14 0.00000 -30075E+00 0.00000 --15344E-11 0.00000

NATURAL FREQUENCY= .1	02477E+04
-----------------------	-----------

NATURAL FREQUENCY = 102477E+04
TX TX TY TY TZ TZ RX RX RY RY RX RZ RZ RZ RZ REAL IMAG REAL IMAG REAL IMAG REAL IMAG REAL IMAG
-13645E-13 0.0000022336L+00 0.00000 11262E+00 0.00000 .85954E-01 0.0000013071E-12 0.00000 131515E-13 0.00000
22537E-13 0.0000044763E-01 0.0000019882E+00 0.00000 :13673E-01 0.0000074552E-13 0.0000023812E-13 0.00000
54040E-14 0.00000 .44763E-01 0.00000 -194862E+00 0.00000 .13673L-01 0.00000 .11796E-12 0.00000 -94916L-14 0.00000
-29691E-14 0.00300 : .16728E+00 0.00003 71852E-01 0.00000 -57623E-01 0.00000 -20506E-13 0.00000 -115116-13 0.00000
21803E-13
622446-14 0.00000 .250036.00 ,0.00000697126-01 0.00000136306.00 0.00000 -107046-12 0.00000401826-13 0.00000
E.36100E-13 G.0000025003E+00 0.0000069712E-01 0.0000013630E+00 0.0000062467E-13 0.0000027954E-13 0.00000
-31063E-13 0.00000 -10636L+00 0.00000 84056E-01 0.0000016740E-01 0.00000 84173E-13 0.00000 34637E-13 0.00000
40311E-13 0.0000010636E+00 0.000000 .84056E-01_0.0000016740E-01 0.0000079474E-13 0.00000 -29015E-13 0.00000
-19436E-13 0.00000 -10636E+00 0.00000 -04056E-01 0.00000 -16740E-01 0.00000 17036E-13 0.00000 -28877E-13 0.00000
-28352E-13 0.00000 .10636+00 0.00000 .84056E-01 0.00000 .10740E-01 0.0000043836E-13 0.00000 .61344E-14 0.00000
36729E-13 0.0000025003E 00 0.0000069712E-01 0.0000013630E+00 0.00000646970E-13 0.0000013819E-13 0.00000
.21333E-13 0.00000 .25003E-00 0.0000069712E-01 0.00000 .13030E+00 0.0000019157E-13 0.00000 .20050E-13 0.00000
-52/705E-14 0.0000016728E+00 0.00000 -71852E-01 0.00000 -555363E-13 0.0000010351E-13 0.00003
-31282E-13 0.00000 -16728E+00 0.00000 -71852E-01 0.00000 -57623E-01 0.0000021301E-13 0.00000 -27192E-13 0.00000
_43979E-13 0.00000 .44763E-01 0.0000019882E+00 .0.0000013673E-01 0.0000047396E-13 0.00000 -27750E-13 0.00000
=.30648E-13 0.0000044753E-01 0.0000019882E+00 0.0000013673E-01 0.0000075473E-14 0.0000018433E-13 0.00000
12255E-13 0.00000 .22336L+00 0.0000011262E+00 0.0000085954L-01 0.0000047406E-13 0.0000033466E-13 0.00000
59443E-14 J.0000022336E+00 0.00000 .11262E+00 0.0000085954E-01 0.0000038436E-13 0.00000 .44472E-13 0.00000

REPART BULLDIES FORMS IN 37

NATURAL	FREQUENCY	-103705E+04

TX REAL	TX .	TY	TY -	TZ	TZ THAG	RA	RK IMAG –	RY	ÂY IHAG	REAL	RZ IHAG
		645676-02						43491E-12			
-28379E-13	0.00500	64569E-02	~o.ooooo_	366906-01	0.00000		0.00000	•52834E-12	a: 00 à <u>0</u> (ō_	.11769£-12	0.00000
-34190L-13	0.00000	-57364L-01		*10643E+00	000000	79287É-0Î	0.00000	12014E-12	0.00000	34839E-13	_0.00000_
•86338E-13	0.00000	5%364E-01	0.00000	.106838+00	0.00900	79287E-01	0.00000	•59362E-13	0.00000	302392-13	0.00000
-28490E-13	0.00000	-25774E-01	″ 0.00000¯	19854E+00	0.00000	.36118E-01	0.00000	.39957É-12 "	0.00000	.718201-13	_0.0000
66669E-13	0.00000	~25774E-01	0.00,000	19854E+00	0.00000	-3ali8t-01	0.00000	~.32121E-12 "	0.00000	- •37604F-73.	
522038-13	3.00000	.12511t-02	0.00000	.286671+00	0.00000	30843L-01	0.00000	.50838E-12	0.00000	15042c-13	0.00000
.79017E-13	0.00000	125116-02	.0.0000	28667E+00	0.00000	30843E-01	0.00000	61468E-12	.u• ōo ōo o_	109041-13	0.00000
-44638E-13	0.000000	34375£-01	0.00000	30535£+00	0.00000	.304720-01	0.0000	38093E-12	0.00000		0.00000
1-671438-13	0.00000	.44375L-01	0.00000	305356+00	0.00000	.304721-01	0.00000	24455E-12	0.00300	.16701c-13	0.00000
66227E-13	0.00000	44375E-01	0.00000	30535E+00	0.00000	.30472E-01	0.00000	28705E-12	0.00000	20004t-13	0.00000
.69895E-13	0.00000	.44375E-01		.30535E+00		.3047ZE-01	_ 0 <u>*</u> 0000 <u>0</u>	19407E-12	0.00000	12201E-13	0.00000
-26567E-13	0.00000	-12511E-02	0.00000	-,.28667E+00		'30843E-01	0.00000	,56388E-12	0.000,00	.24760E-13	_0•00000_
523286-13	0.00000	12511E-02	0.00000	- 28667E+00	0.00000	300436-01	0.00000	.06921E-12	0.00000	13412E-13	0.00000
48116E-13	ñ*09000	25774E-01	_0.00000	198546+00	0.00000	.36118E-01	0.00000	4330dE-12	0.00000	.22720E-13	0.00000
38213E-13	`` v . ooooo	25774E-01	0.00000	.198546+00	0.00000		0.00000	.45516E-12	0.00000	69904E-14	0.00000
53781E-14	0. 00000		_0.00000	10683E+00	000000	792871-01	3.00000	-864Óy£-13` <u>_</u>		24215t-13	0.00000
.92291E-14	0.00000	593641-01	0.00000	10683E+00	_0.00000	79287L-01	0.00000	6053dE-13	0.00000		0.00000
14810L-13	ŭ*002 <i>0</i> 0	64569L-02	0.00000	.36690L-01	0.00000	.856621-01	0.00000	.55516E-12_	0.00000	.24635E-13	0.00000
176248-13	0.00000	645646-02	0.00000	.36690E-01	0.00000	.8>662E-01	0.00000	571676-12	0.00000	27519e- <u>1</u> 3	0.00000

		NATURAL	- ÈŘFONFÝČ	Y=1044081	L+04						
TX REAL	THAG	KLAL	TY IMAG.	TZ REAL	ÎHĂC .	RX Real	RX IHAG	RY REAL	THAG .	REAL	R2 'IMAG
-1960 JE-01	0.00000 -:	65.984E=13	0.00000	.31907E-13	ŏ*0 <u>0</u> 000	. 184358-13	0.00000	436708-02	0.00000	11099£+00	0.00000
.1968)E-01	0.000,00	34540E-13	0.00000	57240 <u>E</u> _13_	_0. <u>0</u> 00000	143676-13	_0.0000 <u>0</u>	436706-02	0.0000	.11099E+00	0.60000
~73347E-01	0.00000	41054L-13	0.00000	, 194736-13	0.00060	.75658E-13	0.00000	.592216-01	0.00300	. 444388-01	1 3.00000
73349E-01	0.00000 .	23519E-13	"ผ•ย0ยผงุ	64972E-13	0.00000	20770E-13	0.00000	.59221E-01	₫ <u>*</u> 00000	444386-0	L0.00000_
14742E+00	0.00000 .	376168-13.		21240E-13_	0.00000	24593E-13	0.00000	14900E+00	0.00000	46836E-01	r 0.00000
.14742E+00	0.00000	569536-16	0.00000	26758E-13	0.00000	11660E-14	ğ. v0000ğ	14900E+00	0.00000	. 468 36E - 01	r 0.00000 <u>0</u>
-20718E+00	0.00000 .	52852E-13	0.00000	41871E-13	0.00000	16707E-13	0.00000	. 19485E+00	0.00000	30795E-01	r _0:00000 _
20715E+G0	0.00000	577936-13	0.00003	-1523998-13	0.00000	203991-13	0.00000	.194851+00	0.00000	[30/95b-0]	1_0.00001
23548E+00	0.00000	36,1158-13	0.00000"	.65024E-13	0.00000	669270-14	0.00000	225856+00	_0.000 00,	98881L-0	2 0.0000
-23548E+00	0.00000	59516L-13	0.00000	,.62779E-13	0.00000	14708E-13	0.00000	22585E+00	0.00000	98881E-03	2 0.00000
~Z3548E+00	"0.00000 " -:	147,36E-13.	"0.00000" _.	- <u>-</u> 583906-13	0.60000	105301-13	.0.0000_	.22585E+00°	0.00000	3899_FE-05	5_0.0000
-23548E+00	0.00000	1770aL-13 -	0.00000	58402E-13	0.00060	141498-13	0.00000	.22585E+00	-0-0096 <u>0</u>	988 <u>31c-0</u> ;	2 0.00000
-+20718E+00	0.00000	19573L-13	0.0000	.25497E-13	0.00000	.54061E-13	0.00000	19485E+ÕÕ	0.00000	.30795e-01	1 0.00000
.20718E+03	0.00000 .	58931E-13 .	.o.oooo -	1,3883E-13	0.00000	.34583E-13	0.00000	194858+00	_0,00000	`307 <u>25</u> È-0	r0*00000
•14742E+00	0.00000	128384-13	0.00000	55226E-14	0.00060	.1>254c-13	0.00000	~.14900E+00	0.00000]		L_0.00000
:-14742E+00	0.00000	561536-13	0.00000	.70766Ë-14	0.00000	.30180E-14	0.00000	.14900E+00T	9.00000	46836E-0	1 0.00000
73349E-01	0.00000	391005-14	0,00000	12914E-13	0.00000	.65496E-14	0.00000	59221E-01	0.00000	4443dL-0	10.00000
[.73349E-01	0.00000	175201-14	0.00000	11876E-13	0.00000	.107846-13	0,00000	59221E-01	0.00000	444386-0	10.00000
.19669E-01	0.00000 .	737926-14.	0.00000	-201256-13	0.00000	27782c-13	0.00000	43670E-02	5.00000	110996+0	0.03000
-19689E-0L	0.00000	62365E-13	_0.00000 .	20223É-13	0.00000	28297E-13	0.00000	43670E-02	0.00000	110976+0	o o o o o o o o o o

TX TX	IY IY	1/ ' 1/	QΥ	BX . BA			
REAL THAG	TY TY	REAL IHAG	REAL	RX RY THAG THEAL	THÁG T	REAL	L'HAG
14796E-13_0,00000	97427E-13 0.00000	13386E-12 0,000	000 -22275E-12	0.0000028176E+0	0 00 000 00 -	24557 <u>6-</u> 13	0.00000
91327E-14 0.00000	1009512 0.00000	12722 <u>E</u> _12 _ 0.00	000 1 .26495E-12	0.0000028176E+0	0 00000 -	123335-14	0.00000
38779E-1+ 0.00000	.220836-12 0.00000	.32576E-12 0.000	00024242E-12	0.00000 .49469E-0	0.00000	441796-13	0.00000
56429E-13 0.00000	1163iE-12 0.00000°	.32606E-12 .0.000	00024116E-12	0.00000494698-0	i 0.00000 .	437376-113	_0.00000
68121E-14 0.00000	.20555t,-12 0.00005	55950E-12 0.000	000 .12796L-12	0.0000022361E+0	0.00000	104496-13	
.53894E-13 0.00000	.93936E-13 0.00000	54575E-12 0.000	000 .10460E~12	0.00000 .22361E+0	0.00300, **	279716-13	0.00000
-24177E-13 0.00000	78460E-14 .0.00000	84269E-12 0,000	000 57143t-13	0.00000 -31233E+0	0 . 0 . 0 0 0 0 0	1,7057E- <u>1</u> 3_	0.00000
12767E-13 0.00000	-69972E-13_0.00000	.d3946E-120.000	100 - .8442dE-13	0.00000 .31233E+0		,53827E <u>-</u> 14]	
74024E-13 0.00000	27298L-12 0.00000	90165E-12 0.000	000 :7 2109E-13	0.0000014356E+0	0,000,000	.176426-13	0.00000
38066E-13 0.00000	.16197E-14 0.00000	91617E-12 0.000	.11602E-12	0.00000 .14356E+	0 00 00 00 00	452334-13_	0.00005
61593E-13 0.00000	231316-12 0.00000	.87207E-12 0.000	000 -78210E-13	0.00000 .143566+0	0 0.00000 -	218766-13	0.00000
20121E-13 0.00000	30583E-13 _0.00000		000 +65311t-13	0.00000143568+0		.30837E-14	0.00000
72795E-13 0.00000	848238-13 0.00000		000 °97740€-13	0.0000031233E+0	0.00000	49656 <u>2</u> 13	0.00000
59251E-13 0.00000	.17410E-13 0.00000	-,84364E-12_ 0.000	000107716-12	0.0000031233E+0	o <u>" o oo</u> ouo"	540276-13	0.0000
-15800E-13 0.00000	.26847E-12 0.00000	-58027E-12 0.000	060 -10592E-12	0.00000 .22361E+0	0.00000 ==	.305596-13	0.00000
±.30220E-13 0.00000	76224E-13 _0.00000	57053E-12 0.000	00 - •939536-13	0.0000022361E+0	0.00000 -	.12296E-13	0.00000
25275E-14 0.00000	.23147E-12_0.00000	27853E-I2 0.000	(0023399Ê-12	0.0000049469E-	1 0.0000	.4 <u>3930E-1</u> 3	0.00000
.99399E-13 0.00000	14079E-12_0.00000	28110È-12 0.000)0023829E-12	0.00000 .49469E-	01 0.00000	.137152-13	
74008E-13 0.00000	16736E-12 0.00000	.95021E-13 0.000	000 .273656-12	0.0000028176E+0	0.00000 -	.974036-13	0.00000
45191E-15 0.00000	14620E_120_00000	-41043E-13 D.000	10026913E-12	0.00000 .28176£+0	og_u.ogugoj	·1712596-15"	0.00000

MATURAL FREQUENCY= __.109690=+04 __ YX ΤY TZ 17 КX КX REAL JHAG REAL IMAG REAL IHAG -.18482E-13 0.00000 .869495-14 0.00000 --25583E+00 0.00000 -.31009E-13 0.00000 -.43844E-13 0.00000 .29151E-13 0.00000 --233696-13 0.00000 -.25583c+00 0.00000 .-20584E-13 0.00000 .70707E-13 0.00000 .40291e-13 0.00000 .135976-13 0.00000 .24297E-14 0.00000 .97720b-01 0.00000 -44083L-14 0.00000 --209265-13 0.00000 -.9611dE-13 0.00000 .32884E-13 0.00000° -3d234E-13 0.00000 .977208-01 0.00000 -.43507E-13 0.00000 .94085E-13 0.00000 .11830E-13 0.00000 -1406ZE-13 0.00000 -.34014ë-13 0.00000 -31023£+00 0.03000 .35958C-13 .29836E-13 0.00000 -.14362E-13 0.00000 0.00000 -.37207E-13 0.00000 -30914E-13 0.00000 0.00000 .31623£ .00 -16958E-13 0.00000 .37220E-13 0.00000 -7522dE-13 0.00000 -.25504e-13 0.00000 -.38332E-13 0.00000 . .97720E-01 0.00000 -.35261E-13 0.00000 --282216-13 .22500E-12 0.00000 .81879E-14 0.00000 0.00000 -42506E-14 0.00000 .97720L-01 0.00000 -- 42061E-14 0.00000 -.48979E-13 0.00000 --154676-12 0.00000 .34253E-13 0.00000 -.23027E-13 0.00000 -.25533£+00 0.00000° 0.00000 .31283E-12 0.00000 .89255E-14 0.00000 __.43067E-13 0.00000 .26901L-13 -30374E-13 0.00000 --25583E+00 0.00000 -10603E-14 0.00000 -10467E-13 0.00000 -.27817E-12 0.00000 -11822E-13 0.00000 .83807E-14 0.00000 --25583E-00 0.00000 _-78999E-14 0.00000 -.43978E-14 0.00000 .84224E-13 0.0000 -.22849E-13 0.00000 -56143E-14 0.00000 -.25583E+00 0.00000 .28057E-13 0.00000 .157766-14 0.00000 -.343836-13 0.00000 -.956836-14 0.00000 .80368E-15 0.00000 .977206-01 0.00000 -.10095E-13 0.00000 -39385L-13 0.00000 -.3205LE-12 0.00000 -.216526-13 0.00000 --25072E-14 0.0000 -97720E-01 0.00000 -- 74692E-14 0.00000 1.13561E-13 0.00000 30084E-12 0.00000 39295E-13 0.00000 .31623E+00 0.00000 .76115E-14 0.00000 .98079E-14 0.00000 -.41094E-12 0.00000 --10323E-13 0.00000 -28191E-13 0.00000 -31623E+00 0.00000 -24079E-13 0.00000 -21073E-13 0.00000 -35822E-12 0.00000 --22093E-13 0.00000 -26880E-14 0.00000 -.12050E-14 0.00000 .97720E-01 0.00000 -.53584E-13 0.00000 .15722E-13 0.00000 .54688E-13 0.00000 .54688E-13 0.00000 --197728-13 0.00000 --255838+00 0.00000 116228-13 0.00000 --275878-13 0.00000 --471458-12 0.00000 --673698-13 0.00000 75098E-14 0.00000 -.25583E+00 0.00000 -.11372E-13 0.00000 -.34532E-14 0.00000 -.42162E-12 0.00000 .46921E-13 0.00000

	,	NA TURAL	. FREQUEN	CÝ= .112863	E+04						
T.A Real	TX IHAG	TY .	TY IMAG	TZ .	T Z I mag	K X K E A L	RX EHAG	RY Real	IHAG -	REAL	
.33689E-13	0.00000	.222396-12	0.00000	.182776-13	0.00000	.29623E-13	0.00000	.25583E+00	0.00000	.93808E-14	, -
-10627E-13	0.00000	.281958-12	0.00000	-1495dE-13	0.00000	.215466-13	0.00000	25583E+00	0.00000	101566-12	
11407E-13	0.00000	10353E-12	0.03000	553138-13	0.00000	19611E-13	0.00000	97720E-01	0.00000	16244E-13	•
819586-13	0.00000	79188E-13	0.00000	329G8E-13	0.00000	14389E-13	0.00000	.97720E-01	0.00000	995436-14]	_o•ooooo
.267646-13	0.00000	30651E-12	0.00000	.69085E-13	_0.00000	.46783E-13	0.00000	31623E+00	0.00000	. •212426-13.	o <u>•</u> 03000
-661216-14	0.00000	31535E-12	0.00000	. 40113E-13	0.00000	19203E-14	0.00000	.31623E+G0	0.00000	.19473E-14	0.00000
.32151E-14	0.00000	57721E-13	0.00000	36247E-13	_ 0.00000	57886E-13	0.00000	97720E-01	0.00000	.12875c <u>-</u> 13	0.00020
51601E-14	0.00000	12 /526-12	0.00000	497508-13	_ û * 00 0 00	40350E-13	0.00000	.97720E-01	0.00000	17440E-13	0.00000
20326E-13	0.00000	[.21735E-12	0.00000	.20438E-13	_0.00000	.37255c-13	0.00000	25583E+00		48505E-13	0.00000
107435-13	0.00000	.20250E-12	0.00000	78463E-13	0.00000	.645556-13	0.00000	25583E+Q0	0.00000	-42865=-13	0.00000
.16593E-14	_0.00000	.23547E-12	0.00000	18747£-13	^^ 0. 000000	~19431E-13	0.00000	25583E+Q0_	0.00000	36331E-14	0.00000
-43095E-L3	0.00000	.25892L-12	0,00000	.76021E-15	0.00000	35120E-13	0.00000	25583E+00	0.00000		_0.00000
77833E-13	0.00000	96405E-13	0.00000	.100878-13				97720E-01	0.000 <u>0</u>	-11404E-13	0.00000
-90401L-14	_0.00000		0.00000	-40836E-11		369.j1g-13_	0*30000		0.00000	31589E-14	0.00000
2563JE-13	0.00000	27305E-12_	0.00000	-,37528E-13	0.00000	185146-13	_0.0ō0 <u>0</u> 0	316236+00	0.00000	.27276E-13	0.00000
46198E-13	0.0000	341716-12	0.00000	13274 <u>6-13</u>		41880E-13	<u>0</u> .000 <u>0</u> 0	• 3 fes 3F+00		.25479=-13	0.00000
72128E-13	0.00000	68748E-13	0.00000	43918E-13	~ a'₊aoaōo	.41722E-14	0.00000	977208-01	0000000		
85906E-14	J.00000	12434 <u>e</u> -12	0.00000			~.17372E-13	0•00000	97720E-01	<u>ō</u> •oōnôō	19488E-13	0.00000
4591oE-13				172126-13			0.00000	25583E+00	0.00000	46859E-13	0.00000
-814265-13	.0.00000	.26336E-12	0,00000	~22460E-13	- 0.00000	~70604E-14	_ 0.00000	25583£+00	_0.00000	65768E-13	0.00000

Market per II or lower, the H

NATURAL FREQUENCY - .113131E+04

TX _ REAL	XI DAH1	TY .	TY	T.Z KEAL	TZ IHAG	RX Real	KK IHAG	RY REAL	Y DAM1	KEAL THAC
.15597E+0J	0.00000	73070E-13	0.00000	.347828-13	0.00000	553028-13	0.00000	.26599E-12	0.00000	37940=+00_ 0.00003
•15597£+0u	0.0000	.50310E-13	0.00000	-14072E-13		.L4789E-12	0.00000	321568-12	0.00000	37940E+00 0.00000
20667E+00	0.00000	.17533€-13	0.00000	72030L-13	0.00000	205766-13	0.00000	13791E-12	0.00000	.48199±-01 0.000000 j
-20667E+0J	0.00000	.152818-13	0.00000	.363s5E-13	0.00000	37890é-13	0.00000	.14512E-12	0.00300	.48199E-01 0.0000J
*10092E+00	0.00000	.87977E-13	0.00000	10434E-12	0.00000	135816-13	0.00000	59189E-12	0.00000	13021=+00 0.00000
-100851+00	0.09050	84708E-14	0.00000	51864E-13	0.00000	13573E-13	0.00000	•30457£-12	0.00000_	1302t=+00 0.00000
-68627E-01	0.00000	.441526-13	0.00000	.639971-13	0.00000	204526-13	0.00000	50770E-13	0.00000	.76572E-01 0.00000
686276-01	0.00000	333586-13	0.00000	147220E~13	0.00000	.13330b-14	0.00000	_ 33670E-12	0.00000	.76572E-01 0.00000
.18471E-01				299765-13	0.00300	122666-13				81504E-01-0.00000
-184716-01	0.00000	27365E-13	0.00000	415648-13	0.00000					81504E-01 0.00005
[.18471E-01	0.00000	330566-13	0.00000	.64887E-1J	0.00000	-29476E-14	0.00000	-4850oE-12	~ 0000go	.81504E-01 0.00000
-18471£-01	0.00000	. 25665E-14	0.00000	34859E-13	0_000000	+22645t-13	0.00000	22114E-12	0.00000	.81504£-01_0.0000J
68627E-01	0.00000	31>74E-13	0.0000	381846-13		.10169E-13	0.00000	112835E-12	0.00000	76572E-01 0.00000
		39198Ě-13				-				76572=-01_0.00000
100858+00	3.00000	-12087£-13	600000	1124516-13	o . `00 v00 `	.29896E-13	`Ö•000ÓU	32802L-12	0.00000	130216+00 0.00005
.+10085E+00	.0.00000	. 745386-13	0.00000	11672E-13	_ 0.00000	.31103±-13	ó•n000g	408878-12	0.00000	*13051F+00 0.00000
										48199E-01 0.00000
20667E+00	0.00000	-44085E-14	~0.000 00	.35619E-L5	-0.00000	38430c-14	0.00000	.533816-13		48199E-01 0.00000
155978+03	, ງ• 00010	20103E-13	0.00000	"d5959E-14	0.00000	631286-14	0.00000	28158E-12	0.00000	.37940E+00 _0.00000
155975+00	0.00000	229628-13	0.00000	11023E~13	0.00000	53146E-14	0•00000	33649E-12	_0.000000	.37940E+00 0.00000

NATURAL FREQUENCY .114542E+04

TX REAL	TX TY KEAL .	TY INAG	TZ REAL	TZ IMAG	RX Real [RX I MAG	RY REAL	RY THAG	RZ	RZ MAG
	0.00000281298-1	3 0.00000	133168-13	0.00000	.395706-13	0.00000	.43041E-12	0.00000	.36426E+ <u>0</u> 00	0 <u>0</u> 0000
.15747E+00	0.00000 .41627E-1	3 0.00000	60946E-13	0.00000	90759c-13	0.00000	.34017E-12	0.00000	364266+00	0.00000
.21803E+00	U.00000 .25044L-1	3 0.00000	114726-13	3.00000	77859£-14	0.00000	-80067E-13	0.00000 [-	.21696L-01(0.00000
.21803E+0J	0.0000069723E-L	i ο.υοουο :	20986E-13	0.00000	10884E-13	0.00000	.12341E-13	0.00000	. 510.065 <u>_0</u> 1(0.00000
13226E+00	0.00000 .136241-1	3 0.00000 -	31266E-13	0.00000	94957£-14	0.00000	-19407E-13]		. 95833 <u>=</u> _0 <u>1</u> _0	0.00000
132258+00	0.00000 .154346-1	3 0.00000	25943E-13	0.00000	11/81E-14	o'• ca o o ó	.11531E-12	_0.00000	.95033 <u>e-01</u> !	0.00000
*12396E*00	0.00000 .28929E-1	3.0.00000	38687E-13	0.00000	.43371E-14	0.00000	_15065E-13	0.00000 -	.250d0t-01	0.00000
.12396E+00	0.0000037929E-1	3 0.00000	-,39480E-13_	0.00000	. 17180L-14	0.00000	19986E-12_	0.00000 -	. 250806-01	0.00000
10676E+0J	0.00000 .43935E-1	3 (0.00000	-67741E-13	0,00000	20180L-13	0.00000	43375E-13	0.00000	1752 JE -01	ច្ចិច១០១១
-,10676E+00	0.00000441631-1	3_0.00000	65537E-13`	0.00000	74732E-14	0.00000	12183E _ _12	0.00000	. 17523E-01	0.00000
•10676E+00	0.00000 .311526-1	3 0.00000	37319E-13	000000	42773E-13	*0.03000	.12278È-12	`0.00000	•17523E-01	ġ• <u>0</u> 9000
.10676E+U0	0.00000 <u></u> .407524-1	30.00000	36258E-13_	_0.00000.	25426t-13	_0.00000_	17470E_12	_0.00000	175236-01	0.0000
123768+00	0.0000013419E-1	3_0.000000	73988É-13_	0.00000	.46364E-13.	0.00000	-23866E-13	0 • 000 00 - _	[25080E=01]	ō•0 <u>0</u> 0000
12396E+00	0.0000038148E-1	3 _0.00000		_0,00000	11063E-13	0.00000	42246E-13	_o. ōoooo _=	. <u>2</u> 5080 <u>2</u> -01	0.0000
•1322oE+00	0.000,0039365¢-1	.3 0.00000	45912L-13	0.00000	.20148E-13	_0.00000	•5,7653E-13	0.00000	.95333 <u>E</u> -01	<u>o•</u> 00005
.13226E+00	0.00000 .49927E-	3_0.00000_	31138E-13	0.00000	.76360E-14	0.00000	45739E-13	0.00000	.95833E-01	0.0000
21803E+UO	0.0000049035E-1	3 0.00000	-10903E-13	_0.00000	.37461E-13	0.00000	185428-13	0.00000	.21696E-01 -	0.00000
21803E+00	0.0000043065E-1	3_0.00000	Z4183E-13	_0.00000	31175E-13	0.00000	67484E-13	_0.00000 <u>_</u>	.21696E-0 <u>1</u>	0.0000
	0.0000030066E-1									
.15747E+00	0.0000022218E-1	3 0.00000	17452E-13		211851-13	0.00000	19871L-13	0-00000	·36426E+00]	0.00000

NATURAL FREQUENCY= .118472E+04

TX	TX IHAG	TY .	TY IMAG	TZ REAL	TZ 1HAG	kX KEAL	RX Imag	RY REAL	RY IMAG	RZ REAL	RZ
•94264E-14	0.00000	.173181+00	0.00000	64245E-01	0.00000	19199L+00	0.00000	413576-13	0.00000	.16511t-12	0.00000
-532716-14	0.00000	179186+00	0.00000	64245E-01	`j.00000	~.19199E+00	0.00000	13792E-12	6.00000	21467E-12	0.00000
-17127E-13	0.00000	113192+00	0.00000	•14612E+0U	0.00000	.80740E-01	0.00000	.71632E-13.	0.00000	29757E-13	0.00000
11759E-14	0.03000	•11819L+00	0.00000	.146126+00	0.00000	.80740=-01	0.00000	.16857E-12	u.00000	653111-13	0.00000
27170E-13	0.00000	24336E+00	0.00000	53985E-01	0.00000	•11036E+0Ô	0.00000	~535456-13°	_0.00000 <u>_</u>	~25892L-13	0.00000
.15255E-13	0.00000	.243,36E+00	0.00000	539a5E-01	0.00000	+11036E+00	000000	38794t-13	0.00000	.351576-13.	0.00000
-26177E-13	0.00000	64114E-01	0.00000	36605E-01	0.00000	.430626-01	0.0000	65236E-13	0.00000	47358t-13	0.00000
163186-13	_0.00000	641141-01	0.00000	36605E-0I	0.00000	.43062E-01	0.00000	373258-13	0.00000	.276986-13	0.00000
5413JE-14	0.00000	.20458É+00	0.60000	~~.63127E-01	~o.00000	112i2L+00	0.00000	27642E-13	ັ້ງຄືວ່ວດດວ່າ ຼື		0.0000
28062E-13	0.00000	20458£+00	0.00000	63127E-01	0.00000	11515F+00	0.00000	5958E-13]	0.00000	69357E-14_	0.30003
13645E-13	0.00000	- 204536+00_	0.00000	.63127€-01	0.00000	11212L+00	0.00000		_0.00100	.67930E-13	0.00000
243458-14	0.00000	204582±00	0.00000	6312?E-01	0.00000	11212E+00	0,00000	61148E-13	0.00000	922416_13_	0.00000
49091E-13	0.00000	64114E-01	0.00000	14602E01_	0.00000	.43062E-Ő1	0.00000	-62997E-13	្ត់ ច្នុំ១០០០០	14438E-13	0.00000
20345E-13	a. 00j000		0.00000	36605E-01	0,00000	+43062E-01	0.00000	12024E-12	0.000000	732256-13	0.00000
•47611E-13	0.00000	243360+00	0.00000	.53985E-01	0.00000	· .11036E+00	0.00000	18036È-IZ	o. ŏou oo ¨	71804E-13	
38851Ê-13	0.00000	-24336L+00	0.00000	53965E-01	0.00000	•11036E+00	0.00000	.20776[-13	0.00000	32760g-13_	0.00000
88654E-13,	[0.00000]		_o <u>.</u> ō o <u>o o o</u> .	14612E+00		86940E-01_	0.0000	25615E- <u>i</u> 2	0.000.00	56006E-13	0.00000
50299E-13	0.00000	•11819E+00	0 ∓ ဝဝ်ဝိစၥ	14612E+00	0.00000	-88940E-01	0.00000	91416E-14	0.00000	· · 212446-13	<u>_0.0</u> 00 <u>0</u> 0
•68725E-13	0.*00*30	.170138+00	0.00000	• 64247E-01	ง.งว่งบง	19199E+00	0.00000	•51138E-14	0.00000	143486-13	0.02007
116306-12	0.00000	1/8185+00	0.00000	.64245E-01	0.00000	19199±+00	0.00000	229868-12	v.gavoo_	102736-12	0.00000

NATURAL FREQUENCY= .119231E+04

TX PEAL	TX . IHAG	TY Real	TY IMAG	TZ REAL	TZ I HAG	RX REAL	RX Imag	RY REAL	RY IMAG	REAL	RZ IHAG
										26328E-12	
•73829E-13	0.00000	427946-12	0.00000	19870E+00	`p.00000.	.42654L+00	0.00000	42260É_12		10 <u>843E_12</u>	ō • go gọ g
.86074E-13	0.00000	290106-12	0.00000	112626+00	0.00000	105546+00	0.00000	92907E-13	0.00000	.61549E-13]	0.00000
•14735E-13	0.00000	.295138-12.	0.00000	11262E+00	0.00000	.10554L+00	0.00000	.208816-12	_0.0000 <u>0</u> _	50179E-13	0.00000
										27515E-13	
-22811E-13	0.00000	.605256-12	๊อ.อุวอุก <u>ว</u> ั		_0.00000	35349E-01	0.00000	_ •22443E-12	0 • 00 ½ ç o	104536-12	0.00000
.23550E-13	`o*,0000o;	[7906E-12]	_0.00005_	15146E_01		37874E-01_	0.00000	•19364E[2		71171E-14	<u>0.00000</u>
.27086E-13	0.00000	15636E-14_	_0.000005	15146E- <u>0</u> 1	_0000.00	37874E-01	្តី•០០០០ <u>០</u>	12050E-14	_0.02000_	423576-13	0.0000
.10437E-12	0.00000	.50575E-12	0.00000	162536-01	0.00000		ó. 0000 <u>0</u>	.288390-12	n• o.o. <u>o</u> .o.o.j	81468E-14	0.02000
•79140E-13	0.00000	43392L-12	0.00000	16229E-01		1123iF-01	0.00000	15792E-12	0.00000	44016E-14_	0.00000
.57966E-14			0.00000	1655AE_QT		115316-01	<u>. o • ŏo o o g</u>	93850E-13	000000	65487E-13	0.0000
-28031E-13	0.00000	55200E-12	0.00000	16229E-01	0.00000	.115314 <u>-</u> 01	Ţġ•ÓÓ <u>ŌŌ</u>	. Ž203 3E - 1 <u>Z</u>	0.00000	409926-13	0.00000
										314096-13	
										13946E_ <u>_13</u>	
										.64218E-13	
19507t-12	_0.00000	33018E-12	. ၁ <u>. ၀၀၀၀</u>	<u>11</u> 2025 + 00	_0.00000	-10554E+00	0.00000	11903E12	0.00000	392616-13	0.00000
19266E-12	0.00000	.323365-12	0.00000	• 11252E+00	0.00000	10>546+00	0.0000	39478E-12	0.00000	14979c-12	0.00000
.18528E-12	0.00000	.45297E-12	0.00000	"	0.00000	.42654L+00	0.00000	69730E-12	0.00000	216406-12	0.00000
•17217E-12	0.00000	454106-12	0.00000	19810E+00	0.00000	42654t +00	í o •nooòó	26124E-1	_0.000,00	1908 /E-12	o•ñoua <u>9</u>

NATURAL FREQUENCY= .119250E+04

YX Real	TX -	. KEAL	TY Imag	TZ REAL	17 1446	RX REAL	RX IHAG	RY REAL	RY THAG	REAL TO	THAG
22404E-13	0.00000	.15413E-12	0.00000	.19992E+00	0.00000	42 d 1 O C + O O	0.00000	17240E-12_	0.00000	.150d3c-12	0.00000
29675E-13	0.00000	13058£-12	0.00000	-,19992E+00	0.00000	.42dL0E+00	0.00000	.809518-13	0.00000	28578E-13	<u></u>
-462416-13	0.00000	747086-13	0.00000	~.11209E+09	0.00000	10570c+00	0.00000	.23664E-12	0.00000		0.00000
16319E-13	0.00000	.91008E-13	0.00000	.11209E+00	0.00000	.10570E+00	0.00000	20975E-12	0.00000	10075E-13	0.00000
+671d1E-14	0.00000	19637 <u>L</u> -12	0.04000	862436-01	0.00000	.34097t-01	0.00000	•12043E-12	0.00000	69274E-13	0.00002
21253E-13	0.00000	.19071E-12	0.00000	.d6243E-01	0.00060	34097E-01	0.00000	15715E-12	0.00000].37911E-13	<u>_0</u> 0000_
17459E-13	0.00000	432901-13	_0.00000	<u>18034E-01</u>	0.00006	.32349E-01	0.00000	<u>.</u> 20454E-12.	0.00000		0.00000
27950E-13	0.00000	.5326ÎE_13		180346-01	0.00000	32349E-01	0.00000.	.27802E-12		18461E-13	<u>0.0000</u>
 55425E-13	3.00000	.14767E-12	0.00000	203258-02	0.00000	.59023E-02	0.00000	97203E-13	0.00000	.107995-13	0.00000
49123E-13	8.00000_	1516aE-12	0.00000	20325E-04_	0.00000	59623E-02	_0.00000	.15177E-12	0.00000	14096E_13_	0.00000
33072E-13	000000	158238-12	` 0. 00000		0.00000	.59o23E=02	0.00000	• 22537E-12	.0.00000	62476c- <u>13</u>	0.00000
19670E-13	0.00000	16513E-12	0.00000		~0.00000	59623E-02	0.00000	27492E-12	0.00000		_ัง รูก่องจรั
-10767E-12	0.90909	447116-13	0.00000	180346-01	0.00000	.323496-01	0.00000	27834E-13	0.00000	1d147E-13	0.00003
10410E-12	0.00000	.274951-13	_0.00000	=,18034E-01	0.00000	323496-01	0.00000	181005-15	.0.00000_	.13669E-12_	0.00000
133258-12	0.00000	192131-12	0.00000	.86243E-01	0.00000	.34097E-01	0.00000	44649t-12	0.00000	81231E-Ī3	0.00000
95133E-13	0.00000	-19481E-12	. 0.00003_	86243E-01	0.00000	34097E-01	ġ.0000v	89635L-13	0.00000	154 <u>1</u> 7e-12	0.00003
424288-12	0.00000	11856E-12	0.000000		0.00000	10570t+90_	0.00000	4121 <u>B</u> E-12	0.00000	14553E-12"	0.00000
379498-12	0.00000	-10665L-12	0.00000	11209E+00	0.00000	.10570E+90	0.00000	13197E-12	0.00000	-17117E-12	0100000
+37995E-12	9.00000	•13d13L-12	0.00000	199928+00	0.00000	426106+00	0.00000	79997E-12	0.00000	49363£-12	0.00000_
=.38517E-12	0.00000	14275g-12	0.00000	00+356661	0.00000	.42810L+00	0.00000	11064E-11_	0.00000	-44340E-12	0.00000
**		•	-	•				-	**	. ,	

NATURAL FEEQULACY= .119940E+04

- TX PEAL	TX IMAG:	TY KEAL	TY IMAG	TZ Real	TZ '	K X K t a L	RK Imag	RY Real	YF DAM1	RZ RZ RZ RZ REAL IMAG
-12403E+0J	0.00000	749556-13	0.00000	500581-13	0.00000	.23218E-12	0.00000	18605E+00	U-00000	.22490E-10 0.00000
-•12403E+00	0.00000	.90>776-13	0.00000	-13098E-12	0.00000	3d625b-13	0.00000	18605[+00	0.00500_	21,936-10 0.00000
.12403E+00	0.00000	+40067F-13	å•09001	.44859E-13	0.00000	-381206-13	0.00000	18605£+00	0.00000	.69975E-11 0.00000
·•12403E • 00	0.00000	.55090E-13	0.00000	644476-13	0.00000	76197E-13	0.00000	18605E+00	0.00000	70400E-11 0.00005
.12403E+00	0.00000	.709376-13	0.00000	345216-13	0.00000	64393E-13	0.00000	18605E+00	0.00000	.75983z-11 0.00000
-12403E+00	0.00000	55557E-13	0.00000	,139710-12	_0.99000	19197E-13	0.00000	18605E+00	0.00000	74005E-11 0.00005
.I12403E+00	_0•000n0 <u>_</u>	61307E-14_	0.03000	72598E-13_	. ģ.aauoo	41134L-13	0.00000	18605E+ <u>6</u> 0	_o•oō'n <u>oo_</u>	
-124036+00	0.00000	69967E-13	0.00000	_=-139338-13	_ō.ooooo	. •48798E-L3	0.00000	18605E+00_	0.00000_	376966-11 0.00000
-12403E+00	o. aaceu	839756-13	0.00000			.247805-14	0.00000	18605E+00	n <u> 0</u> 00000	-383646-11 0.0000
-12403E+U0	0.00000	890476-14	0.00000	628165-13	0.00000	.53285E-L3	0.00000	18605E+00	c.00u00_	386536-11 0.00000
-12403E+00	000000	~42289E-13	0.00000	675628-13	0.00000 `	.45094E-13	0.00000	18605E+0G		
-1240 JE+00	0.00000	21749E-1 <u>3</u>	0.00000	32621E-[3	_0.00000	· .31687E-14	0.00000	18605E+00	0.00000	140386-11 0-00000
.12403E+00	_0.00000	•46243[-13	ó.G0000	.108458-13		68649E-14	0.00000	18605E+00	~0.00000 <u>~</u>	316726-11-0.00000
₹12403E+00	0.00000	103276-13	0.00000	.20721E-13	0.00000	13938E-13	0.00000	18605E+00	_0.00.00_	322756-11 0.00000
_12403E+00	0.00000	- •96879E-13	0.00000	152846-13	_0.00000	59050E-F4	0.30000	18605E+00	.0.00000	.61457E-11 0.00000
-12403E+00	_ 0.00000	11035E-13	_0.00000	60485E-14]	_0.00000_	222678-13	0.00000	18605£+00°	. 0.00000.	610698-11 0.00000
-12403E+00	0.00000	.409796-13	0.00000	.14530E-13	0.00000	100646-13_	0.00000	18605E+00_	_0.00000 ⁻	.57077E-11 0.00000
*12403E+00"	0.00000	271306-13	0.00000	56542E-13	0.00000	405598-13	0.00000	18605E+00	u.00000,	56/01E-11 0.00000
•12403C+0J	0.00000	103492-12	0.00000	. 417925-14	0.00000	-10312E-12	0.00000	18605E+00	0.00000	.18756E-10 _0.00000]
-12403E+00	0.00000	29723E-13	0.00000	47307E-13	~ ő.ooooo ·	55930£-14	0.00000	18605E+00	0.00000]	10342E-100.00000

NATURAL FREQUENCY= .1200398+04

TX REAL	XT DAKI	. TY	TY Imag	TZ REAL	T2 IMAG	RX REAL	RK I Mag	RY	RY RZ RZ IMAG REAL IMAG
+16477E+00	ō•00000	77739E-13	0.00000	23514E-12	0.00000	20152E-12	0.00000	35484E+00	0.00000 .16581E+00 0.00000
16477E+00	0.00000	•62379E-13	0.00000	18096E-12	0.00000	-27516E-12	0.00000	35484E+00	0.000001658100000
•16160E+00	0.00000	.30317L-13	0.00000	10022L-12	0.00000	13119E-12	0.00000	139546+60	0.00000 7 .51349=-01 0.000000
161aJE+0U	0.00000	-297408-14	0.00000	72891E-13	0.00000	-11946E-12	0.00000	139546+00	0.0000051349E-01 0.00000
+62420E-J1	0.00000	.677591-13	0.00000	36482E-13	0.00000	202986-13	0.00000	12598E+00	0.00000 .547426-01 0.00000
62426E-01	0.00000	912626-13	0.00000	.11768É-12	0.00000.	367496-13	0.00000	12593E+00	0.00000547421-01-0.0000
•5113o6- <u>0</u> 1	0.00000	.66973E-13	0.00000	-41674E-14	0.00000	251631-14	0.00000	-+47597E-01	0.00000 2763001 0.00000
51136E-01	0.00000	52903L-13	0.00000	.39294E-1J	0.00000	71852E-13	0.00000	47597E-01	0.00000276308-01 9.00000
.70495E-02	0.00000	19367L-13	0.00000	64342E-14	0.00000	41423E-13	0.00000	26231E-01	0.00000
704958-02	0.00000	•36951E-13	0.00000	.13564E-13	0.00000	[332916-15	0100000	262316-01	0.0000028898E-01 0.00000
704958-02	0.00000	733586-13	0.00000	.262216-13	0.000,00	.40251E-13	0.00000	.26231E-01	0.00000584985-01. 0.00000
.70495E-02	0.00000	.44174E-13	0.00000_	231126-i3	0.00000	.39716E-13	0.00000	26231E-01	0.00000 288 98E-01 0.00000
51136E-01	0,00000	44265E-13	_0.00000	416156-13.	0.0000ñ	22472E-14	_0.00000_		0,00000 [276306-01 [0,0000]
.51136E-01	0.00000	557916-14	0.00000	25866E-13	0.00000	.26012L-13	_ 0.00 <u>,000</u>	47597E-01	0.0006027630E-01 0.00000°
624201-01	0.00000	.634161-13	0.00000,	239926-14]	0.00000	87416E-14	0.00000	1259dE+00	0.00000 1 .5474ZE-01 0.00000
-62426E-01	0.00000	-,34705E-13	`0.00000"	25870E-13	0.00000	13355E-13	0.00000	.12598E+UQ	0.000005474201 0.00000
16160E+00	0.00000	.81457£-13	0.00000,	-28900E-13	0.00000	485856-13	0.00000	+13954E+00	0:00000 .51349e-01 0.00000
161u0E+03	0.00000	23024E-13	0.00000	794896-14_	`o` 10000 _	34862E-14	0.00000	-13954E+00	0.00000 -1513498-01-0100000
- <u>.</u> 16477E+00	0.00000	86J77t-14	0.00000	~• £34326-13	0.00000	21528E-13	0.00000	- 135484E+00	0.00000165816.00 _0.00000.
-16477k+00	0.00000	27660L-14	0.00000	.47058E-13	0.00000	.6+655E-13	0.00000	.35484E+00	0.00000 165812+00 9.00000

ORIGINAL PAGE IS OF POOR QUALITY

. YX . REAL	TX Imag:	TY Real	YT IHAu	TZ REAL	TZ I HAG	K X Real	147.0 K4	RY	< T 1 M A G	. KZ KEAL	, RZ
-10041L+00	0.00000	150376-13		666136-13		•34745E-12				25571E±00	
10041E+03	0.00000		_								
	, ,	.28510t-13	•	•11415E-12	0.00000	26303E-12	0.00000	32064E+00	0.00000	26571 <u>L+</u> 00	0.00000
.96932E-01	0.00000	-602298-13	0.00000	-13844E-12	0.00000	+17502E-13	0.00000	.20283E-01	0.00000	.70028E-01	0.00000
-•96932E-01	0.00000	.21895E-11	0.00000	12522E-12	_ 0.00000	713162-13	0.00000	•20283E-01	0.00000	- <u>-</u> 76023E-01	
50512E-01	0.0000	•30266E-13				83163E-13				.70602E-01	
•50512E-01				10507E_12							
				31Z86E-13							
.57299E-01.	0.00000	356926-13	0.00000	30156E-13	0.00000	.158128-13	0.00000		0.00000	1467 <u>5E</u> -0 <u>1</u>	0.00000
.89535E-U1	_0.00000	_,37803E_13_	0.00000	19956E- <u>1</u> 3	_0.000000	_4704766 <u>-14</u>	0.00000	. <u>i</u> 3678E+00	_0.00000	•15941E-0 <u>1</u>	0.00000
				\$3056L-11							
89535E-01	0.00000	22561E-13	_0.0 <u>0</u> 00 <u>0</u> 0	B0990E_14	_0.00000	20741E-13		i3678E+00	_o*,öōōo <u>,</u> o_	15941, -01	0.00003
89535E-01	0.00000	-58713L-13	. ō • ō o o o ō	800778-14	_0.00000	335646-13		. [3678E+00	0.00000	. 15941E-01	0.00003
				186041-13							
-57279E-01	0.00000		0.00000	2.4913£-13_				12951E+00		.19675E-01	
50512E-01	0.00000	34972a-13	0.00000	14614E-13	0.00000	251,78E-13	0.00000	-34062E-01	0.00000	76602=-01	0.00000
-50512E-01	0.00000	488728-13	0.0000	167038-13	0.00000i_		0•0 <u>0</u> 0000	34062E-01	0.00000	.70002E-01	0.00000
				65311E-14							
96932E-01	_0.00000	23082Ê-13	0.00000	17095E-13	_ีที•000กย์	35328E,=13]	_ 0.00000.	-,20283E-01		.76028E-01	0.00001
.10041E+00	0.00000	21279E-13	0.0000	16312E-13_	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	-60942E-13	0.00000	32064E+00	_0;00000	26571E+00	0.000000_
•10041E+00 ₋	0.00000	.41476E-14	₫•₫₫₫ <u>₫₫</u>	19531E-13	0.00000	334946-14	0.00000	32064E+00	0.00000	•20571E+00	0.00000

NATURAL FREQUENCY= .120587E+04

TX REAL	TX Dari	TY REAL	TY IHAG	TZ REAL	TZ I mag	RX REAL	RX I MAG	RY Real	Y X Qahi	RZ RZ
19639E-13	0.00000	•18124E-13	0.00000	19534E-12	0.00000	.43957L-12	0.00000	.22361E+00	u.00000	13046 <u>E</u> -12 0.00005
•90635E-14	0.00000	5097dE-13	d00000	· 14645E-12.	0.00060	440248-12				_15016 <u>=_15_</u> _0°00000
.68378L-14	0.00000	924991-14	0.00000	.17934E-12	0.00000	•97762E-13	0.00000	22361E+00	0.00400	168822-13 0.00003
2195>E-13	0.00000	74669£-16	0.00000	16187E-12	0.00000	120072-12	0.00000	•22361£+00	0.00000	
.13285E-12	0.00000	47229E-13	0.00000	.165048-12	0.00000	•16212E-15	0.00000	22361E+00	ุ้ง•ังวงจี้จั	54341E-13 0.00000
828106-13	0.00000	•74760E-13	0.00000	12300E-12	0.00000	.79882E-13	0.00000	•22361E+00	. 0.00000	.42660F-f3 0.0000 <u>0</u>
		40603E-13_				T. 773426-13	_0.00000	*553ê1E+00	. 0 o o o o o o o	267126-13 0.00000
		.27110t-13		•			0.90000	223t1E+00	0.00000	107765-12 0.00000
		.17416E-13		81237E-13_	0.00000	72993E-13	0.00000	.22361E+00°	0.00000.	-60294E-13 0.0000
		614926-13		•59960E-13 "						90857L-140.00 <u>000</u>
										518806-13 0.0000
	0.00000						0.00000	. 55397£+00	0.00000	96393c-14_0,00000
.44400E-1J	0.00000			318508-13						57131E-13_0.00000
61446E-13										61703E-13 0.00000
	0.00000									.43944E-13 0.00005
38406E-L3	0.00000			1509ZE-1Z	~0.0000°	98981E-13	0.00000	~~22361É+00	″0.700000°	.75918E-13 0.00000
-15154E-12		12221E-13		.26080E-12			0.00006	. •55391E+00.	0.00000	48863E-13 0.000000
499808E-13		•29529E-15		30890E-12	_0.0000g	.164106-12	0.00000	22361E+00 T	0.00000	
	0.00000	-42d36L-13		30040E-12		83781E-12	0.00000	22361E+00	0.00000	27050L-12-0.00000
- <u>+</u> 12199E-12	0.00000	43913E-13	0.00000	• 29604E-ĪZ	0.00000	.82101L-12	0.00000	-22361E+00	0.00000	.232976-12 0.00000

	NATURAL FRE	วักรพกล้ <u> - ไร</u> 1505ก	4E+04	•					
TA IX	TY TY	TZ	TZ .	RX REAL	RX IMAĞ	ŘÝ RĚÁL	THAG	RZ REAL	HAG
279056-01 0.00000	11303E-12 0.00	000 - 10033E-15	0.00000	664185-13	0.00000	13135E+00	_0.00000_	.28273E+00	0.00000
.279056-01 0.00000	145832-12 0.00	.564 LGE-14	0.00000	-28375E-12	0.00000	13135E+00	. <u>0.00000</u> <u>.</u>	282736+00	0.00000
1372dE-01 0.000J0	.8d377L-13 0.00	000154736-12	0.00000	105136-13	0.00000	-22074E+ÕO	0.000000	.57962c-01	
.19928E-01 0.00000	388206-13 0.00	00015619E-13	0.00,000	476036-13	0.00000	.22074E+00		57962t <u>-</u> 0İ	
14G0dE+00 0.00000	.10746E-12_ 0.00	000 <u>.</u> .22958E-Li	_ 0.00000	32434E-13	0.00000	.17884E+00	_0.00000	307742-01	_0.00000
.1400dE+00 0.00000	18695E-12 0.00	000 .50V12E-13	0.00000	10746t-12	0.00000	.17884E+00	0.00000	-, 30774 <u>L</u> -01	0.00000
80834E-01 0.00000	.91780E-13 0.00	00002598E-13	o.oo.óo	.47261c-14	0'0000 0	18439E+00		47574E-01	0.00000
.80839E-01 ,0.00000	10223E-1,2_ 0.00	000l1054E-13	0.00000	85715E-13	0.00000	18439E+00	_0.00600_	-47574E-01	0.00000
46064E-01 0.00000	106928-12 0.00	000 - 59451E-13	~~ooooo	~40174E~13	0.00000	-50746E-01	0.00000	64511E-01	0.00000
_46064E-01 0.00000	·102828-12 0·00	000442046-14	_0.00000	•66975E-13	0.00000	.50740E-01	_0.00000	-6451 <u>1E-01</u>	0.00000
-46064E-01 0.00000	14986E-12 0.00	000 15718E-13	0.00000	.92331E-13	0.00000	50746E-01	_0_0000 <u>00</u> _	64511E-01	0.0000
-:46064E-01 0.00000	•15691 <u>L</u> _12, 9,00	000. 507,30E-13	0.00000	107171-12	o• ŏōooó	50746£-01	0.00000	64511E=01	ຼືດ <u>້ວ</u> າວວັງ
-80839E-01 0.0000ò	79565E-14 0.00	000 420416-13	000000	50787E-13	0,0000.0	18439E+00	0.00000	475748-01	0.00000
80839E-01 0-00000	49730E-130.00	000335688-13	0.00000	59330E-14	0.00000	18439E+00		-475746-01	0.00000
14008E+00 0.00000	~~.16694E-İŞO.00	000 [48412E-13	0.00000	61683E-13	000000	17884E+00	0.00000	30774=-01	. 0.00000
140G8E+00 0.00u00	173878-12 0.00	00u345/dE-13	0.00000	59699c-13	0.00000	17884E+00	_0.0000 <u>0</u>	30774 <u>E</u> =01	0.00000
.19928E-01 0.00000	10786E-12 0.00	000 - 38265E-13		790878-13	0.00000	22074E+00	0.00000	.57962e-01	0.00000
19928E-01 0.00000	86131E-13 0.00	000 .82738E-13	0.00000	38986E-13	0.00000	22074E-00	0.00000	57902:-01	0,00000
-279056-01, 0.00000	1003)L-12 0.00	003395/16-13	0.00000	.14036c-12	0.00000	•13135E+00	0.00000	.28273E.00) o•ñooño
27905E-01 0.00000	*11533E=12 0.00	0001836dE-13	0.00000	•13598E-12	0.00000	13135E+00	0.00000	2827,36±00	0.000000

NATURAL FREQUENCY=_ -122981E+04

TX Peal	TX lhag	46 <i>1</i> F 14	TY Imag	TZ KEAL	T Z I MAG	K X KŁ AL	Rx I MAG	RY . Real	Y X Dan 1	RZ.	RZ Inas
-78367E-01	0.00000	.23707E-13	0.00000	453432-13	0.90000	•77456E-13	0.00000	.20985E-01	0.00000	264076+00	0.00000
78367E-01	0.00000	421361-13	0.00000	. •42150E-13	0.00000	11476t-12	0.00000	20985E-01	0.00000	. 26407=+00	0.00000
-46422E-01	0.00000	.207521-13	0.00000	11651E-13	0.00000	-11d0aL-13	0.00000	2575dE+00	0.00000	.48215E-02	, 0.00900
404226-01	0.00000	14379E-13	0.00000	•11734E-13	0.00000	24666t-13	0.00000	25753£+00	0.00000	4d215e-02	0.00000
.67552E-01	0.G0u00	165466-13	0.00000	.46781E-13	.0.60000	.14087E-13	0.00000	82454E-01	0.00000	5.4355£-01	0.00000
67552E-01	0.00000	.302330-13	0.00000	•28540E-LJ	0.00000		0.60000	82454E-01	0,000,00	54J55E-QI	0.00000
59991E-01	0.00000	22020E-13	0.00000	~.23773E-13	0.00000	74773E-14	0.00000	.76324E-01	្ចំ , ១០០០០០	10440=+00	0.000,00
59991E-01	0.00000	.56306E-13	0.00000	32321E-1 <u>3</u>	_0.00060	.22425E-13	0.00000	7632 4E - 01	0.00000	10440E+00	0.00000
12635E+00	0.00000	· 214485-13	0.00000	-,-19,137E-13	0.0000	32245E-13	0.000005		0.00000	3 <u>5</u> 903 <u>e</u> -01	5.00000
+120356+30	0.00000	331858-13	0.00000	. 34323E-14	0.00000	46389E-14	0.0000	-24272E+00	U.000[00]	35 <u>9</u> 03E-01	<u></u>
-12635F+00] a• da9aa [-,14198E-13	0.00000	.187306-13	<u></u>	10334E-13	0.00000	_ <u>.</u> 2427 <u>2</u> E+00_	0.00000	<u>3</u> 59036-01	0.00000
-126356+00	.0.00000	574646-13	0.00000	132275-13	0.00000	743846-14	0.00000	242726+,00	ō•6030 <u>0</u>	35,903,6-01	0.00000
59991E-01	0.000.00	. •17849E-13	0.00000	.583286-15	.0.00000	~+95454E-14]	0.60000.	76324E-01^			0.00000
•29991E~0T	0.00000		0.00000	-,75756E-14	0.00000	.89861C-14	0.00000_	.76324E-01	0.00000	.10440E+00	0.0000
-67552E-01	0.00000	46227E-13	0.00000	13800E-13	0.00000	-46163L-13	0.00000	82454E-01	. o• oòoōo.	54355E-01	0.00000
675526-01	0.00000	.566066-13	0.00000	• 1880 1E-13	_0.00000			82454E-01	0.00000	•54355E-01	0.00000
40422E-01	0.0000	51645,6-13	_o.uoōoj	114566-13	0.00000	-26919E-13	o 00 0 0 0 0	25758E+00	0.00000	48215e-02	0.00000
-+40422E-01	0.00000	.74135Ē-15	`0.00000]	37699E-13	0.00000	•4+775E-13	0.00000	25758E+00	0.000,00	48215E-02	0.00000
-,78367E-01	0.00000	•50642E-13	0.00000	21866E-14	0.00000	31241E-13	0.00000	.20985E-01	0.00000	-26407E+00	0.00000
78367E-01	0,00000	24108E-13	_0.000 <u>0</u> 0	141406-13	0.00000	45319E-13	0.00000	-209856-01	v. 000°06′	26407E+00	0.00000

NATURAL	FREQUENCY=	.126367E+04

		NATURA	L FREQUEN	CY= .126367	E+04						
TX Real	TX IHAG	IY KEAL	TY Imag	T/ Real	TZ [HAG	RX XEAL	RX IHAG -	RY - REAL	RY THAG	KEAL .	RZ LHAG
·98034E-01	0.00000	.47894L-13	0.00000	+23868E-13	0.00000	*33436E-13	0.00000	52228E-01	0.00000	~23950±÷Õ(0.00000
98084E-01	0.00000	626414-13	0.00000	350848-13	0.00000	25680E-13	0.00000	52226E-01	6.00000_	. 23950E÷0€) _ 0_0000 <u>0</u>
•17440E-01	3.00000	.31371E-13	0.00000	.4791UE-13	0.00000	36884E-13	0.00000	21106E+00	0.00000	.76377E-01	0.00000
174408-01	0.00000	-63753E-13	0.00000	.13380E-13	0.00000	63331t-14	0.00000	21106E+00	0.00000	76377E-01	
-#30720E-01	0.30600	11783L-12	0.00000	102226-13	0.00000	./33156-13	0.00000	-109346+00	0.00000	.882190-01	L0.000005
.30720E-01	0.00000	.62508E-13	0.00000	45662E-13	0.00000	.44971L-13	0.00000	.10934E+00	0.000,00	88219E-01	<u>0</u> .00000 <u>2</u>
:-12901E-00	0.00000	106216-12	0.00000	24568E-13	0.00000	15049E-13	0.00000	+24563E+00	0.00000	loss6E0	r0:000 <u>00</u>
*12901E+00	0.00000	64074E-13	0.00000	.5360dE-15	`0.00000	.1/825L-13	0.00000	.24563E+00	0.00000	lo886E-0.	r0.00000
59123E-01	0.00000	. •58980£-13.	0.00000	79893E-14	0.00000	lo449t-13	0.000,00	14582E+00	_ a.oon@@_	1132[E+00	0.00000
.59123E-01	0.00000	33661E-13	0.00000	15738E-13	0.00000	35368E-13	0.00000	.14582E+00	0.00000	-11321E-0	0.00000
-59123E-01	0.00000	702902-13	0.00000	-238668-13	0.00000	34665E-13	0.00000	14582E+00	0.00000	11321E+00	0.0000
-59123E-01	,0.00000	. •52963E-13	0.00000	13808E-13	00000.0	110966-13	0.00000	~.1458ZE+00	_0.00760_	ii321E+00	2.00039
+12901E+00	0.00000	225168-13	0.00000	19169E-13,	0,00000	.34284L-13	0.00000	-+2456JE+00	0.00u00_	16836E0	<u>. 0.</u> 0000 <u>0</u>
-12901E+00	0.00000	-39408E-13	0.00,000	61469E-14	0.00000	~~.28416E-13	0.00000	24563E+00		16886E-01	0.00000
-30720E-01	0.00000	113938-12	0.00000	• 33034E-13	_0.00000	104031-13	0.00000	10934E+00	_ თ.თასტი	.88219c-01	L_0_00000
307206-01	0.00000	248996-13	0.00000	.20830E-13	_0.00000	72542E-14	0.00000	10934£+00	0.00000	802196-0	0.00000
174436-01	0.00000	848398-13	0.00000	43312E-13	0.00000	•52268E-13	0.00000	.21106E+00	0.00000	76377E01	เ จ•ุจจจจฐ์
_17440E-01	0.00000	409518-15	0,00000	29750E-13	0.0000	.637110-13	ò.000ŏo	21100E+00	_0.00000		i0.000 <u>00</u>
98084E-01	0.00000	-10185E-12	0.00000	•16074E-13	រី.០០០០០	85892E-13	0.00000	-5222dE-01	0.00000	23950E+00	00000,0
.98084E-01	0.00000	.319346-13	0.00000	78134E-15	0.00000	89004E-13	0.00000	•5222âE =01	0.00000	.23950E+00	0.00000

TX	TX	KEAL .	TY	. TZ	TZ IMAG	KX LEAL	RX 1 -	RY REAL -	IMAG	REAL	RZ IHAG
-32213E-13	0.00000	28233c-13	. 0.000n T	598398-12	0.00000	31125e-12	0.00000	-18587E+00	0.00000	85725E-13	0.00000
						.37191E-12					
						.33064E-12					
.73325c-14	0.00000	942735-15	0.00000	.704758-12	0.00000	30278E-12	0.00000	.30075E+00	0.00000	.29451E- <u>137</u>	0.00000
.45851E-13	0.00000	.51840E-13	0.00000	-165948-12	0.00060	.92174E-12	0.00000	20245E-12	0.00500	117516-13	0.00000
.41600E-13	0.00000	48040L-13	0.00000	15823E-12	0.00000	93665E-12	0.00000_	39650E-13_	0.00,000	.56229E-13	0.00000
-60386E-13	0.00000	.20080E-13	0.00000	.130186-11	0.00000	.48566E-12	0.00000	.30075E+00	0.00000	42354E-13	0.00000
-46197E-13	อ. อออัจโอ	64574E-13	0.00000 "	12302E-11	0.00000	57047±-12	0.00000	300758+00	0-00000	, 300 = 1Ê-13	_0.0003 <u>0</u> _
72795E-14	_0.000 oo_	54069E-13	0.00000	13463E-11[-:35212E-12	0.00000	18587E+00	ັບລັດດູດ້ວິດ	.10035E-12	0.00000
- <u>.</u> 33838E-14	0.00000	.445736-13	0.00004	130576-11	0.00000	.449411-12	0.00000	.185876+00	0.00000	650924-15	0.30000
13451E-13	u.00000	57368L-13	0.00005	35608E-12	0,00000	801131-12	0.00000	18587E+00	0.00000	*406ARF-14_	0.00000
	9•00n00°	62547 <u>C</u> -13	0.000055_	386A <u>1</u> £_15	`ó:000è	. 87891E-12	_o´-ōoooo_	18587E+00		14266E-14	0.00000
-105565-13	0.00000	93452c-14	0.00000	56681E-12	0.00000	4do34L-12	0.0000	0075£+00 و.	0.00000	26347c-13	0.00000
.31555E-13	•	76466E-14				.46247E-12					
-30535E-13	0.00000	.36718E-13	0.00000	68365E-12_	_0.00000	17073E_12	0.00000	-11289E-12	0.00000	51591E-13	0-00000
:,24123E-13	0.00000	52034E-13	0.00000	.64481E-12	0.00000	17434E-12	``o.ōoōoo`	13883É-12	0.00000	27306E13	<u>0.0000</u>
	0.00000	.66819E-13	0.00000	128726-12	0.00000	.17695E-12	0.00000	30075E+00	0,00000	53496E-14	0.00000
12385E-13	0.00000	40604E-13	0.00000	.22776E-12	0.00000	271556-12	0,00000	.300758+00	0.00000	16715[-13]	_ 0 <u>_</u> 00 000 j
36143E-14	0.00030	32369E-13	0.00003	230521-12	0.00000	2/134L-12	0.00000	1858/6+00	0.00000	.79430 <u>E</u> -13	0.00000
3067/E-13	J. 00020	.362136-13	0.00000	.1921ot-12	0.00000	.441156-12	0.00000	18587£+06	0.00000	7>7716-13_	0.0000

NATURAL FREQUENCY= .128934E+04

TX Real	TX 1HAG	TY REAL	TY IHAG	T2 Real	T Z I MAG	KX Real	R A I HA G	R y Real	AAC	RZ	RZ IHAG
171736-14	0.00000	.10742E-13	0.00000	.10126E+00	0.00000	.88224L-01	0.00000	.75350E-12	0.00000	2222dE-13	0.00000
57066E-14	0.00000	563128-13	0.00000	10126E+00	0.00000	852241-01	0.00000	7114dE-12	0.00000	.16067L-13	0.00000
855336-14	0.00000	.94205L-14	0.00000	.117486+00	0.00000	947581-01	0.00000	117098-11	0.00000	.33702E-13	0.00000_
39333E~14	0.00000	.77716E-13	0.00000	1174sE+00	0.00000	.947586-01	0.00000	.11839E-11	0.00000	.198936-13	_0.00000_
393678-14	0.00000	.1493dE-13	0.00000	11557C+00	0.00000	193261+00	0.00000	22424E-13	0.00000	.14066E=13	
100940-13	0.00000	.68992c-13	0.00000	115578+00	0.00000	.19326L+00	0.00000	.40611E-13	0.00000	.43 jao=-13	0.00000
12497E-13	9.00000	24745E-13	0.00000	30329E+00	0.00000	227341-01	0.0000	.11118E-11	_0.00000)	.25371E-14	_0.000 <u>03</u> _
197076-13	0.00000	611375-13	0.00000	********************	0.00000	.22734t-01	0.00000	11426E-11	0.00000	10872E-13	_000000
27487E-13	0.00000	· .16713E-13	0.00000	16539E+00	000000	21549E+06	0.00000	63492E-12		24935E-13	0.00000
28420E-13	0.00000	66087E-13	0.00000	.16539E+00	0.00000	215496+00	0.00000	.59693E-12	0.00006	 85806E=14	0.00000
157796-13	0.00000	.127116-14	0.00000	16539E+00	0.00000	.21549£+00	0.00000	71512E-12	0.0000		0.00000
36564E-14	0.00000	.42162E-13	0.00000	16539E+00	0,00000	215495+00	_ 0.00000	•68787E-12	<u>.</u> 00000	2911d <u>c=</u> 13	0.00000
51803E-14	0.00000	250275-13		30329E+00	0.00000	22734L-01	0.00000	10115E-11	~0.0000°	, 97302E-14	
Î7143E-13	0.00000	.666558-13									
2400oE-13						L7326E+00					
22866E-13	0.00000	46382E-13	0.00000	11557E+00	000000	. 19326E+00	0.00000	51745E-13	_ 0.00000	38004E-1	0.0000
84324E-14				117406+00				99461E-12			
28164E-13	0.00000	75632E- <u>1</u> 3_	_ 0.0000g	11748E+00		94758E-01	0.00,000	-90880E-12	_0.000 <u>0</u>	43262e-14	0.00000
		95016E-14						_			
18766E-13				.10126E+00			0.00000	59943E-12	_0.00000	.145176-13	ສີ ວັ• ໐ັດ ດວກ <u>ີ</u>

NATURAL FREQUENCY+ .129083E+04

TX REAL	TX IHĀG	TY REAL	ŢY THAG	REAL	. T7	Ř.X , REAL	RK IMAG	REAL	THAĞ	REAL T	RZ IMAG
-40962E-13	0.00000	25507E-13_	0.00000	+17858L+00	0.0000	549021-02	0.00000	46085E-12	0,00000	92061E-14	0.00000
.84964E-14	.	258196-13		17858E+00	_0.00000°	.54902E-02	0.00000	39488E-12	0.00000	13193E-13	0.00000
.22853[-13	0.00000	.25952t-13	0.00000	178031+00	0.00000	41619b-01	0.00000	70979E-12	_0.00100 _	.10590c-13	
.7150dE-14	0.00000	.209166-13	0.60000	17803E+00	0.00000	.416196-01	0.00000	.78068E-12	`` 0. 00000	.407266-14	0.00000
•18856E-13	0.00000	.96740£-14	0.00000	.893696-01	0.00000	14003E+00	0.00000	23470E-13	_0.00000	.10487E-13	0.00000
.79105E-14	0.00000	-13066E-13	0.00000	±•89369E-Q1	0.00000	.14003E+00	0.00000	21022E-13	0.00000	.33831E-13	o.ooooo
-124098-13	0.0000	223186-13	0.00000	12436£+00)	0.00000	18939E+00	0.00000	.83735E-12	0.00000	322748-13	0.00000
.911418-14	0.00000	405206-13	0.00000	.12436E+00	0.00000	·13}79E+00	0.00000	84643E-14		56567E-13	0.00000
.30928F~1J	0.00000	381918-15	0.00000	32162E+00	0.00000	91139E-01	0.00000	5748oE-12	_0.055000 _	14430E-13	0.00000
.57579E-14	0.00000	53064E-13	0.03000	.321u2E+00	0.00000	.911396-01	0.00000	.6256dE-12	0.00000	22761E-13	0.00000
-145d7L-13	0.00000	84456t-14	0.00000	32162E+00	0.00000	.911398-01	0.00000	5193dL-12	. oʻ-öôəno <u>.</u>	24d53b-13	0.0000
-1,43306-13	0.00000					91139L-01					
-327448-13	0.00000	29251E-14	, ô.oogooō	12436E+00	_0.000no[0.00000	897,44E-12	_0.00000	50222E-13	0.00000
-104792-13	0.00000	.53874E-13	0.60000	.12436£+60	0.00000	199998+00	0.00000	963618-12	0.00000	12d14E-13	0.00000
-18091E-13	0.00000	13532E-14		,	•	.14003L+00					
-22044E-13	0.00050	40285E-13	0.00000	8 <u>9</u> 369£-01_	o.ooo.oo	=_14003E+00,	0 - 000000	34240E-13	0.00000	121184-13	0.00000
•20473E-13	0.00000	10279E-13	0.00000	.17803E+00	0.00000	.41619L-01	0.00000	96347E-12	0.00000	.155526-13	0.00000
.23150E-13	0.00000	601172-13	0.00000	17803E+00	0.00000	41619L-01	0.00000	.94514E-12	0.00000	67349=-13	∵ ǧ•₫oooō
.94619E-14	0.00000	.41716b-14	0.00000	17858E+00	0.00000	.54902E-02	0.00000	.62045E-12	_0.00000	27975b-13	0.00000
.164435-13	J.00000	.319338-13	° 0.0000	178536+00	0.00000	-154902E-02	0.00000	59606E-12	0.00000	.52069E-13	_0_00000

NATUPAL FREQUENCY= .130794E+04

тх	1X 14	TY	TZ	72	кX	n.		2 v		
REAL	IMAG REAL	LHAG		LHAG	REAL	THAG ""	REAL "	IMAG -	REAL .	I HAG
	0.0000041099E-13	0.00000	.107966-11	0.00000	.16441E-12	0.00000	10272E+00	0.00000	-20403E+00	0.00000
10049E+00	_0.00000701116-14	0.400000	i10521E-1i(0.00000	50503E-13		.102726.00	,0*000ō0]	20403 <u>E+00</u>	0.00000
-21424E-01	0.00000 .934726-13	0.00000	[+10633E-11]" (0.00000	202651-12	à.0000u `	10160E+00	0.00000	134048+00	<u> 6.60003</u>
214246-01	. 0.0000016412E-13	0.00000	1151dE-i1 (0.00000	.11996[-12	0.00000.	.10160E+00	0.00000	-13484E+00	0.0000
	0.00000313416-13	0.00000	-83841E-12 (0,00000	23274E-12	0.00000	25809E+00	0.00000	30901E-01	
	0.00000312451-13	0.00000	751496-12 <u> </u>	0.0000	.28908E-12	0.00000	25809E+00	0.00000_	3090iE01	0.00000
-64715E-01	0.0000010150E-12	0.00000	•52299E-12	0.00000	14694t-12	0.00000	13577E+00	<u>[</u> 000000]		0.00000
04715E-01	0.000003,7726-14	0.00000	50403E-12 (0.00000_	19408E-12	0.00000	13577E+00_	ŭ•009 <u>00</u>	=.11904E+00	0.00000
76170E-01	0.0000028892t-13	0.00000	.37306E-12	0.0000	21170C-12	0.00000	.1d954E+00	0.00000	f003eE+00_	0.00000
.76170E-01	0.00000 .27043E-13	0.00003	425526-12 3	0.00000	.140216-12	0.00000	.18954L+UQ	0;000000	10036E+00	0.00003
76170E-01	0.0000059126L-13	0.00000	-10118E-12 0	0.0000	44204L-12°	0.00000	*** • 1.895 4E • 00	0.00000	i0036E+00	0.00000
	0.00000 .53261E-13	0.00000	à0,135E-19 _	j. 00000	.41358E-12	0.00000	.18954E+00	_0.00000	100365 00	0.00000
64715E-01	0.00000 .16461E-13	0.00000	43739E-12 (0,00000	42260L-12	0.00000	13577E+80	0.00000	~_11904E+00_	<u> </u>
647156-61	0.00000 .77993E-14	0.00000	.450246-12	00000	.42046E-12	0.00000	13577E+00	0.00000	_ +11904Ē+00	0.00000
.90522E-01	0.0000021:336-13	0.00000	82224E-12	0.00000	17461E-12	0.00000	25809£+00	0.00000	-30901E-01	0.00000
	0.00000 -1169816-13	0.00000	.78733E-12 -	000000	.19696E-12	ó.000av	25809E+00	.0.00000_	3040 <u>1E-0</u> 1	0.0000
_ +21424E-01	0.00000161336-13	0.00000	867716-12	00000	-,• 4×0206-13	0.00000	-101602+00	0.00000	13484L+QQ_	0.0000
21424E-01	0.00000282986-13	0.00000	.081376-12, (0.00000	.16708E-13	0.00000	.10160E+00	0.00000	134846+00	0.00000
10049E+UU	0.00000 .100502-13	0.00000	8715oE-12 (0.00000	32066t-13	0.00000	•10272E+00	0.00000	204036.00	0.00000
aloo49E+00	0.0000027784E-13	0.00000	.87732E-12 0	00000	, -90787E-13	.0.00000	10272E+00	0.000000	- 204036+00	0.00000

NATUŘ	AL FREQUENCY=, *130990	DE L U4					
TX TX TY TY THAG TEAL	TY KEAL	TZ _IHAG	KEAL K	KK	RY	RY INAG	RZ RZ REAL IMAG
24276E-13 0.00000 -,29207E-12	0.0000028686E+00	0.00000	50365E-02	0.00000	.58108E-13	0.000.00	.10320E-12 0.00000
.31503E-13 0.0000020224c-12	0.0000028686£+00	0.00000	.55865E-02	0.00000	72124E-14	0.0000	996936-13 0.00000
-81041E-14 J.00000 .78053L-12	0.03096 287416.00	0.00000	.304986-01	0.00000	10255E-13	0.00000	4/392E-13 0.03000
-20906E-13 0.00000 .254716-12	"0,00000 ".28741E+00	0.00000	304981-01	0.00000	.572bdE-13	0.00000	
-352476-13 0.00000 .281216-12	0.00000224746+00	0.00000	.82947±-01	0.00000	21070E-12	0.00000	.911396-140.00000
41013E-13 0.00000 .28958E-12	0.UU00022474E+00	u.00000	829476-01	0.00000			~62678Ë-14~ 0.00000
-70396E-14 0.0000030340L-12	0.00000117/16+00	0.00000	.94718E-01	0.00000		•	
23861E-13 0.0000022255E-12	0.00000 .117716+00	0.00000	947186-01				32448E-13_0.00000
14298E-13 0.0000030630E-12	0.0000031074E-01						.51755E-13 0.00000
.6581JE-13 0.0000025899E-12	0.0000031074E-01	0.00000					
-36973E-13 0.00000 .30110E-12							
.326166-13 0.00000233256-12						=	
	0.00000117716+00						
-12944E-13 0-00000 -24218E-12							
-26996E-13 0.0000026512E-12							1>9876-14 0.00000
-44103E-13 0.0000023982E-12	0.00000 =.224748+00	0.00000					
-73253E-14_0.0000029767E-12							
.80640E-14 0.0000025365E-12							
.315595-13 0.00000 .277931-12			508651-02				88191E-13 0.00000
.34096E-13 0.00000 .26082t-12	0.0000028606E+00	0.00000					192661-13 0.00000
·				•	_ • •		

		HATUKA	L FKEQUEN	CY= -131635	E+U4					
TX REAL	TK IMAG:	TY .	TY IMAG	TZ R£AL	TZ IHAG	K X Keal	RK Imag	RY REAL	RY . THAG	RZ RZ REAL IMAG
-37009₺-13	0.00000	746871-01	0.00000	.407341-01	0.00009	.27751E+00	0.00000	45836E-13	0.00000	.16576L-13 0.00000
-19406E-13	0.00300	.746876-01	0.00000	-40734E-01	0.00000	.27751E+00	0.00000	34610E-13	_0.00000 -	290765-14 _0.03000
25789E-13	0.00000	.208012+00	0.00000	10803E+00	0.00000	-:18175E+00	0.00000	37837E-13	U+00000	.195014-12 n.00000
319035-13	0.00000	20401E+00	0.00000	10853E+00	0.00000	16175E+00	0.00000	.3963dE-13	0.00000	.16611E-12 0.00000
659258-13	J.00000	.940761-01	0.00000	.90673E-01	0.00000	20059E-01	0.00000	.97121E-13	0.00000	1,07282-12 0,00000
.4397JE-L5	0.00000	940761-01	0.00000	.90673L-01	0.00000	28859E-01	0.00000	14894E-13	0.00000	16387E-12 0-00000
45921E~13	0.00000	103986+00	0.00000	.222808-01	0.00000	.96445E-01	0.00000	.52138E-13	0.00000	-31500E-15 0.00000
<u>:</u> •39279€−13	0.00000	- 16398L+00	0.00000	-222808-01	0.00000	.964452-01	0.00000	-1970JE-13	0.00300	.3561dL-12 0.00000
55554E-14	0.00000	14032L+00	0.00000	44858E-01	0.00000	.10658E+00	0.00000	122586-12	0.00000	.291292-12-0.00000
-18702E-13	0.00000	.14032L+00	0.00000	448586-01	0.00000	.10658E+00	0.00000	33597E-13	0.00000.	29940E-12 _ 0.00000
.19419E-13	0.00000	.14032E+00	0.00000	44858E-Ó1	.0.00000	106582+00	0.00000	.41459E-1 <u>3</u>	ñ•000'00 <u> </u>	3d563E-12 _0.00000
137046-13	0.00000	14032E+00	0.00000	44858E-01	0.00000	10658E+00	0.00000	10344E-12	0.00000	.37483E-12 <u>0.0</u> 000 <u>00</u>
.87572E-14	0.00000	.1o398L+00	0.00000	.25580F-òF	0.00000	96445E-01	0.00000	.2355¢E-13	0.00000	*58080F-7,5 _0.00000
+68764E-13	0.00000	163981+00	0.00000	22280E-01	0.00000	964458-01	0.00000	.49950E-14	0.00000	.19715E-12 _0.00000
156398-13	0.00000	-:94076E-01	0.00005	9067JE-01	0.00000	.Z8859E-01	0.00000	39561E-13	" 0. 00000 [*]	.22179E-12 0.00000
-23930L-13	0100000	.74076c-01	0.00000	. 90673E-01	0.00000	.28859t-01	0.00000	-14432E-12	_0.00100	. 222158-12 0.00000
.38345E-13	0.00000	20801E+00	0.00000	10883E+00	0.00000	.18175[+00	0.00000	.53954E-13	0.00000	11652F-15 0.00000
-74212E-13	0.00000	.20d01L+00	0.00000	108831+00	0.00000	` .1c1756+00	0.00000	73904E-13	~ooooo,	17075E-12 0.00003
-42152E-13	0.00000	.746878-01	0.00000	.40734E-01	0.00000	27/51E+00	0.00000	61031L-13	0.00000	:43642E-13 0.00000
,555362-14	0.00000	746878-01	0.00000	.40734E-01	0.00000	27751E+00	_0.00000	911872-14	0.00000_	53478L-130.00000

NATURAL FREQUENCY= .1319576+04

TX REAL .	XX IHAG	TY REAL .	YT JAH1	T1 .	T Z L HAG	RX / KEAL	RK IMAG	RY REAL	LHAG _	REAL IMAG
85573E-14	0.00000	.90445E-01	0.00000	203950+00	0.00000	.63451E-03	0.00000	84754E-13		63878E-13 0.00000
-136975-13	0.00000	99445e-01	ő.0000ű	20395£+00	0.00000	684516-03	0.00000	10853E-12	[[0.000000]	43329E-13 0.00000
-418365-13	0.00000	90445E-01	0.00000	20395E+00	0.00000	6d451E-03	0.00000	15652E-12	ີ່ບໍດດຸວ ດໍດີ	12969E-12 0.00000
311846-1-	0.00000	9u445E-01	_0.60000	•503A>E+00	0.00000	.00+51c-03	0.00000	.149856-12		57/200=-13 0.00000
•2099JE-13	0.00000	904452-01	0.00000	205326+00	0.00000	00451E-03	0.00000	.23360E-13	0.00100	9920E-13 0.05065
.387796-13	0.00000	904456-01	0.00000	.20532E+00	_ 0•00000	63451=-03	0.00000	13435E-12	0.00000	12578E=12 [0.0000]
.24912E-13	0.00000	.90445E-01	0.00000	.T+20532E+00	0.00000	.68451E-03	ú:noòoo	.384746-13	0.00000	39502E-130.00000
.24390E-14	0.00000	.90445=-01	0.00000	-20532E+00	J.00000	63451L-03	0.00000	40722E-13	0.00000_	861/6=-13 0.03000
-36016E~14	0.00000	.90445E-01	0.00000	F-20345E+00		.68451E-03	0.00000	~•12975E-13	0.00000	134085-12 0.0000
.173145-13	0.00000	.904456-01	0.00000	.20395E+00	0.00000	63451E-03	0.00000	98866E-1J	0.00000	148136-12 <u>0.0000</u>
-24633E-14	0.00000	90445=-01	0.0000	203458+00	0.00000	684511-03	0.00000	18192E-13	0.00000	#8377E-13 0.00003
_88458E-14	0.00000	90445t-01	0.00006	20395E+00	0.00000	.63451E-03	0.0000	.52135E-13	_0•00000	71393E-13 0.00000
-114418-13	0.00000	90445C-Q1	0.00000	. T+20532E+00	0.00000	6d451£-03	0.00000	.24320E- <u>1</u> 3	0.00000	14039L-12 0.00000
169798-13	0-00000	90445E-01	0.00000	.205328+00	0.00000	.6J451E-03	0.00000	66196E-13	.000000	89030E-13 0.00000
•10103£-13	0.00000	-90445k-01	0.00000	20532E+00	0.00000	.68451E-03	0.00000	89187E-13	_ 0.00000	`14000E-13_[0.00000]
-36085E-13	0.00000	.904456-01	0.00000	.205326+00	0.00000	684511-03	0.00000	-,194338-13	0.00000	207206-130.00000
-24279E-13	0.00000	.904452-01	0.00000	503425+00	0.00000	.68451E-03	0.00000	.93417E-14	0.00000	.83332E-14 0.00000
.106878-13	0.00000	. •90445E-01]	0.00000	-20395E+00]	_a_000000	68451t-03	0.00000		<u>, 0 , 00 0 0 0</u>	.59805E-14 0.00000
•18546E-14	0.00000	90445E-01	0.00000	203956+00	0.00000	684516-03	0.00000	.19027E-14	_ 0.00000	38602E-13 0.00000
"26447E-13	0.00000	90445=-01	0.00000	-203956+00	0.00000	-68451c-03	0.00000	65156E-14]a. 00000	42130 <u>c-</u> 14" [0,00090]

NATURAL FREQUENCY= .1319576+04

				-				
TX Real	TX IHAG	₹¥ ₹¥	EY ` IHAG	TZ REAL	T Z I HAG	R X RE AL	RX Imag	RY KY KZ RZ REAL IMAG KEAL IMAG
.72582E-14	0.00000	10485E+00	0.00000	.81717E-01	0.00000	£14225£+00	0.00000	.37078E-13 0.0000079407 <u>E-13 0.0000</u>
-21740E-13	0,00000	10485L+00	0.00000	81717E-01	0.00000	142258+00	0.00000	538966-13 0.0000049648E-13_0.00000
-427866-13	0.00000	•10435£•00	0.00000	.d1717E-01	0.00000	14225E+00	0.00000	14397E-12 0.00000 .10464E-12 0.00000
-10310E-13	0.00000	.10485£+00	0.00000	817176-01	0.00000	.14225E+00	0.00000	.11271E-12 0.00000 .20991E-14-0.000000
-,33428E-13	n•00900 ·	.10485E+00	0.00000	20279E+08	0.00000	142251+00	0.00000	.18580E-12 0.0000040463E-13 0.09000
-412852-13	0.00000	.104856+00	0.00000	.20279E+00	0.00000	+14225E+00	6,0000.0	29398E-13 0.00000 1 38929E-13 0.00000
45464E-13	0.00000	10485E+00	0.00000	202798+00	0.00000	.14225E+00	0.00000	.53101E-13 0.00000 72886E-15 0.00000
·• 94999E-14	0.00000	10485E+00	0.00000	.202796+00	0.00000	14225t+00	0.00000	.13865E-13 0.00000 0.99771E-13 0.00000
.50499E-13	0.00000	10485E+00	0.00000	.81717E-01	0.00000	.14225£+00	0.00000	27104E-12 0.00000 -44309E-14 0.00000
-88410E-14	0.00000	10485L+00	0.00000	:817178-01	0.00000	142256+00	0.00000	.13364E-12 0.00000 .47823E-13 0.00000
.275176-13	0.00000	.104856+00	0.00000	.817176-01	~ó.00000	-14225E+00	0.00000	.13500E-12 0.00000 .58292E-13 0.00000
·•121/dE-13	0.00000	.104856+00	0.00000	81717E-01	0.00000	.14225E+00	0.00000	24676E-12 0.0000053048E-13 0.00000
•13261E-13	.0*00000	-10485E+00	0.00000	202/9E+00]	0.00000	14225E+00	0.00000	19426E-13 0.00000 - 35226E-13 0.00000
10382E-13	0.00000	.10485E+00	00000	-20279E+00	0.00000	-14225E+Ŏ0	0.00000	.9478 1E-13 0.00000 2-29127E-13 0.00000
-283246-14	0.00000	10485E+00	0.00000	=.20279E+00	0.00000	:14225E+00	0.00000	13152E-12 0.00000 18268E-13 0.00000
+12564E-14	0.00000	10485L+00	0.00000	.20279E+00	0.00000	,14225€+00	0.00000	
16854E-13	0.00000	10485E+00	0.00000	.81717E-01		14225E+00		15139E-12 0.0000 .16330E-13 0.00000
90031E-14	0.00000	10485£+00	0.00000	817176-01	0.00000	142256+00	000000	29380E-12 0.00000 1.12876E-13 0.00005
.551855-13	0.00000	.10485E+00	0.00000	.81717E-01	0.00000	142256+00	0.00000	11008E-12 0.00000 7.45012E-13 0.00000
.20257E-13	ñ*ó9900	.10485E+00	0.000000	81717E-QL	_0.00000	.142251+00	`o*ooooō	
•	•							

NATURAL FREQUENCY= .131957E+04

TX REAL	IX IHAĞ -	IY REAL	TY THAG	- TZ REAL	TZ IMAG	RX KEAL	RA [HAG	RY' . REAL .	IMAG	REAL IMAG
-36432E-14	0.00000	16324t+00	0.00000	15333E+00	0.00000	101215+00	0.30000	11639E-12	0.00000	
-32605E-14	0.00000	16324L+00	0.00000	.15333E+00	0.00000	.101216+00	0.00000	.70812L-13	ა • 00 0 0 0	14692E-13 0.00000
.67902E-13	0.00000	.16324E+00	0.00000	153336+00	0.00000	.101216+00	0.00000	.258891-12	0.00000	31205E-13 [0.00700]
.36938E-14	0.00000	.16324E+00	0.00000	.15333E +00	0.00000	10121E+00	0.00000	271396-12	0.00000	11467E-13 0.0000
-897285-14	0.00000	.163246+00	0.00000	- 490626-01	0.00000	.101214+00	0.00000	14228E-12	0.00300	14097E-14 0.00000
.7717sE-14	0.00000	+163248+00	0.60000	49082E-01	`0.00000	101216+00	0.00000	.17730E-12	0.00000	208046-13 0.00900
*19278E-14	0.00000	16324E+00	0.00000	49082E-01	0.00000	10121E+00	0.00000	42967E-13	0.00000	-,36254E-13_0.00000
.5849JE-15	0.00000	16324E+00	0.00000	490028-01	0.00000	.101216+00	0.0000	532828-13	0.00000	.53567E-14_0.000000
-1263dE-14	0.00000	16324E+00	0.00000	1533 JE+00	- 0.00000	10121E+00	0.00000	.20102E-12		11903E-13 0.00000
.1522JE-13	. 0 . 0 0 0 0 0	16324E+00_,	0.00000	12333E+00	0.000000	-10121E+00	0.00000	24763E-12	0.00000	.22112E-15 0.00003
.84892E-14	0.00000	-1¢324£+00	0.00000	15333E+00	0.000,00	.10121E+00	0.00000	÷.21171E-12	0.00000	414726-13 0.00000
-577668-14	0.00000	.163246+00	0.00000	1533JE+00	0.00000	10121E+00	0.00000	. <u>2</u> 2982E-12	_0.00000	47582E-13 0.00000
-14053E-13	0.00000	.16324E+00	0.00000	.49082 <u>E-</u> 01		-10121E+00_	0.00000	30722E-13_		41271E-13 0.00000
.24155E-13	0.00000	-163246+00	0.00000	49082E-01	0.00000	10121E+00	0.00000	19490E-13	0.00000	38742E-13 0.00000
97999E-14	<u>0</u> .00000	16324£+00	0.00000	49082E-01_	0.00000	10121E+00	0.00000	-24146E-12	. 0.00000	10986E-12 0.00000
.95944E-14	0.00300	163241+00	0.00000	49082E-01	3.00000	.101216+00	0.00000	20206E-12	0.00000	96481E-13 0.00000
43749E-13	0.00000	163248+60	0.60000	1533JE+00	0.00000	101216+00	0.00000	282626-12	n•0ô0ô0 <u>.</u>	63489E-13 0.00000
.15452E-13	0-00000	163244+00	0,00000	.15333E+00	0.00000	.101216+00	0.00000	.321146-12	0.00000	173 d5E-14_0.0000 <u>5</u>
13841E-13	_0.00000	.163244.+00	0.00000	153338+00	_ 0,00000	10121E+00	0.00000	18841E-12	0.00000	.23169e-13 0.00000
.90625E-15	0.00000	.16324E+00	0.00000	·15333E+00	0.00000	10121E+00	0.00000	99056E-13	0.00000	43252E-13 0.00003

MATURAL FREQUENCY= .132474E+04

TX REAL	TX -	KEAL -	TY .	T Z Real	TZ I HAG	, KX KEAL	RX	. RY .	· IHAG	KŽ	RŽ
-24521E-01	0.00000	.743576-13	0.00000	10987E-12	0.00000	.20051±-12	0.0000	31807E-12	0.00000	78565E=02	0.000005
-245212-01	0.00000	.100358-12	0.00000	•16521E-12	0.00000	131/3e-12	0.00000	145466-12	0.00000	78565£-02	
·.39200E-01	0.00900	83405E-13	0.00000	781138-13	0.00000	756076-13	0.00000	m.33399E-12	0.00000	.174156+00	0.00002
39200E-01	0.00000	9d214E-13	0.00000	.5731/6-13	0.00000	.64580c-13	0.00000	233138-12	0.00000	.17215 <u>t</u> +00	~ 0.0000)`
:-1426dE-01	0.00000	308646 <u>-</u> 13	0.00000	253016-12	0.00000	11651E-12_	0.00000	.65237t-12	0.00000		0,00000
14263E-01	0.00000	100065-12	0.63000	.2434JE-12	0.00000	.94158E-14	0.00000	.43257E-12	0.00000	-19171E+00	0-00000
25497E-01	0.00000	•13472E-12	0.00000	19798E-12	0.00000	17786E-13	0.00000	.34657E-12	. 0.00000	. 29537E+00	0.00000
254976-01	0.00000	-25452t-13	0.00000	-239346-12	0.00000	882011-13	0.00000	.33270E-12	0.00100_	.29537E-00	oʻ. <u>. 0</u> 5 5 5 5 5 <u>5 5 5 5 5 5 5 5 5 5 5 5 5 5</u>
•49055E-02	0.00000	185552-13	0.00000	13905E-12	0.00000	-143506-12	0.00000	54446E-12		30565 <u>E</u> +00	0.00000
•49055E-02	0.00000	.13793L-12	0.00000	.156168-12	0.00000	.241116-13	0.00000	+33742E-12	.0.00000	•30565 <u>E</u> • 00	0.00000
~49055Eu2	0.00000	74137E-13	0.00000	149398-12	0.00000	-119256-13	0.00000	~-,454 <u>j</u> 35-i2			0.00002
-490558-02	0.00000	103270-13	0.00000	.72359£-13	0.00000	87647E-14	0.00000	00662E-12	0.00000	•30565 <u>e</u> •05	<u> </u>
.25497E-01	0.00000	.12275E-13	0.00000	151508-12	0.00000	84440L-13	0.00000	.30299E-12		295378+00	
-25497E-31	0.00000	10360L-12	0.00000	156128-12	0.00000	5d230E-14	0.00000	338956-12			o <u>o_ō</u> o.oóź
-14268E-01	0-00000	. 97443F-13	0.00000	178636-12	0.00000	31792L-13	0.00000	.73960E-12	" 0.00000"	··· .19171E+0	0.00000
14268E-01	0.00000	18246E-13	0.00000	. 18962E-13	0.00000	13331E-12	0.00000	86485E-12	0.00000	19171E+0	0.0000
-39200E-01	_0• 0 <u>0</u> 0000		0.00000	54978E-13		•TS048E-1 <u>7</u>	<u>0.00000</u> 0	94311E- <u>1</u> 3	0.00000	•17215E+0	0 0.00000
-39200E-01	0.00000	.124765-12	0.00000	+644465-13	0.00000	240326-13	0.00000	30293E-12	0.00000	.17215L+0	00*60000
.24521E-01	0.00000	75885E-13	0.00000	378326-13	0.00000	93201E-13	0.00000	26610E-12	a•00150 ⁻	78565E-0	5 0 • 000007
-245215-01	0.00v00	₹•1753dE-13	0.00000	51844E-13	0.00000	13502E-12	ó•00000	177716-12	0.00000_	70565E-0	รั๋ง•ักัจงดีวั

		NATURAL	. FREAUEN	CY= .134055	E+04						
TX REAL	T X 1 M A G	TY KEAL	YT Dahi	. TZ REAL	I Z I MAG	RX Real	XX Imag	RY Real	KY IHAG	REAL	RZ
14317E-12	0.00000	11342E-12	0.00000	33864E-12	0.00000	16d13E-12	0.00000	.1435bE+00	0.00000	.12859E-12	0.00000
-76678E-13	0.00000	10604E-12	0.00000	. 35971E-12	0.00000	.197796-12	0.00000	14356E+00	0.00000	21067E-13	0.00000
£1-305018.	0.00000	-14857E-12	0.00000	3476>E-12	0.00000	.25470L-12	0.00000	31233E+00	0.00.00	.3d792e-12	0.00000
.4473sE-13	0.00000	.136552-12	0.00000	.33811E-12	0.00000	234/60-12	0.00000	.31233E+00	0.00000	.49940 <u></u> -12	0.00000
-437348E-13	0.00000	•15765E~12	0.00000	.15415E-12	0.00000	-20283F-15	0.00000	-553916+00	0.00000	41109E-13	0.00000
-112066-12	0.00000	.91961E-13	0.00000	168568-12	0.00000	20308c-12	0.00006	223016+00	0.00000	23344p-13 _	0.00005
.623005-13	0.00000	103856-12	0.00000	.21881E-12	0.00000	19599k-12	0.00000	.494678-01	0.00000	.65612=-12	0.00000.
-94074E-13	0.00000	13993E-12	0.00000	1664UE-12	0.00000	.lo984L-12	0.00000	4946YE-01	0.00000	54419E-12	0•00000
-41856E-14	0.00000	14995E-12	0-00000	21413E-12	0.00000	10799E-12	0.00000	2817oE+00	0.00.00	"33784E-12"	0.0000
-38366L-13	0.00000	867238-13	0.00000	•19146E-12	0.00000	.16157L-12	0.00000	.28176E+00	_0.00000_	259111-12_	0.00002
.95731E-13	0.00000	10045É-12	0.00000	~.12665E-12_	0.00000	26229E-12	0.00000	.28176E+00]	0.00000	- 133763E-12	0.00000
131897E-13	0.00000	13751E12	0.00000	-i0778E-12	0.00000	21755E-12	``0•000 0	281760+00		37402E-12	0.00005
										61557E-12	
.736730-13	0.00000	.919276-13	0.00000	278026-12	0.00000	251446-12	0.00000	49469E-01		~73732L_12 _	0.00000
										.27109£-13	
										385306-14	
.77819E-13	0.00000		0.00000	.23604É-13	0.00000	9336,7E-13	0.00000	*31533F+00	0.00000	654574-12	0.00000
.74169E-13		80416E-13		46533L-13						5745 <u>9</u> £-12	
14601E-12	0.00000	.14205E-12	0.00000	.53041E-13	_0.00000	57997E-13	0.00000	14356E+00	0.00000	566016-13	0.00005
-18673E-12	0.00000	.15162E-12	0.00000	40770E-13		17655L-12	0.00000	[-14356E+00"	0.00000	13517E-12	0.00000

MATURAL FREQUENCY= 1.134105E+04

YX REAL	TX THAG	REAL	YY	TZ TEAL	FZ IHAG`	RK	- 1440	RY RY RY RZ RZ RZ RZ REAL IMAG
<u>7</u> 41686-01	0.00000	. 32450 <u>t-13</u>	_ 0.00000_	370616-13	_0.00000	13123E-12	0.00000	13867E14 _0.0000051985E-Q1 _0.00000
-,74163E-01	_0_00000	- 30078E-16	0.00000	26910E-13]	0.00000	77961E-14	0.00000	.11165E-I1 0.00000 .51385E-01 0.00900
-406238-01	0.00000	-,10316b-12	0.00000	5302E-14	0.00000	.710266-13	0.00000	.95074E-12 0.00300 .29684E.00 0.0000
.40623E-01	0.00000	.273158-13	0.00000	.16470E-13	0.00000	.377865-13	0.00000	15013E-11 0.00000 .29684E+00 0.0000
29392E-01	0.00000	57093E-13	0.000000	25373E-13	0.00000	.27981L-13	0.00000	18867E-11 0.0000017137E-01 0.00000
-29392E-01	0.00000	.59do4E-13	0.00000	42931E-14	0.00000	.633054-13	0.00000	10072E-12 _0.0000017137E-01 _0.00005
-435728-01	0.00000	.10304E-12	0.00000	19394E-13	0.00000	.54341E-13	0.00000	.50612E-12 0.000u0 3375dE.00 0.00000
-43572E-01	0.00000		0.00000	3664 <u>1</u> E-13	ŭ.0000 <u>0</u>	43439E-13	_0.00.000	
-19365E-01	0.00000	.40s16L-13	6.90000	.534236-13	0.00000	52977E-13	0.00000	.19062E-11 0.00000 "19233E+00 " 0.00000]
.19365E-01	0.00000	623316-13	0.0000 <u>0</u>		_0.00000	53202E-15	_0.00000	41680E-12 0.0000019233E+00 0.00000
_19365E-01	0.00000	74049L-13	0.00000	.77389E-15	0.00000	.27357E-13	0.00000	22125E-11 0.00J0014233E+00 0.0000J
.19365E-01	0.00000	361885-13	0.00000		0.00000	392354-14	0.00000	.84746E-13 0.00000 119233E+00 0.00000
-43572E-01	0.00000	774616-14	0.00000	25593E-13	u.00000	•16357£-13	0.00000	25118E-12 0.0000033758E+00 0.00000
.43572E-01	0.00000	.81311E-13	0.00000	-,27403E-13	`ò.000G0	.12816E-13	0.00000	72704E-12 0.0000033758E+00 0.00000
29392E-01	0.00000	.2505at-13	0.00000	374716-15	0.00000	.72044L-13	0.00000	.22807E-11 0.00300 .17137E-01 0.00000
29392E-01	0.00000	.24627E-13	0.00000	79015E-14	0.00000	.53603t-14	0.00000	.61191E-12 0.00000 .17137E-01 0.00000
.40623E-01	0.00000	.558581-13		36202E-L3_	0.00000	12509L-12	0.00000	11658E-11 0.00000 29684E+00 0.00000
.40623E-01	0.00000	955711-13	0.00000		ŭ.00000	51945E-13	0.00000	.1361dE-11 0.0039029684E+00 0.00000
74165E-Ui	0.00000	29682k-13	0.00000	313208-13	0.00000	.58126±-13	0.00000	10213E-12 0.0000051985E-01 0.00000
-,74168E-01	0.00000	118762-14	0.00003	 .31547E-14	0.00000	-100446-12	0.00000	12890E-11 0.0000051945 <u>E-01 0.00</u> 000

NATURAL FREQUENCY ... 135881E+04 ...

TX ŘEAL	TX THAG	KLAL	TY THAG	TZ REAL	TZ IMAG	K.C.	RK " IHAG	RY	ky	REAL	kZ Inag
-19340E-03	0.00000	.995421-15	0.00000	-29362E-13	0.00000	.70615E-13	0.00000	26549E-11	0.00000	-45164e-0	0.00000
.193408-03	0.00000	69486E-13.	0.0000	-,62154E-14	0.000000	12316E-12	0.00000	26389E-11	<u></u>	-451644-0	<u> </u>
-10141E+00	0.00000	.216926-13	0.00000	-555978-13	0.00000	.614372-13	0.00000	.59637E-12	0.00000	147621+0	ด์ _ื่อ•อำอัติฮ
-10141E+00	`a₊¢აoōo๋	.450496-13	0.00000	38253E-13	0.00000	248776-13	0.00000	.533078-12	0.00000	14762E+0	0_0.00000
-41078E-01	0.00000	.246546-13	0.00000	-72068E-13	0.00000	52867£-13.	0.00000	.53648E-1ļ	0.00000	361946•0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
.41078E-31	0.00000	107986-13	0.00000	11421É-12		.427566-13	9.00000	.55435E-11	0.00000	361942+0	00+00000_
.50639E-02	0,00000	223536-13	<u>"0.00000</u> -	.10475E-13	_0.00000	18202E-13	_ 0.00000.	274736-11	0.00000		1 000000
.506398-02	0.00000	31884[-13	0.00000	10985E-L3	0.00000	.42953E-13	0.00000	293126-11	0.00000	720426-0	r 0 *00 <u>0</u> 00
-65593E-01,	0.00000	~3?853 <u>E</u> -13	0.00000	.44720E-13	_0.00000	-11493E-14	0.00000	41300E-11	0.00000	27764E+0	_0 <u>_00000</u> 0_
.65543E-01	0.00000	.525322-14	0.00000	87930E-13	_0.00000	31736t-13	_0.0000v_	385a9E-11	_ 0• ,000000	277 <u>04c</u> +0	<u>0.0000</u>
-655936-01	0.00000	35232É-13	0.00000	*14421E-13	0.00000	952318-13"	0.00000	-40725E-11	0.00000	.27764E+0	0_0.00,001
.655938-01	0.00000	.26437E-13	0.00000	38932E-14	0.00000	.633036-13	0.00000	.383968-11	0.00000	. 277646.0	0 0 0 0 0 0 0 0 0
.506392-02	0.00000	26947E-13	Ô.00000 Î	351760-13	0.00000	.526798-13	0.00000	-28056E-11	0.00000 _	.72642E-0	r 0.00000_
.50639E-02	0.00000	213076-13	0.00000_	.858526-14	0.00000_	64937E-13	0.00000	29395E-11	ò.00000 _	72642E-0	1.0.00000
.41078E-01	0.00000	145221-13	0.0000	.10509E-12	0.00000	.329221-13	0.00000	53694E-11	0.00000	.301942+0	o_ 0*0?0ō5
,41078E-01	0.00000	240608-13	0.00000	-,82945E-13	0.0000	454698-13	0.00000	54829E-11	ō•00ōcò _	.301946+0	io _ 5- 50 200
101416+00	0.00000	-59016E-14	0.00000	*889256-14	0.00000	45535E-13	ò•00000	01727E-12	0.00000		<u>10_10.000</u> 00
.101416+00	0.00000	.487731-13	0.00000_	293718-13	0.00000	-128278-12	0.00000	50493E-12	0.0000	.147626+0	0.00000
19340E-03	0.00000	196615-13	0.00000	471178-13	0.00000	.249435-13	0.00000	-26630E-11	n* 00 0 0 0 ,	45164E-0	ir ģ•boban
193408-03	5.00900	2006BL-13	0.00000	77682E-13	0.00000	775306-13	_0,00000		0.00000	45104E-0	1 0.00000

TX	% F V L	TY	TZ	I
IHAG		IHAG	, REAL	HI.
			,	

NATURAL FREQUENCY= .135899E+04

TX Real	TX Imag	K F V ľ L Å	TY Imag	TZ REAL	T Z	кx	Rx	RY	. RY _	RZ TI	- RŽ
-		WENE	TIMO	, XEAL	, I HAG	4F AL	DAHI	REAL	IMAG	" KEAL	OAhI
-92605E-01	0.00000	-511426-13	0.00000	.28252E-14	0.00000	827346-13	0.00000	-,12691E+00	0.0000	164826+00	0.000000
•92605E-01	0.00000	.169925-13	0.00000	41267E-13	0.00000	.15594E-12	១•៣០០ថ្មីភ្នំ	12691E+00	0.00109		
.57432E-01	0.00000	11011E-13	0.00000	36519113	0.00000	28462E-13	0.00000	.27056E-01			
.57432E-01	0.00000	76857E+13	0.00000	24990E-13	0.00000	14263£-13	0.00000			15945E+00	•
.833936-01	0.00000	.24539L-14	0.00000	56665E-14	0.00000	.185191-13	0.0000			B9203=-01	
.83393E-01	0.00000	30048E-13	0.00000	-47345E-13	0.00000	-34742t-13	0.00000		1	.89203E-01	
,39957E-01	3.00000	•15A35E-13	0.00000	_33461E-13	0.00000	.59797E-13	0.00000			<u>.14076</u> £ <u>*</u> 00	
139957E-0L	0.00000	.24539L-13	0.00000	-17665E-13	0.00000	950646-14	0.00000			-14076£+00	
,70130E-01	0-00000	•13288€-13	0.00000	.70542E-14	0.00000	- "-996261-15	0.00000			1006d£+00	
.70130E-01	0.00000	.23252E~13	0.00000	20692E-13	0.00000	.19939E-13	0.00000			10068E+00	
701305-01	0.00000	58410b-13	~0.0000 ₀	27817E-13	0.00000	.753208-13				•100mBd+00	
-70130E-01	0.00000	651056-13	_0.00000 <u></u>	.12508E-13	_0.00000	47959E-13	0.00000			10068E+00	
.399576-01										14076E+00	
39957E-01	0.00000	10174E-13	0.00000	41906E-13	0.00000	25693£-13	0.00000	-13664E+00	. 0. 00000	+14076E+00	0.0000
.833936-01	0.90000									86503E-0T	
-83393E-01	0.00000	75746E-13	0.00000	-167448-13	0.00000	49475E-13	0.00000	25971E+00	~ ~~0.00000	89203k=01	0.0000
.57432E-01	0.00000	531996-13								15945L+00	
57432E-01	0.00000	.392081-13	0.00000	19822E-13	0.00000	-67022Ê-13	0.0000			15945£+00	
10-340926	J.00000	.14076[-13	0.00000	.10875E-13	0.00000	140025-12	0.00000			16482E+00	
92005E-01	0.00000			• d2664E-1,4.						• 16482L+00	

NATURAL FREQUENCY= .137313E+04

TX REAL	TX IHAG	TY KEAL	TY .	TŽ Řeal	T. I HAG	KX	R.A. I MAG	" REAL	RY IMAG	REAL	RZ IHAG
.10392E-12	5.00300	.2/122E-13	0.00000	.11096E+00						.34938E-13	
39732E-13	0.00000	389596-14	0.00000	11096±+00	0.00000	196006+00	0*00000	87910E-13	[0.000.06]	190546-13	0;• 0 0 0 0 0 0 0 0 j
.71073E-14	0.00000	-112596-12	0.03000	.455471-01	0.00060	205791+00	0.00000	34344E-12	0.00000	.401002-12	0.00000
•34917E-13	0.00000	118448-12	0.00000	45549F-01	0.00000	.20579E+00	0.00000	+35355E-12	0.00000	52925E-12	0_00009
.1346/E-12	0.00000	62176E-13	0.00'000	233596+00	0.00000	.51021E-02	0.00000	.259646-12	0.00000	155956-12	0.0000
-98002E-13	0.00060	.39268E-13	0.00000	.23359E+00	0.00000	51021E-02	0.00000	381218-12	0.00000	.99706c-13	0,00000
.30811E-13	0.00000	57058E-13	0.00000	.53720E-01	0.00000	243576+00	0.00000	86638E-13	~9• 0000ē	•30>93¢-13	oʻ*nōòōō
-25013E-13	0.00000	.11¢36E-12	0.00000	53720E-0i	0'-00000	24357E+00	_0+0000 <u>0</u>	•15025L-12	0.00000	47790L-13	0.00000
.105398-12	0.00000	- 1578Í6L-13	0.00000	- 17329E+00	ŭ:00000	13571E+00	0.00000	40912E-13	0:00000	1d2d0[-12	0.00000
•12710E-12	0*00300	875391-14	a*aaoán	17329L+00	.0.00000	.13571E+00	0.00000	;~1-3 410£-12_	000000	13495E-12	
-51093E-1J	0.00000	.20433E-13	0,00000	~17329E+00	0.00000	13571E+00	0.00000	.15515E-12	0.00000	42046E-12	0.00 <u>000</u>
-10043E-12	0.00300	689268-13			0,00000	•13571E+00	0.00000	27972E-12	0.00000	41133E-12	0.00000
-42169E-13	0.00000	94223E-13	0.00000	23720E-01	0.00000	- +24357±+00	ó•00000	25157E-12	0.00000	.17230E-12	0.00000
•56257E-13	0.00000	.746678-13	0.00000	.53720É-0Ĺ	0.00000	24357E+00	,o•áaooo	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	_0.00009		_ 0.000 <u>0</u>
-74405E-13	0.00000	126516_13	0.00003	533255r+00	0.00000	51021E-02	, ö•ōoooo	19890E-14	0.00200	54365E-13	0.62000
-88953E-14	0.00000		0.00000	~~.Z3359E+00	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	51021E-0Ž	0.00000	12171E-13		12674E-1Z	<u> </u>
-66957L-1J	0.00000	.15308E=12	0.00000	45549E-01	0.00000	20579E+00	0.00000	561168-13	_ 0.00700 ⁻	•34375 <u>E</u> -12	0.00000
49639E-13	ŏ.0000o	94585E-13	0.00000	.4554 JE-01	0.00000	.20579£+00	0.00000	.819286-13	0.00000	.40029E-12	อ์•์ดวดื้อฏี
.12476E-12	0.00000	64396E-İ4	0.0000	[10966÷00	0.00000	136005+00	0.00000	371o3E-13		996405-13	0.00000
-60024E-13	0.00100	302081-13	0.00000	.110966+00	0.00000	19600L+00	0.00000	823126-13	0.00000	_ •50596 5 -13	`0*0000 <u>5</u>

NATURAL FREQUENCY= -137652E+04

TX . REAL .	TX IHAG	TY Real	TY IMAG	TZ Real	TZ 1HAG	R K RL A L	RX Ihag	RY Real	RY IMAG	RZ REAL	IMAS —
-84676E-01	0.00000	545408-13	0.00000	• 36809L−13	0.00000	.652411-13	0.00000	.54919E-12	0.00000	45620E-01	0.0000
.84676E-01	0.00000	-,94677E-15	0.00000	•13,74LE-13	°0.00000	.32440E-13	0.00000	.503118-12	[0.00000°	[45620E-01]	0.00000
27462E-01	0.00000	.22026L-1J	0.00000	75371E-13	0.00000	424748-13	0.00000	88181E-1J	0.00000	39990E+00	0.00000
27462E-J1	0.00000	•17965E-13	0.00000	13124E-13	0.00000	.53020E-13	0.00000	491465-13	0.00000	399906+00	0.00000
-+64429£-01	0.00000	41G181E-12	0.00000	29509E-13	0.00000	50751E-13	0.00000	125156-11	0.00300	•ิงอุดอัลธ์ดัฐ	0.00000
64427E-01	ŭ.00000	33175E-13	0.00000	.100588-12	0.00000	919996-13	0.00000	115806-11	_0.0 <u>0</u> 0000		, o • o ɔ ɔ ɔ ɔ ɔ ɔ ɔ ɔ ɔ ɔ ɔ ɔ
91139E-02	0.00000	6d200t-14	0.00000	~25413E-14	0.00000	.94207E-14	0.00000	55636E-12	0.00000	678678-01	_0:0000 <u>0</u>
- ₄ 91137E-02	J.00J00	.162891-13	0.00000	16896E-1J	0.00000	354171-13	0.00000	.53321E-12	0.00000	678676-01	_0•0000 <u>7</u>
87030E-01	0.00000	77323b-13	0.00000	``.12735E-Ĭ3	0.00000	13664=-13	0.00000	•12227E-11	0.00000	~25332E+00	0.00000
870308-01	0.00000	.404166-13	0.00000	2,7099E-13	. 0.00000	.82492E-13	0.00000	.12769E-11	_ n• hopo ô	25332E* <u>0</u> 0_	<u> </u>
-870308-01	0.00000	231088-13	0.00000	~~. 41973E-13	0.00000	298608-13	0.00000	94816E-12	0.00000	25332=+00	_ <u>0</u> _000000
-87030E-01	'u.00000	11019E-13	ີວໍ.ດ່ວນບໍ່	.13416E-13	6.00000	10116E-14	0.00000	~.45828E-12	0.00000	25332E+00_	_0_00000
-91139E-02	0.000,00	.31137 <u>t</u> -13	0.00000	89670E-14	0.00000	40859E-14	0.00000	116878-11	0.00000	67867E-01	0.00000
.911398-02	0.00000	22350E-13	0.00000	£1-351885•	0.00000	58093E-13	0.00000	12128E-11	0.00000	67867E-01	0.00000
_+64429E-01	0.00000	.23568 <u>E</u> -13	0.00000	. •447226-13	0.00000	.17821E-13	0.00000	150438-11	0.00000	00009E-01	0*00000
.64429E-0L	0.00000	.73067L-14	0.00000	~44438E-13	0.000,00	.48794E-13	0.00000	.159426-11	_ 0.00000	-60068E-01	0.0000
-27462E-01	0.00000	.429928-13	0.00000	18997E-13	0.00000	848216-13	0.00000	. •44874E-12	0.00000	-* 3å330F+00	0.00003
.27462E-01	0.00000	407316-13	0.00000	.51665E~13	0.00000	.116336-13	0.00000	.34466E-12	0.00000		0.0000
846758-01	0.00000	11488E-13	0.00000	711315-14	0.00000	.68219E-13	0.00000	96246E-12	0.00000	45620ç-01	_o•0000á
84676E-01	J.000J0	-33506E-14	0.00000	172166-13	0.,00000	.44452E-13	0.00000	89705E-12	0.00000	45620L-01	0.00000

NATURAL FREQUENCY = .1387861+04

TX	TX	TY T	TY THAG	TZ TZ	TZ	KEAL .	RX IMAĞ	REAL	TWAC	RZ	THAG .
Z-67064E-13	0.00000	128718-13	0.00000	239166,-13	0.00000	102228-12	0.00000	977206-01	0.00000	.25680E-13	0.00000
1894bE-13	0.00000			.80165E-1J	0.00000	.209228-12	0.00000	977208-01	ี จึงเืออยจิ <i>ด</i> ์	23624 <u>E</u> -13	0.00000
24617E-13	0.0000ô	.394258-13	0.00000	-20324E-1J	0.00000	.19203E-12	0.00000	25583E+00	0.00000	16683E-12_	0.00000
277678-13	0.00000	507606-13	0.00000	616508-13	0.00000	234826-12	0.00000	.255J3E+00	0.00000	·23635£-12]	0.00000
-428436-13	0.00000	163088-13	0.00000	.32887E-12	0.00000	982558-13	0.00000	•31623E+00	0.00000		.0.00000.
58768E-14	0.00000	104721-14	0.00000	28450F-12°	0.00000	•91845E-13	0.00000	31623E+00	_ 0.00,000	74555 <u>E</u> -13	0.00000
+15837E-13	0.00000	605556-13	0.00000	645846-13	0.00000	182901-12	0.00000	-+255835+00	0.00000	.2d744E-13	0.00000
	0.00000	•66768E-13	0.00000	.53119£-13,	0.00000	•337531-12	ō•0ōōan	255a3E+00	0.00000	. <u>. 5</u> 9761 <u>E</u> -13	<u>0.0000</u>
60777E-13	0,00000	. 25786£-13	0.00000	15799E-12	0.00000	~ `.L0429E-12	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~97720E-01 <u>~</u>	0.00000	18406E-12	0.00000
-40915E-13	.0.00000	449586-13	0.00000	.104a5E-12	0.00000	171356-12	0.00000	977201-01	0.00000	- <u>_</u> 10012 <u>-</u> 12	0*03005
35863E-13	0.00000	.40204E-13	0.00000	.178248-12	0.00000	.149606~13	0.00000	. 977208-01	U.00000	16309[-12]	0.00000
= <u>.27774</u> F-13	_o•oööoo_	572176-13	0.00000	14636E-12	000000	98989£- <u>13</u>	_0.00000_	97720E_01	0.00000	27036E-1Z	0.00000
- -778696-13	3.00000	384601-13	0.00000	.366308-13	0.00000	17314t-12	0.00000	25583E+00	0.00000	35582E-13	0.00000
-117912E-13	0.00000	-409766-13	0.00000	.162188-13	0.00000	•23285E-12	0.00000	.25583E+00	u•00000	103306-13	0.00000
140598-13	0.00000	-*300\IF-Ti	0.00000	20000e-12_	0.00000	.414626-13	ù.º00000 ¯	-316236+00	_0.000 <u>00</u> _	844186-13	0.00000
88301E-13	0.00000	· .14878L-Ī3	0.00000	~~.14230E~12~	0.00000	.168826-13	0.00000	316236+00	0.00000	_18038E-12	0.00000
635788-13	0.00000	-25668E-13	` 0.00000		0.00000	.11420t-12	0.00000	25583E+00	0:000.00	.3600ZE-12	0.00000
.211oJE-13	0.02000	661391-13	0.00000	223746-13	0.00000	19757E-12	0.00000	255d3E+00	0.00000		_์0ั≛คงดงจั
13849E-13	0.00 000	.47801±-14	0.00000	.95631E-13	0.00000	33026t-13	0.00000	_ 49772UE-01	0.00000	407116-13_	_0*00000
81435E-13	9.00000	51233,-14	0.03000	123008-12	0.00000	-175736-12	0.00000	977200-01	0.00000	.63457t-13	າ ວາງຄຸ

NATURAL FREQUENCY= .140128E+04

TX Real	TX I hag	TY Real,	TY Imag	TZ ' REAL	TZ I mag	RX KEAL	R.K. I MÅ G	PY REAL	T Y Y	RZ R KEAL IN	.Z IAG
.20156E-01	0.00000	+25604t-12	0.00000	.16644E-12	U.00000	-16524E-11	0.00000	.38080E-12	0.00000	.51989b-01 0.	.00000
20156E-U1	0.00000	22629E-12	0.00000	•15224E-12	0.00000	.16130E-11	0.00000	-235728-12	0.00000	.51989E-01 0.	00000
.11150E+00	0.00000	.90233E-12	0.00000	27952E-12	0.00000	10248E-11	0.00000	374858-12	0.00000	46142=-01,04	000005
•11155E+0p	0.00000	891106-12	0.00000	29997E-12	0.00000	10015E=11	0.00000	20055E-12	0.00000	461426-01 0.	, ດວ <u>້</u> ນວວີ
.47914E-01	3.00000	58684E-12	0.00000	.397146-12	0.00000	.74467L-12	0.00000	25147E-12	_0.00000	<u>418216+00 _ 0.</u>	တဲ့တို့တို့တွင်
.47914E-01	0.00000	.494188-12	0.00000	.413265-12	0.00000	.793246-12	10.00000	185858-12	0.00000	41821E+00 0.	. <u>0</u> 0002 <u>0</u>
.10997E+00	0.00000	60614E-12	0.00000	ُةِ-1ِ\$5020 كَلْ. - -	0.00000	.43172E-12	0.00000	.58927E-12	_`````````````	. 18344E+00 . Ó.	,00000
-10797E+0J	0,00000	.50017E-12	0.00000	26846E-12	0.00060	.42194E-12	0.00000	. j. 55309E-12	0.00000	18344£ <u>+</u> 00 <u>0</u> .	, 0 <u>000</u>
.47127E-01	0.00000	.63516E-12		13302E-12	0.00000	434226-12	0.00000	431896-12	0.00000	.11315c+00 0.	00000
.471278-01	_0.00000	51119E-12	0.00000	16447E-12	0.00000	50826E-12	0.00000	40487E-14	<u> </u>	•11315e+00 0.	03000
.47127E-01	0.00000	.50022E-12	[0.00000]	15255E-12	_0.00000	-, 44854E-12	0.00000	21612E-12j		11315E+000.	. 00,000
-471278-01	0.00000	502728-12		<u>-184276-12</u>	0. <u>0</u> 00000	32705E-12	0.00000	37888E-12	0.00000		00000
-10997E+00	0.00000	68978E-12	.0.00000	<u>.2</u> 41356-12	0.00000	.52997E-1 <u>2</u>	. 0.00000	.45446E-12	<u> </u>	.183446+00 0.	00000
•10997E•00	0.00000	.60650E-12	0.00000	+295448-12	. 0.00000	.39634c-12	0.00000	.820571-12	0.00000	.183448+00 0.	. 00000
.47914E-01	0.00000	435546-12		38218E-1Z	0.00000		0• <u>0</u> 0000_	22441E-12	0.00000	41a21E+000.	. 00000
.47914E-01	0.00000	.4455BE-12	0.00000	47431Ē-12	0,00000	.64763E-12	`~ 0.0000°	522271-12	0.00000	41821E+00 0	เกรียนรู
.11156E+0V	0.00000	.937338-12	0.00000	29937E-12	_0.00000	104066-11	0.00000	32834E-12	0.000,00	40142=-01 0-	00005
•1115 ₆ E+00	0.00000	874415-12	0.00000	_ •32492E-12	0.00000	97352E-12	0.00000	21460E-12	0,00000	461426-01 0	.00000
.20156E-01	0.00000	.13515E-12	. 0.000000			.14722E-11	_ 0.00000	.33847E-12	000000		00000
*2015oE-01	0.00000	17172E-12	0.00000	140556-12	0.00000	.1547/2-11	0.0000	-321766-12	0.00000	.51989E-01 O.	, სენეშ

NATURAL FREQUENCY= .140228E+04

	TX REAL	TX IMAG	TY KEAL	TY IMAG	TL' REAL	TZ DANI	R X Al Al	R.K. IHAG	RY Real	KY Imag	RZ REAL	RZ THAT
			_	0.00000	.27796E-01	0.00000	.30640E+00	0.00000	15039E-12	0.00000	_*1300gr_T	2 0.00000
	308746-13		400/7E-01	0.00003	.27790E-01	0.00000	.30640£+00	0.00000	34878E-13	0.00000_	_4#68BE-1	<u>i </u>
	199108-12		.178558+00		581078-01	0.00000	20233E+00	0.00000	7.220348-13	0.00000	. 19769£-1	50.030000_
	.138336-12	0.00000	17H55E+00	0.09000	581071-01	0.00000	202336+00	0.00000				3 0.0000
	.23248E-13	0.00000	10196L+00	0.00000	65435E-01_	0.00000	-13870L+00	0.00000				2 0.0000
	81923E-13		-10196L+00				-138702+00		548226-13			
	.16457E-12	0.00000	12790E+00	0.00000	58437E-01				•			
	789950-13	0.00000		0.00000	58437E-01	0.00000	. •94170£-01	0.00000	69604E-13	0.00000	24405 <u>L</u> _1	3 0.00000
;	58383E-13	0.00000	-11273E+00	0.00000		_9•00000	91585E-01	00000	.10185E-12	_0.00000	.501936-1	3 0.00000
	.36042ê-Î3	0.00000	112736+00	0.00000	33202L-01		915856-01					
	.964405-13	0.00000	.112731+00	0.00000			01585:-01					
;	75680E-11	0.00000	11273E+00	0-00000	.33202E-01	0.00000	`91585E- <u>Ô</u> l	_0.00 <u>0</u> 00			20323E-1	13 0.00000
	.137286-12	0.00000	12790£+00	0.00000	.56437E-Ó1	0.00000	.94170E-01		19562E-13			
	.18309E-12	0.00000	•12790L+00	0.00000	.584376-01			,	23082E-12			
	.11015E-12	0.00000	101966+00	ŏ•0000ō	85439E-01	^.000 <u>0</u> 0	138798+00					
	. 38339E-13	0.00000	~ 10196E+00	0.00000					- 24877E-12			
	_13587E-12	0.00000	.17855£ • 00	00006.0	58107E-01	0.00000	20233E+00					_
	-235056-12	0.00000	178551+00	0.0000	.58107E-01	0.0000	20233E+00	~0.0000	232788-13			
	.508752-13	0.00000	.40077E-01	0.00000	27796E-01	0.00000						
	.917406-13	0.00000	40077E-01	0.00000	277966-01	0.00060	.30640L+09	0.00000	695778-13	0.00000	• 17447E-	15 0.00000

NATURAL FREQUENCY= .140788E+04

TX Real	TX IHAG	TY Řeal	T¥ I HAG	TZ Real	IT I HAG	KX Keal	R.K. I HAG	RY Real	AA KA	KŽ – KŽ –	ŘZ THAG
.677696-01	0.00000	40579E-13	0.00000	-34134E-13	0.00000	.11651t-12	0.00000	132236-10	U.00000	311836-01	້ ດີ . ພວກທົ່ງ
.6776+E-01	0.00000	209146-13	0.00000	30146E-13	0.00000	.741155-13	0.00000	13244E-10	0.00000	~.311a3E-01 <u></u>	0.00003
-16291E-01	0.00000	.650071-13	0.00000	54685C-14	0.00000	76537E-13	0.00000	.135271-10	0.00000	35297E+00_	0*00000
.16291E-01	0.00000	89936E-14	0.00000	34214t-13	0.00000	235116-13	0.00000	•13574E-10°	0.00000	35297E+00	0.00000
-13920E+00	0.00000	.510346-13	0.00000	36594E-13	0.00000	936818-13	0.00000	•12005E-10	0.00000	.150558+00	0.00000
1392GE+00	0.00000	+86731E-14	0.00000		0+00000	256961-13	0.00000	.12062E-10	0.00000	.15055F+00	0.00000
-53942E-01	0.00000	534248-13	0.00000	~ 46553L- <u>1</u> 3	0.00000	.10761t-12	0.00000	26287E-10	0.00000	292716+00	
.53942E-01	0.00000	-59678E-13	0.00000	26695E-13	0.00000	.3/5851-13	0.00000	,26120t-10	0.00100	29271E+00	0.00000
-337816-01	0.00000	.31968E-13	0.00000	₹29132E~13	0.00000	14759E-12	0.00000	140538-10	_0.00000	391576-01	0.0000
-33781E-u1	0.00000	37835E-13	0.00000	49752E-13	_0.00000	+2Jl16E-13	.0.00000	13840E-10	_a.ooooò	39157E-01	0.0000
33781E-01	0.00000	.17J99E∸13	0.00000	27841E-13	0.00000	68384Ê-14	0.00000	T13468E-10	0.00000	391576-01	<u> </u>
_337dlE-01	0.00000	18595E-13	0.00000	51747E-13	Q.00000	.16511E-13	0.00000	.137596~10	0.00000	.39157E-01	0.00000
-539426-01	0.00000	645178-13	0.00000	.44524E-13	0.00000	93797t-13	0.00000	26023E-10	_0.00000	29271E+00	0.00000
.53942E-01	0.00000	.14007E-13	0.00000	,29480E-13	0.00000	·1186ZE-13	0.00000	26258E-10	0.00000	29271E+00	0.00000
-13920E+00	0.00000	.167131-13	0.00000	•46838E-14	0.00000	810951-13	0.00000	-12246E-10	0.00000	12022E+00	0.00000
.139208+00	0.00000	.129246-13	0.00000	31437E-13	0.00060	.30416E-13	0.0000	-124126-10	0.00000	-•150555+00	0.00000
-16291E-01	0.00000	.61412E-13	0.00000	351740-13	0.00000	.35004£ - 13	0.00000	.13516E-10	0.00000	-35297£+00	_0.02300
-16291E-01	0.00000	.81957E-15	0.00000	.646d7t-13	0.00000	83646E-13	0.00000	-13348E-10	u.00000	.352976+00	0.0000₫
-67769E-01	0.00000	204656-13	0.00000	.32732t-13	0.00060	96552L-14	0.00000	1335/E-10	0.00000	.31183c-01	0.00000
-67769E-01	0.00000	30477L-13	0.00000	49122E-13	0.00000	•11367e-12	0.00000	131996-10	0.00000	~31183É-01	0.00000

NATURAL FREQUENCY -141188E+04

TX	00 _ 0 • 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0
-80295E-01 0.0000046307E-13 0.000001892E-13 0.00000 .36345E-12 0.00000 .12803E+00 0.0300012769E+00 .79055E-01 0.00000 .23112E-12 0.000004855E-13 0.0000026433E-12 0.0000013043E+00 0.0000014739E+00 .79055E-01 0.0000015144Ê-12 0.0000012326E-13 0.0000015005E-12 0.0000013043E+00 0.0000014739E+00 .7905E-12 0.0000015190E-12 0.0000015190E-12 0.000004855E-13 0.00000 .24955E-12 0.0000011755E+00 0.00000 .20406E+00 .7905E-12 0.0000011755E+00 0.0000020406E+00 .7905E-12 0.0000020406E+00 0.000002	000*00000_ 000*00000_ 000*00000_ 000*00000_
.790\(\frac{1}{2}\) 0.00000 \\ \tag{-1514\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-12326\(\hat{E}\) -13} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1500\(\hat{E}\) -12} \\ 0.00000 \\ \tag{-1755\(\hat{E}\) +00} \\ \tag{-1755\(\hat{E}\) +00} \\ \	000 • 00 00 0
.79035E-01 0.0000015144É-12 0.0000012326E-13 0.0000015075E-12 0.0000013043E+00 0.0000014739E+0 .33191E-01 0.0000015190E-12 0.00000 .47855E-13 0.00000 .24955E-12 0.0000011755E+00 0.0000020406E+0 .33191E-01 0.00000 .86630E-13 0.0000083785E-13 0.00000 .14493E-12 0.0000011755E+00 0.0000020406E+0	0 _ 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
.33191E-01 0.0000015190E-12 0.00000 .47855E-13 0.00000 .24955E-12 0.0000011755E+00 0.00000 .20406E+0 .33191E-01 0.00000 .86630E-13 0.0000083785E-13 0.00000 .14493E-12 0.0000011755E+00 0.0000020406E+0	0.000000
.33191E-01 0.0000015190#-12 0.00000 .47855E-13 0.00000 .24955E-12 0.0000011755E+00 0.00000 .20406E+0	
-331910-U1 0.00000 .866306-13 0.00000 -83785E-13 0.00000 .14493E-12 0.0000011755E+00 0.0000020406E+0)0 <u></u> 0*0000_
.75438E-01 0.0000012350E-12 0.0000015813E-13 0.00000 .77427E-13 0.00000 .25255E+00 0.0000013136E-0	<u> </u>
.75438E-01 0.00000 .75985E-13 0.00000 .74292E-13 0.00000 .44100E-13 0.00000 .2525,E+00 0.00000 .131366E-0	วтอ•ัยวัง <u>ด์จั</u>
.43459E-DL 0.00000 .14929E-12 0.000001567dE-00 0000010031E-12 0.0000013260E+00 0.000001567dE-0	10 0.00000
-43454E-01 0.0000085926E-13 0.0000042715E-13 0.0000078527E-13 0.0000013260E+00 0.0000015678E+0	o 0.00000
.43459E-01 0.00000 .15956E-12 0.00000 .65908E-14 0.0000011208E-12 0.0000013260E+00 0.00000 .15678E+0	00 0.00000
-434596-01 0.00000927216-13 0.00000 -334946-13 0.00000118326-12 0.00000132606+00 0.00000156786-6	
-75438E-01 0.0000013751L-12 0.00000 ./7483E-13 0.00000 .11294E-12 0.00000 .25255E+00 0.00000 .13130E-0	
-75438E-01 0.00000 -43295E-13 0.00000 1.33812E-13 0.00000 .60653E-13 0.00000 -25255E+00 0.0000013136E-€	oi " oʻōooōōoʻ
.33191E-U1 0.0000010633E-12 0.0000064497E-13 0.00000 .12195E-12 0.0000011755E+00 0.0000020406E-0	
-33191E-01 0.00000 -10143E-12 0.0000049886E-13 0.00000 -18320E-12 0.0000011755E+00 0.0000020406E+	000 • 00 000
-79085E-01 0.00000 -18576E-12 0.0000099300E-14 0.0000013223E-12 0.0000013043E+00 0.0000014739E+0	00 0.00000
79085E-01 0.0000012146E-12 0.0000078851L-13 0.0000022351E-12 0.0000013043E+00 0.0000014739E+	
80293E-01 0.00000 .24706E-13 0.00000 .36009E-13 0.00000 .24042E-12 0.00000 .12803E+00 0.0000012769E+	00 `0.00000
.80298E-01 0.0000062198E-13 0.0000056028E-13 0.00000 .26320L-12 0.00000 .12803E+00 0.00000 .12769E+	

		` NA TURAI	. FREGUEN	CY= .141740E	• 04						
TX REAL	TX IMAG	IY KEAL	TY IHAG	T/ REAL	TZ I MAG	, RX Real	RX Dahi	RY Real	KY Imag	REAL	RŽ IHAG
26720E-13	0.00000	-32785E-13	0.00000	312876-13	0.00000	.86943E-13	0.00000	49469E-01	0.00000	.76180E-13	0.00000
-98900E-13	0.00000	70363E-14	0.00000	.584756-13	0.00000	-21097L-12	0.00000	-49469E-01	0.00000	15830E-12	0.00000
.91871E-15	0.00000	.90955E~13	0.00000	28261E-13	0.00000	404271-13	0.00000	.14356E+U0	0.00000	222774-12	0.00000
1485UE-12	0.000,00	112865-12	0.00000	515146-13	0.00000	197268-12	0.00000	143566+00	0.00000	.352336-L3	0.00005_
25176E-13	0.00000	510281-13	0.60000	.97957E-13	0.00000	.753276-14	0.00000	22361E+00	0.00100,	.51280c-12	0.00000
78175E-13	0.00000	.24007E-13	0.00000	17265E-13	0.00000	.11280E-12	0.00000	.22361E+00	0.00000	.19290b-12	
.46231E-13	υ. 00000	755076-13	0.00000	10842E-12	0.00000	.40137L-13	0.00000	.281766+00	.0.00000	.14463E-12	0.00000
-155141-12	0.00000	.712398-13	0.00000	23154E-13	0.00000	.698325-13	0.00000	28176E+00	`u.00000~	14089E-12	_o•vôაō₁ <u>_</u>
.14076E-14	0.00000	.44094L-13	0.00000		`a.aŏaaa	.51098E-13	0,60000	31233E+00		17495 <u>E-</u> 12	0.00000
405016-13	0.00000	371058-13	0.00000	54860E-13	0.00000	135776-12	0.00000	₹31233£+00	[0.00000]	.111795-12-	_0*00000 <u>1</u> _
-98070E-13	0.00000	.28420E-13	0.00000	.429666-13	ò.00000	109746-12	0.00000	31233E+00	_0.00000_	.232866-12	
-42177E-14	v.000u0	885898-13	0.00000	517282-13	0.00000	.12675E-14	0,00000	312338+00	_ 0.00000 ~	.63349E-14	
10195E-13	0.00000	60973E-13	0.00000	54274E-14	0.00000	49665E-13	0.00000	28176E+00	[0.00,100]	26884E-12	0.00000
•12794E-12		304351-13		.4790ZE-13	4					33375E-12	
<u></u> _8005>E-13	0.00006	283246-13_	0.00000	296416-14_		736902-13	0.00000	223e1E+00	6.00000_	3707oE-LZ	0.00000
122558-12	0.00000	^ .57522E-13	0.0000	69562E-13	0.00000	.43380E-13	0.00000	" =.22361E+00	0.00000		_0.00001 <u>_</u>
						-:11147E-12					
10118E-12	0.00000	68660È-13	0.00000	. 81687E-13,	0.00000	36532E-13	0.00000	.14356E+00		322195-13	0.00000
41545E-13	.0.00000	.13449E-13	_0.0000	40784E-13	0.00000	-28956L-12	. 0.00000	.49469E-01		77977b-13	0.00000
-731715-13	0,00000	19247E-13	0.00000	/0761E-14	0.00000	.29/64E-13	0.00000	49469E-01	0.00000	.11532E-1 <u>2</u>	

NATURAL FREQUENCY= .143130E+04

								D.L.	S. 19	9.2	
TX Real	IX Imag	TY REAL _	TY IMAG	TZ Real	T Z [HAG	RX .	RX IHAG	RY "ƙEAL	IHAG	RZ	I mAG
.15267E-01	0.00000	330706-13	0.00000	.385118-13	0.00000	.16d20E-12	0.00000	.24946E-12	0.00000	3u563t-01	0.0000
-15267E-01	0.00000	50486E-13	0.00000	16922E-13	0.00000	36046E-13	0.00000	▲18443É-12	0.00000	305635-01	<u>0 • 0 0 0 0 0 0</u>
6837>E-01	0.03000	.40364E-13	0.00000	73502E-13	0.00000	630164-13			_	54458L-02	
68375E-01	0.00000	.296751-13	0.00000	.62686E-13	0.00000	.1d831t-13				54958L-02_	
.214708-01	0.00000	21358E-14	, 0°0000	47832È-1J	0.00000					•58591E+00	
-21470E-01					0.00000					2828it+00	
		[51584E-13									
		212256-13									
:-10486E+00	0.00000	42948E-13	0.00000	18000E-13	0.00000	15408E-12	0.00000	15562E-12	0.00000	33274e+00	0.00000
194866+00	0.00000	22306E-13	0.30000	.395808-13	0.00000	238494-13	0.00000	29643E-12	0.00000	33274E.00	<u></u>
10486E+00	0.00000	34667E-13	0.00000	.78240E-14	0.00000	.83593E-13	0.000000	44517E-12	_ 0: 000000	-33274E+00	0.00003
104666+00	0.00000	.93257L-13	-	-68050E-13							
-13650E+00	0-00000	11411E-12	0.00000	.12293E-13	0.00000	132166-12	0.00000	.71613E-12]	. ń . 000 o ó _	.17257L+00	0.00000
•13650E+00	0.00000	.14575E-13	0.00000	138158-12	0.00000	.958758-13	0.00000	-69658E-12	Õ₊000 Õ0	.17257E+00	0.00000
.21470E-01	0.00000	.12720E-12	0.00000	60754Ê-13	-0.00000	24804E-12	.0.00000	26128C-12	0+00000	282816+00	0.00000
.21470E-01	0.90000	108716-12	0.00000	.66812E-13	0.00000	86141E-13	0.00000	24219E-12	0.00000	28281c+00	_0•0000 <u>0</u>
68375E-01	0.00000	.19734E-13	0.0000 <u>0</u>	55625E-13	0.00000	-21406E-12	_ 0:00000_	35346L-12	<u></u>	54958E-02	0.00005
68375E-01	0.00000	.10278E-12	0.00000	-62127E-13	0.00000	548458-13	0.00000	37263E-12	0.00000	54958c-02	_0.00000
.15267E-01	0.00000	12176L-12	0.00000	.81167E-13	0.00000	222536-12	0.00000	.43036E-12	0.00000	.305634-01	0.00000
-15267E-01	0.00000	.47978E-13	0.00000	54418E-L3	0.00000	622626-13	0.00000	.47523E-12	0.00000	.30563e-01	0.00000

NATURAL FREQUENCY= .143337E+04

TX Real	TX IHAG	TY REAL	TY IMAG	TZ REAL	TZ 1HAG	KX Real	RX IMAG	RY REAL	RY T IMAG	REAL	RZ IMAG
•36973L-01	0.00000	.24533L-13	0.00000	96226E-13	0.00000	18913r-12	0.00000	.9827oE-13	0.00000	15501e-01	_ 0.000000
.36973E-G1	0.00000	.110576-12	0.00000	.29950E-13	0.00000	.70128E-13	0.0000	.916056-13	0.00000	`-•15501E-01	
-745908-02	0.00000	13464t-12	6.00000	.7627dE-13	0.00000	.32/59c=13	0.00000	592788-13	0.00000	20409E+00	0.00000
.745538-02	0.00000	600958-13	0.00000.	583495-13	0.00000	223888-13	0.00000	503596-13	0.00000	20409##00	0.00000
•11399E+00	0.00000	191776-13	0.00000	106298-13	0.00000	.505401-13	0.00000	53760E-12	-0.00000	.99866E-01	0.00000
.113792+00	0.00000	.73J00t~15	0.00000	792786-13	0.00000	.7a764E-13	.0.00000	394948-12	0.00000	. 79806E-0 <u>1</u>	_0.00000
.67772E-01	0.00000	.16743c-12	0.03000	285718-13	0.00000	895d3£-13	0.00000	•51512E-12	0.00000	.32161E+00	0.00000
.67792E-01	0.00000	28802E-13	_ 0.00000	.29533E-13	0.00000	15336E-12	0.00000	-4876>E-12	0.00000		
•123oaE+Jo	0.00000	113015-12	0.00000_		0.00000	150132-12	0.00000	.41917E-13	~0.000 <u>0</u> 0		0.60000
.123u8E+u0	0.00000	12025E-13	0.00000.	.365856-13	0.00000	. •319216-13	0.00000	-156540E-14	. 0.00,000	250346-00	0.00000
*12364E+00	0.00000	653386_13	_0.00000]	167048-13	_0.00000	36423E-13	0.00000	816578-12	~.000 uō	25834E+00	0.00000
-12368E+00	0.00000	702118-14	0.00000	93360E-13	_ 0.00000	24509E-14	0.00000	77630E-12	0•000000	25d34E+00	0.00000
10-356229	0.00000	.16312E-12	0.0000	597 <u>88</u> E-13	_000000 <u>.</u>	19624E-İZ	0.00000	83180E12	0.00000	32161£+00	0.00000
67792E-01	0.00000	.25050E-13	0.00000	.108616-12	0.00000	473688-13	0.00000	.87610E-12	0.00000	.32161E+00	0.00000
J11399E+00	0.00000	76897L-13	0.00000]	737366-13	0.00000	257401-12	0.00000	66789E-13	_0.00000		0.000000
.11399E+00	3.00000	.155016-13	0.00000	10012E-13	0.00000	556726-13	0.00000	12518E-12	0.00000	.99800E-01	0.00000
• 74 5908-02	-0.00000	10916t-12	0.00003	.310716-13	0.00000	988746-13	0.00060	099520-12	0.00000	20409E+00	0.00000
.74590E-02	0.00000	632136-13	0.00000	681836-13	0.00000	-16132E-12	0.00000	766388-12	0.00000	2040 #6+00	0.00000
36973E-01	0.00000	•10160C-12	0.00000	66270E-13	0.00000	.265338-12	0.00000	.50272E-12	0.00000	155016-01	0.00000
36973E-01	0.00000	.209545-13	0.00000	.42697E-13	0.00000	~.159>2E-12	0.00000	.57605E-12	0.00000	15501£-01	0.00000

NATURAL PREGUENCY= 1144110E+04

TX REAL	ŠAKI	. TY -	YY IMAG	TZ REAL	TZ IMAG	RX REAL	RK Imag	RY REAL	RY THAG	REAL	RZ'
.76777E-13	0.00000	44315E-13	0.00303	£1253E+30	0.00066	198816+00	0.00000	•35786€-13	. n•00000	59057E-13	0.00000
-77929E-13	`0.00000	-60325E-13	0.00000	.11253E÷00	0.00000	.19891£+00	0.00000	20701E-14	0.00000	~~\$\$490E-13	<u></u>
90207E-13	0.00000	145481-13	0.03000	.41826E-01	0.00000	-22194E+00	0.90900	59723E-13	[0.00000]	28955E-12	0.00000
116658-12	0.00000	65d38£-15	0.00000	418268-01	0.00000	22194E+00	0.00000	27891E-13	0.00000	20712E-12	0.00000
64750E-13	0.00000	.713d7E-13	0.00000	-16215E+00	0.00000	18406£+00	0.00000	85683E-13	. 0.00000	.47910E-12	_0_00000
10181E-12	0.00000	840526-13	0*00000	16215E+00	0.00000	•18406E+00	0.00000	13005E-13	_ 0.00000	.45960E-12_	.0.00000
.22631E-12	0.00000	438068-13	0.00000	18465E+00	0.00000	56097E-01	0.00000		0.00000	.064235-13	000c0.0
.23044E-L2	0.00000	.417236-13	0,0000 <u>0</u>	.18465E+00	ö .0 0000	.56097E-01_	0.00000	752148-14	ŭ•00vô <u>0</u>	.47740E-13	0.00000
-456907E-13	0.00000	55651e-13	9.00000	. #32056-01	0.00000	.22527E+00	0.00000	564358-15	``0.00000°·	53797E-12	, à <u>, cooo</u> ó
:.72824E-13	_0.00000	604676-14	0.00,000	93205E01_	0.00000	22327E+00	0.00000	18107E-13	0.00000	40221 <u>E</u> -12	0.00000
10016E-12	0.00000	160103E-13	0.0000	.93205E-01	0.00000	225274+00	~a_ooooo	~19419E-12			_0.00000
;.16451E-12	_0.00u00 _\	706552-13	`o*00005 ⁻	93205E-01	0.00000	.22527E+00	0.00000	.21466E-13	0.000000	.300296-12	0.0000
-156978-12	0.00000	.32168E-13	0.00000	18465E+00	0.00000	.500975-01	0.00000	- 188596-12	0.00000	167046-12	0.00000
•17374E-12	0.00000	.022616-13	0.00,000	.184658+00	_0.00000	50097E-01	0.00000	65678Ê-13	0.00000		0.00000
7618dE-14	0.00000	105104-12	0.00000	.16215E+00	0,00000	.16406E+00	0.00000	42610E-13	0.00000	51509E-12	0.00000
.210550-14	0.00000	.65857£-13	0.00000	162156+00	0.00000	18406E+00	0.00000	-13672E-12	.0.00000	2741dE-12	0.00000
-652368-13	0.00000	.40129E-13	0.00000	. 418266-01	0.00000	221946+00	000000	13272E-13		-91139E-13	0.00000
112726-12	0.0000	114946-12	0.00000	418265-01	0.00000	.22194E+00	0.00000	123326-12	0.00000	.66974E-13	0.00000
81935E-14	3.00000	•11245E-12	0.00000	11253E+00	U.00000	1/8811+00	0.00000	-33022E-13	0.00000	•11721E-13	0.00000
.44287E-13	0-00000	22257E-13	0.00000	.11253E+00°	0.00000	198816+00	0.00000	.82414E-13	0.00000	.93592E-13	0.00000

TX - Real -	TX IMAG .	KEVE LA	YT OAHI	TZ Real .	TZ 1HAG	RX RX RY RY KZ RZ REAL IMAG REAL IMAG KEAL IMAG
•072358-01	0.00000	.12667E-13	0.00000	.94200E-13	0.00000	.12207E-12 0.0000011119E+00 0.0000094709E-01 0.00000
672356-01	0.00000	13467E-12	0.00000	6561dE-13	0.00000	40723k-13 0.00000 [11119E+00 0.00000 .94709k-01 0.00000]
824026-01	0.00000	646731-14	0.00000	578/7=-13	0.00000	.74729£-13 0.00000 .17511E+00 0.00000 .10197E+00 0.00000
.82402E-01	0.00000	•57004E-13	0.00000	.60160E-13	0.00000	.1/410E-12 0.00000 .17511E+00 0.0000010197E+00 0.00000
. +214636-01	0.00000	.20172E-13	0*00000	69419E-14	0.00000	.3/805E-13 0.0000058977E-01 0.0000025140E+00 0.00000
214638-01	0.00040	.292456-14	0.00000	.11042E-13	0.00000	74945E-13 0.0000058977E-01 0.0000025140E+00 0.00000
25579E-01	0.00000	641691-14	0.00000	53891E-13	_0 <u>,</u> 00000	24093E-13 0.0000099195E-u1 0.00000 .20313E+00 0.00000
25679E-01	0.00000	.85641L-14	0.00000	221010-13	0.00000	.10070L-12 0.0000099195E-01 0.0000020313E+00 0.0000
66741E-01	0.00000	.43017E-15	0.00000	74934E-13	0.00000	.435526-13 0.0000021750E+00 0.0000095687E-01 0.00000
.66741E-01	000000	150621-13	0.00000	.379946-13	0.00000	5JJ00L-14 0.00000 .21750E+60 0.00000 .95687E-01 0.00000
-667415-01	0.00000	21140E-13	0.00000	.72703E-13	0 • 00 000	.43104E-13 0.0000021750E+00 0.0000095687E-01 0.0000
66741E-01	0.00000	553376-14	0.00000	11516E-13	0.00000	.52278E-13 0.0000021750E+00 0.00000 -95687E-01 0.00000
25679E-01	0.00000	'18401L-13	0.00000		0,00000	18049E-15 0.00000 .99195E-01 0.00000 .20313E+00 0.00000
25679E-01	0.00000	,28942E-14	_0.00000	.62705E-14	0.00000	.10010E-12 0.00000 399195E-01 0.0000020313E+00 0.00000
21463E-01	0.00000	.58251E-13	0.00000	- 12786E-13	. 0.00000	.44323E-13 0.00000 .58977E-01 0.0000025140c+00 0.00000
-21463E-01	0.00000	~.21410E=13		-2162786-13	0.00000	11645E-12 0.00000 .58977E-01 0.00000 .25140E+00 0.00000
82402E-01	9 * 00 n 0 Å	11321E-13	0.00000	98935E-14	u <u>.</u> 00000	.65533E-14 0.0000017511E+00 0.00000 .10197E+00 0.00000
82402E-01	0.00000	46329E-14	0.00000	-1525376-14	0.00000	.11558E-12 0.0000017511E+00 0.0000010197E+00 0.00000
67235E-01	0.00000	, •30356E-14	0.00000	10982E-13	0.00000	.15d60e-13 0.00000 .11119E+00 v.0000094709E-01 0.00000
+67235E-01	J. 00000	31612E-14	0.00000	20173E-15	0.00000	18679E-13 0.00000 .11119E+00 0.00000 .94709E-01 0.00000

NATURAL FREQUENCY= -146027E+04

TX REAL	TX IMAG	TY KEAL	TY Imag	TZ REAL	" TZ I MAG	RX REAL	RX 1HAG _	RY REAL	RÝ THAG	RZ RZ
-14632E-13	0.00000	.10075E+00	0.00000	17045E-01	0.00000	.24343E+00	0.00000	32610E-13	0.00000	. 249336-13 0.00000
-14240E~13	0.00000	10875L+00	0.00000	.17045E-01	`_o`.oooo`	24343L+00	,0•00000		_0.00000	249446-13 0.00000
.15453E-13	0.00000	.729654-01	0.00000	116u5L-02	0.00000	134276+00	0.00000	•35108E-13	`0.00000 °	.29340E-13-0.00000
₹72996E-14	0.00000	72965E-01	0:00000	11665E-02	0.00000	1342/2+00	0.00000	185171-13	0.00000	.54648=-13 0.00000
.55319E-14	0.00000	10351E+00	0.00000	.194305-01	0.00000	.273526+00	0.00000	.66255E-13	0.00000	15653e-13 0.00000
-327696-13	0.00000	.18351E+00	0.00000	-19430E-01	0.00000	.27352E+00	0.00000	10453E-ĻŠ	0.00200	25453E-L3 0.000000
~25303E-13	_0.00000	.720656-01	0.00000	82792E_01	0.00000	11189E+00	0.00000_	<u>-</u> 9 <u>716</u> 9E-13	0• jōnō aō_	83274E-13 0.00000
54477E-13	0.00000	726u5£-01	0.00000	82792E-01	0.00000	111895+00	0.00000	<u>4</u> 92016-13	0.00000	24687E-13 0.00000
-71243E-14	0.00000	T12348E+00	0.00000	.47484E-01	0.0000	11266E+00	0.00000	: [428] 6-13	0.00000	. 823898-13 0.00000
-24421E-14	0.00000	123486 +00	0.00000	.474846-01	~0.0000	11266E+00	0.00000	649895-14	~ ń• oóo oò .	10646E-12 0.00000
774321E-14	0.00000	12348E+00	0.00000			*11266E+00	0.00000	.31278E-13	0.00000	179776-12 0.00000
-1442 3E-13	0.00000	12348 <u>E`+</u> 00_	0.00000	47484E-01	0.00000	. £156ef +00	0.0000		0.00000	59980L-13 0.00000
60176E-13	0.00000	72665c-01	0.00000	027926-01	0.00000	11193F+00	0.00000	53800E-13	0.000000_	11073E-13 0.00005
83587E-13	0.00000	726656-01		827928-01	_Ü_00000	11189E+00	0*00000	76696 <u>E</u> -13	0.00000	42607E-13 0.00000
~15107E-14	0.00000	18351E+00	``0.00000	19430E-01	_0.00000	27352±+00	_0.00000	8Ó <u>8</u> 12E-13	0.00000	-22521E-12 0.00000
~33796E~13	~~o.ooooo	18351E+00	000000	.19430E-01	~ 0.00000	~ = 27352E+00	0.0000	.338566-13	0.00000	152346-12 0.00000
-30021E-13	0.00000	72965L-01	0.00000	116651-02		13427E+00	. 0.00000	,96725E-14	0.00000_	196192-12 0.00003
-5Z208E-13	0,00000	.729651-01	0.00000	11665E-0Z	u.00000	·134276+00	-0.00000	. 85602E-14	0.00000_	65631E-13 0.00000
.53404£-14	0.00000	10875L÷00	0.0000	-170456-01	~~o.oooō	243436+00	0.00000	56400E-13	0.00000_	.29170E-13 0.00000
-:793278-13	_0.00000	.10d75E+00	0.00000	1/045E-01	0.,00000	24J43E+00	0.00000	,19252E-13	0.02000	73259E_130.03000

TX IX TY TY TZ TZ RX RX RY RY RZ RZ RZ REAL IMAG REAL IMAG REAL IMAG REAL IMAG
.50273E-01 0.0000016365C-12 0.0000016348E-13 0.0000037741E-13 0.0000077216E-01 0.0000061399E-01 0.00000
50273E-01 0.0000057630E-13 0.0000042470E-13 0.0000011924E-12 0.0000077216E-01 0.00000 .61399E-01 0.00000
64602E-01 0.00000 .23723E-12 0.00000 .39434L-14 0.0000011422E-12 0.00000 .14377E+00 0.00000 .36350E-01 0.00000
.64602E-31 3.00000 .12302E-12 0.00000 .44872E-13 0.0000022039E-13 0.00000 .14377E+00 0.0000036350E-01 0.00000
-43237E-01 0.00000 1.12941E-14 0.00000 .10713E-13 0.00000 .45589E-13 0.0000013251E+00 0.0000019340E+00 0.00000
43237E-01 0.00000 .21999E-13 0.00000 .25676E-13 0.0000060145E-14 0.0000013251E+00 0.0000019340E-00 0.00000
36589E-01 0.0000025004E-12 0.00000 -63372E-13 0.00000 32719E-13 0.00000 .97757E-01 0.00000 23587E+00 0.00000
.36589E-01 0.0000017158E-12 0.0000023346E-13 0.00000 .10184E-12 0.00000 .97757E-01 0.0000023587E-00 0.00000
.76500E-02 0.00000 .18266C-12 0.0000011207E-12 0.0000027654E-13 0.0000031804E-01 0.0000029878E.00 0.00000
76800E-02 0.00000 12023E-12 0.00000 13127E-13 0.0000085494E-14 0.0000031804E-01 0.00000 .295784900 0.00000
-76800E-02 0.00000 -12517E-12 0.00000 -11768E-12 0.00000 -10584E-12 0.00000 -31804E-01 0.00000 -29878E-00 0.00000
76ac0E-U2 0.00000 `.12292E-12 "0.00000 ".35446E-14 0.00000 ".13950E-14 0.0000031804E-01 0.0000029878L400 0.00000
36549E-01 0.0000025139E+12 0.0000087899E-13 0.0000052394L-13 0.0000097757E-01 0.0000023587E+00 0.00000
.36589E-01 0.0000018623E-12 0.0000027765E-13 0.00000 .165276-12 0.00000 .97757E-01 C.00000 .23587E-00 0.00000
.43237E-01 '0.00000' 180015E-14 G.CO000" 14522E-13 0.00000 ".51568E-13 0.0000013251E+00 0.00000 19340E+00 0.00000
43237E-01 0.0000071458E-13 0.00000 .14662E-13 0.00000 -:15422t-12 0.0000013251E+60 0.0000019340c+00 0.00000
6460ZE-01 0.00000227576-12 0.00000744936-13 0.0000074029E-13 0.0000014377E+00 0.0000036350E-01 0.00000
.64602E-01 0.00000 .21189E-12 0.00000 -84338E-13 0.00000 .66102E-13 0.00000 .14377E-00 0.00000 .36350E-01 0.00000
-50273E-01 0.0000011798E-12 0.0000065745E-13 0.00000 .63248E-13 0.000007721cE-01 0.00000 .61399E-01 0.090005
50273E-01 0.0000011899E-12 0.00000 .75266E-13 0.0000011318E-12 0.0000077216E-01 0.0000061399E-01 0.00000

		NATURAL	- FRLOUENC	Y= ,.150975	E+U4		- , -				
TX REAL	TX IMAG	TY REAL TO	TY :	TZ REAL	TZ IHAG	RX REAL	RX IMAG	RY	KY	REAL.	RZ THĀĞ
-35725E-13				28110E-11	0.00000	462206-11		122926-13	0,00000	.69290E-13	0.00000
~.50361E-14	0.00000	18587L+00	0.00006	277466-11	3.00000°	40106E-11		44509E-13	<u>_0</u> ,00000	/3431 ₅ -13	0,00000
•57017E-13	0.00000 -	.300758+00	0.00000	-26216E-11	0.00000	.45073E-11	0.00000	124826-13	0.00000		0.00000
25991E-13	0.00000 -	.300756+00	0.00000	27652E-11	0.00000	42495b-11	0.00000	.303355-13	[0.00000]	61393 <u>E-13</u>	0.00000
-28095E-13	0.00000	.191938-12	0.00000	.59454E-12	0.00000	75443£-11	0.00000	700926-13	~0.00000 ~	357916-13	0.00000
29614E-1J	0.00000 -	.45380E- <u>1</u> 2	0.00000_	38836E-12	0.00000	.60774L-11	0.00000	76962E-13	[0.00000]	- <u>.</u> 81315 <u>-</u> -13	0.00000
16235E-13	0.00000	.30075L+00	0.00000_	22852E-11.	0.00000	54549E-11	, 0. 00000 ,	•92332E-13	0.00000	44565t-13	0.00009
.30055E~13	0.00000	.30075E+00	ô.0000u,	245246-11	0.00000	300006-11	0.00000	.±94252E-13		20279E-12	0.00000
-,583076-13	0.00000 ~	. เีย็รฮ7ีะ+00 ู	0.00000 <u></u>	37103E-11	0.000000	26272E-11	0.00000	11464E-13	0.00000	11873=-12	0.00000
68207E-13	0.00000	.185876-00	0.00000	41925E-11	0.00000	170636-11	0.00000_	.33,1136-13	_0*00000	.114706 <u>-1</u> 2	0.00000
250076-13	0.00000 -	.13587E+00	0.00000	-;37767Ê-1Î	0,00000	22874E-11	0.00000	57924E-13	[0.00000]		0.00000
217056-13	0.00000 -	. 18587E+00		-41870E-11	0.00000	•17979E-11	0.00000	-141757E-13	.0.00000	.7 <u>5</u> 129 <u>E-1</u> 3	0.00000
•48353E-13	0.00000	.39075E+00	[0.00000]	23862E+L1_	0.00000	.51016E-11	0.00000	307641-13	0.00000	52597E-13	0.00000
.33971E-13	0.00000	.39075.+00	0.00000	24912E-11	0.00000	39546E-11	0.00000	211308-13	0.00000	59192=-14	0.00000
21053E-13	0.00000	. 29182E-12	.o.vooo	<u>-</u> _635538-12	0.00000	72825L-11	0.00000	471258-13	_0.00000	452916-113	0.00000
34107E-13	0.00000	. 15762L-12	0.00000	.45036E-12	00000°	.62748E-11	- 6. 50 0 o o	275868-13	0.00000	118958-12	0.00000
14409E-13	0.90000	.30075E+00	0.00000	25671E-11	0.00000	.448748-11	0.00000	.20385E-13	ს.იმიაი "	.92727E-13	
7.36170E-13	0.00000 ~~	.30075£+00	0.00000_		0.00000	42814E-11	0.00000	56545E-13	_ 0 <u>. 0</u> 000 <u>00</u>		0.00000
167746-13	0.00000	.18587E, <u>:</u> 00	0.00000,	.278125-11	0.00000	44707t-11	0.00000	12410E-13	0.00000	.30109£-15	0.00000
.26533E-13	0.00000	.1d5d7L+00	0.00000	27599E-11	0.00000	.40342E-11	0.00000	18152E-13	0.00000	.26658c-13	_0.00000

NATURAL FREQUENCY= .151316E+04

TX REAL .	TX IHAG	TY ⊀EAL	TY IMAG	TZ REAL	TZ IHAG	K X K X	RX IMAG	RY . REAL	YS	KEAL T	RZ
685776-13	0.00000	-32185t-11	0.00000	.11712E+00	0.00000	.17968L+00	0.00000	.41348E-13	0.00000	.77714b-13	_0.00005
-81243E-13	0.00000	.54191E-11	0.00000	11712E+00	0.00000	17968E+00	0.00000	-10863E-12		943376-13	
.34310E-13	0.99000	-,677198-11	0.00000	11115E+00	0.00000	18471E+00	0.00000	519178-13	0.00000	.15350e-13	0.00000
~54622E-13	0.00000	706798-11	0.00000	.11115£+00	0.00000	.18471E+00	0.00000	89012E-13	U.00000	50694c-13	0.00000
45737E-13	0.00000	-143,146-11	0.00000	21642E-01	0.00000	.28560(+00	0.00000	.15331E-12	0.00000	.25670=-12	0.00300
-543776-13	0.00000	14074L-11	0.00000	.21642E-01	0.00000	28560£+00	0.00000	.81302E-13	0.00000	192176-12	0.00000
.22536E-14	0.00000	•51310E-11	0.00000	+10043E+00	0.00000	19340E+00	0.00000	42400E-15	0.00000	14517E-12	0.00000
48897E-14	0.00000	.89807E-11	0.00000	10943 <u>E</u> +00	0.00000	.19340E+00	0.00000	19085E-i3_	0.00000		0.00000
24079E-14	0.00000	3/8826-11	0.00000	16594E+00	0.00000	.88775E-01	0.00000	~.9104LE-13	0.00000	290185-12	<u>_0</u> . 29/00 7_
25311E-13	u.00000	48850E-11	0.00000	.16594E+00	0.00000	885756-01	0.00000	55696C-13			<u></u>
90110E-14	0.00000	27268E-11	0.00000	.16594È+00	0.00000	.88575Ē-01	0.00000	.102508-12	0.00000	~57 <i>29</i> 9 ₂ -13	0.00000
4466 3E-1 3	0.00000	59593E-11	0.00000	16594E+06	0.00000	88575E-01	0.00000	•95664E-13		.22450c-13	0.00000
25507E-13	0.00000	44039£-11	0.00000	10043E+00	0.00000	173406+00	~ o.ooooo	31537E-13	0.00000	.42310t-13	0.00000
33851E-13	_0.0000oj	•95946E-11	ğ.0000 <u>2</u>		_o.oooo	19340[+00]	_0.00 <u>0</u> 00 <u>.</u>		0.00000	20595E-12	0.0000
35076E-13	0.00000	.15066E-11	0.00000		`douco.ŭ `	.542999=	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~			5388L- <u>13</u>	0.00000
30344E-13	0.00000	15309L-11	0.00000	216426-01	0.00000	205606+00	0.00000	5894/E-13	0.00000	1140s£-12	0.00000
14861E-13	0.00000	68161E-11	0.00000	.11115E+00	0.00000	18471E+00_	_0 • 000 <u>00</u>	>8602E-14	<u> </u>	63 <u>535</u> t-13	0.00000
60355E-13	0.00000	~.71840Ē-11	0.00000	11115E+00	0.00000	.18471E+00	0.00000	351728-13	0.00000		_ <u>0</u> .00 <u>000</u> _
.4674dE-LJ	0.00000	.307931-11	9.00000	11712E+00	0.00000	417968E+00	0.60000	=151605E-13	0.00000	=.30793E-13	_0.00000
•35990E-14	0.09000	.5>2856-11	0.00000	.11712E+00	0.00000	17968E+00	0.00000	71804E-13	0.00000	• 78 346c - 13	0.00000

RX RX RY RY RY RZ RZ RZ RZ IHAG REAL IHAG REAL IHAG TX TX TY TY TZ TZ

REAL IMAG KEAL IMAG REAL IMAG --16652E-13 0.00000 --87521E-01 0.00000 --65868E-02 0.00000 --11556E+00 0.00000 -12482E-13 0.00000 -19392E-13 0.00003 -.19029E-13 0.00000 .87521E-01 0.00000 -.65860E-02 0.00000 -.11556E+00 0.00000 .21780E-14 0.00000 .82075E-14 0.00000 .34198E-13 0.00000 .97171E-02 0.00000 -.28685E-01 0.00000 .43752E-01 0.00000 -.40107E-13 0.00000 -.623436-13 0.00000 .407526-01 0.00000 -.485096-13 0.00000 -.71383E-13 0.00000 -31733E-14 0.00000 -.97171E-02 0.00000 -.28685E-01 0.00000 -.25051L+00 0.00000 -.63622E-13 0.00000 -.67277E-13 0.00000 --255b08-14 0.00000 ".11461E+00 0.00000 -43830E-01 0.00000 0.00000 -.11461E+00 0.00000 .43830e-01 0.00000 -.25051E+00 0.00000 .39894£-13 0.00000 -.82064E-13 0.00005 .30144E+00 0.00000 1.10177E-12 0.00000 -.67522E-13 0.00000 -.35891E-13 0.00000 -.17342E+00 0.00000 -.26675E-01 0.00000 -. ZZ39ZE-13 0.00000 .1734ZE:00 0.00000 .. Z6675E-01 0.00000 .. 30184E+00 0.00000 .. 37076E-13 0.00000 .. 21037E-12 0.00000 -.14u26E+00 0.00000 -.67921E-13 0.00000 -.60753E-13 0.00000 .559186-13 0.00000 .82055E-01 0.00000 -.93702E-01 0.00000 -.82055E-01 0.00000 -.93702E-01 0.00000 -.14026E+00 0.00000 17491E-13 0.00000 12637E-12 0.00000 0.00000 -28380E-13 -.14026L+00 0.00000 .26715E-13 0.00000 -.23991E-12 0.00000 .82055L-01 0.00000 -93702E-01 0.00000 --316625-13 0.00000 .64391L-13 0.00000 .611835-13 0.00000 --.82055E-01 0.00000 -.93702E-01 0.00000 --14026E+00 0.00000 0.00000 .26354E-14 0.00000 .30029E-13 0.00000 .301841+00 0.00000 -.17342E+00 0.00000 --.26675E-01 0.00000 0.00000 .17342E+00 0.00000 -.26675E-01 0.00000 .30184E+00 0.00000 -.60809E-13 0.00000 .22666E-12 0.00000 0.00000 -11461E+00 0.00000 -.43830E-01 0.00000 -.25051E+00 0.00000 -.61104E-15 0.00000 .42753E-13 0.00000 .58662E-13 0.00000 .14130E-12 0.00003 0.00000 -.114616+00 0.00000 -.43830E-01 0.00000 -.250516+00 0.00000 .40752E-01 0.00000 --17716E-13 0.00000 --23402E-12 0.00000 .97171L-02 0.00000 .28685E-01 0.00000 0.00000 -14529E-13 .28685E-01 0.00000 .40752E-01 0.00000 -.48577E-13 0.00000 -.37418E-13 0.00000 -.9/1714-02 0.00000 .12793E-13 0.00000 .6580dE-02 0.00000 -.11556E+00 0.00000 .67296E-14 0.00000 .703926-14 0.00000 -.87521c-01 0.00000 0.00000 .65868E-02 0.00000 -.11556E+00 0.00000 -.60842E-14 0.00000 -.63607E-13 0.00000 -.10294E-13 0.00000 .87>21L-01 0.00000

NATUKAL FREDDENCY*

.151740E+04

NATURAL FREQUENCY= .152918E+04

TK REAL	TX TY REAL T	TY I HAG	TZ Real, "	IZ IHAG	KX KEAL	RX I HAG	RY REAL	"IHAG"	REAL	RZ IMAG
.37640E-13	0.0000014757E-01						.259698-13			
46993E-13	0.00000 .147576-01	0.00000	.695548-02	0.00000	.495712-02	0.00000	73729€-13	0.00000	~. 24865E <u>~</u>]13	0.0000
.496538-13	0.00000 .18401E-01	0.00000	29677E-01	0.00000	.14941E-01	0.0000	37649E-13	0.00000 -	192545-12	0.00000
34360E-13	0.0000018401E-01	0.00000	29677E-01	0.00000	.14941E-01	0.00000	26950E-13	'0.0000ò"	.Z4422E-12	0.00000
.545986-13	0.00000 .24173E-01	0.00000	.536758-01	0.00000	11626E+00	0.00000	13168E-12	` 0.00 000 ~	151796-12	_0.00000
61228E-13	0.0000024173£-01	0.00000	.53675E-01	0.60000	116266+00	0.00000	40306E-13	0.00000	.19396E-12	_0,00000
.51934E-14	0.00000958416-01	0.00000	53365E-01	0.00000	-26080E+00	0.00000	.40052E-13	0.00000	26074L-12	0.00000
365755-14	0.00000 .958418-01	0.00000	533656-01	_0.000000	26080E+00	0.0000	43891E-13		.30399E-12	0.00000
.427575-13	0.00000 .150582+00	0.00000	.22411L-01	0.00000	367171+00	0.00000	46470E~14	0.00000	330ab <u>k</u> _12	
13449E-13	0.00000150580+00	0.00000	.22411L-01	_0.00000	36717E+00	0.00000	55002E-13	_0.00000	.36538E-12	0.00000
.75118E-14	0.0000015058E+00	0.00000,	[22411E-01"		36717E+00	0.00000	.33244E-13	"o. 00 g ďô "	37188E-12	
.30673E-14	. 0.00000	_ 0.00000		0.00000	30717£+00	0.00000	47677E-13		.29952E-12	0.0000
229576-13	10.00000	0.00000	533656-01	70.00000	26080E+00	00000	-•32569L-1]3		2075=-12	0.00000
	[0.00000]9584it-01									
~,21614E-13°	0.0000024173E-01	~ o: ōơnoō~	\$3675E-01		-11626£¥00	.000000	-63769E-13	_0.00000 <u>_</u>	16673E-1	0.00000
•717J7E-13	0.00000 .24173£-01	0.00000	. >3675E-01	0.00000	.11626E+00	0.00000	.76307E-13	0.00000	.24890E-1	0.00000
	0.00000164016-01									
~.10234E-13	0.00000184016-01		- .29677E=31	000000	149416-01	00000.0	31739E-14	0.00000	. 237596-1	50.00000_
44998E-13	0.00000 .147575-01	0,00000	.69554E-92	0.00,000	49571E-02	0.00000	- 1453dE-13	0.0000	-93911E-17	7 ~ 0.00000
-396738-13	0.00000147576-01	0.00000	.695548-02	0.00000	495716-02	0.00000	15038E-13	0.00000	.16297E-1	3 0.00000

NATURAL FREQUENCY= .153048E+04

TX REAL	TX IHAG	TY ⊰ēAL	TY [mag	T.Z. Real	T Z I MAG	4EAL XX	AF DAKI	RY Real	RY Ihag	REAL IMAG
.46497E-01	U+00000	324666-13	0.90000	.37062E-13	0.00000	.32079E-13	0.00000	334168-01	0.00000	96993L-02 0.0000 <u>0</u>
-46497E01	0.00000	51476E-13	0.00000	903616-13	0.00000	572956-13	0.00000	33416E-01	0.00000	
.24817E-01	0.00000	102476-13	0.00000	.36222E-13	0.00000	.104042-13	0.00000	15475&-02	0.00000	18734L+00 0.00000
-248178-01	0.00000	.40582t-15	0.00000	.591078-13	0.00000	157428-12	0.00000	15475E-02	0.00000	.187348+00 0.00000
.33860É-01	0.00000	30409E-13	0.00000	11274E-12	0.00000	.890658-13	0.00000	35262E-01	0.00000	18975-+00 0-00000
-33860E-01	0.00000	.24123E-13	0.00000	174616-13	0.00000	.84247t-13	0.00000	35262E-01	ō•00000	13975=+000.00000
.96133E-02	0.00000	.24718b-13	0.00000	.34455E-13	0.00060	142498-12	0.00000	.96385E-02	0.00000	291496+00 0.000000
-96133E-02	0.09000	720126-13	0.00000	.237102-13	0.00000	124976-12	0.00000	.96385E-02	0.00000	.291436+00_0.03000
-12679E-01	0.00000	48152E-13	_0.000001	37021E-13	0.00000	-13450E-12	0.00000	227748-01	ğ. 00000	295386+00_0.00000
-12679E-01	0.00000	.8d485E-13	0.00000	.235298-13	.0.00000	•19393E-12	0.00000	22774E-01	ō• 0ò0 oŏ	.295388+00 0.00000
.12679E-01	0.00000	.56720É~13	0.00000	13430E-13	0.00000	26393E-12	0.00000	.22774E-01,	0.00000	29534E+00 <u>0.00000</u>
.12679E-01	0.00000	406846-13	~o.u0ooo~	30449E-13	_0.00000	147748-12	0.00000	-22774E-01	. 0 • 0 0 0 0 0 0	.2953at+00 0.00000
96133E-02	0.00000	3 <u>î</u> 7896-î3	0.00000	-65964Ê-14		.11035c-12	0.00000	96385E-02	0.00 <u>0</u> 00	29148E+00 10.0000V
.96133E-02	0.00000	.281816-13	0.00000	•32295E-13	0.00000	.107186-12	0.00000	96385E-02	.0.00000	.291486+00 0.00000
-33800F-01	0.00000	42858£_13_	_0.00,000	_d8d7bE-14	0.00000	10201t-12	0.00000	.35262E-01	0.00000	189756+00 0.00000
-3386GE-01	0.00000	12140£-13	"o.00000 ⁻	- <u>-</u> 14483c-13	0.00000	177066-13	0.00000	-352626-01	0.00000	.14975c+00 0.00000
2481 }E-01	0.00000	18074£-13	0.00000_	13308L-13	0.00000	. +811096-13	0.00000	.15475E-02	0.00000	18734E+00 0.00000
+24813E-01	0.00000	.78450E-14	0.00000	499436-13	0.00000	.14703t-12	0.00000	-154758-02	0.00000	.10734E+00 0.000000
-46497E-01	0.00000	.22898E-13	0.00000_	`42,103E-14	.ó•00000		0.00000	33410£-01		96998E-02 _0.03000
-46497E-01	0.00000	2/7576-13	0.00000	64952E-L3	0.00000	.108130-12	0.00000	.334166-01	0.000,00	

NATURAL FELOUENCY= .155597E+04

TX REAL	TX IMAG -	TY "KEAL	TY IHAG	TZ REAL	. TZ IMAG	RX KEAL	RK Imag	RY	RY	RZ	IHAG
.90473E-01	0.00000	_24000E-14	0.00000	.46943E-13	0.00000	.4d564E-13	0.00000	.66668E-01	0.00000	35687E-01	0.00000
.90473E-01	0.00000	14545L-14"	0.00000	69895E-14	ŭ.a o 0000	.17594E-13	0.00000	10-360086-01	0.00000	35687E-01	<u>0</u> .000 <u>0</u> 0
-73501E-02	0.00000	73917E-13	0.00000	43952L-14	0.00000	.48405c-13 ·	0.00000	21679E-01_	0.00000	3%q53₽∓00	0.00000
.73501E-02	0.00000	67J73E-14	0.00000	42976L-13	0.00000	.72027t-13	0.00000	21675E-0i	0.00000	32 8236+00	0.00000
937266-02	0.00000	.238356-13	0.00000	~.55090E-13	0.00000	670561-13	0.00000	.27474E-01	0.00000	-21133E+00	0.00000
•9372±E=02	0.00000	.752685-14,	0.00000	159>85-13	0.00000	/40956-13	0.00000	.27474E-01	0.00000	-,-21133E+00_	o.0000j
.48714E-U1	0.00000	.168136-13	0.00000	.3/778E-13	0.00000	.198816-13	0.00000	42362E-01	0.00000	.273305+00	0.000055
487148-01	0.00000	.17701L-13	0.00000	27021E-13	0.00000	.88721E-i4	0.00000	42362E-01	`ŋ•'öəɔʻoo	273301.+00	
.58482E-01	`J.00000					461836-13					
-+58482E-u1	0.00000	.20973E-13	0.00000	16805E-13	0.00000	184826-13	0.00000	.3.30105E-01	0.00000	31877E-01	0.00000
.58482E-01	0.00000					40752E-13					
58482E-01	0.00000	12319±-13	อั•อาออ๋า	<u>22</u> 353E-14	0.00000	87694E-13	0.00000	30105E-01	0.06200	.31877E-01	. 0. 00000
.48714E-JI	6.00000	183956-13	0.00000	.25525E-14	0.00000	538/0E-13	0.00000	42362E-01	_0•00n\00_	273306+00	0.00000
48714E-01	0.00000	.124456-13	0.0000	21512E-14	. 0.00000	51115E-13	0.00000	42362E-01	0.00000	•27330E+00	0.0000
937268-02	0.00000	`.22217L-13	0.00000	88637E-14	`0.00000	.22d64d-14	0.00000	.27474E-01	0.00000	211336+00	0.00000
.93726E-02	0.00000	.398376-13	0,00003	.34676E-13	0.00000	516336-14	0.00000	27474E-01	0.00500	21133E+00	0.00000
73501E-02	้ง • จ์จึงคอ_ี	53440E-13	, o • o o o o o o	13467 <u>E</u> -13	្តីប្តីភ្នំ ចំពុល្ល	742626-13	<u>, ō</u> •00000	216758-01	00000	<u>3</u> 2833 <u>E</u> .00	0.00000
.73501E-02	00000.	60161E-13	0.00000	94772E-14	~ა.იითი	110426-12	ე. ეეიბე	21675E-01	0.000.00	-32823E+00	0.00000
904738-01	0.00000	.128381-13	9.00000	.u0114E-14	0.00060	.24802E-15	0.00000	.66668E-01	0.00000	356876-01	0.00000
90473E-01	0.00000	.44959E-13	_0•0000¢	31428E-13	u.qoooo	10422E-13	_o.ooooo	•66668E-01	0.00000	35687601_	0.00000

NATURAL FREQUENCY= .157931E+04

TX	IX IHAG	- TY	YY	TZ REAL	TZ I MAG	, R.K KLAL	RX IHAG	. RY REAL	KY .	REAL THAG
723246-14	0.00000	-19912E-12	0.00000	.10382E+00	0.00000	.13253E+00	0.00000	49796E-13	0.00000	.40017t-13 0.00000
24766E-13	6.00000	11666E-12	0.00000	10382E+00	0.00000	13253E+00	0.00000	27B59E-13	`` 0. 00000	.27885E-14 0.00000
.25444E-13	0.00000	160958-12	0.00000	12775E+00	0.00000	92391E-01	0.00000	.22559£-13	0.00000	12835E-12 [0.00000"
367718-13	0.00000	146121-13	0.00000	.127758+00	0.00000	.923918-01	0.00000	•12679E-13	0.00000	42886E-14[0.00000]
137686-13	0.00000	•17404E-14	0.00000	.77042E-01	0.00000	.234568+00	0.00000	.2733JE-13	0.00000	587486-13 [0.00000
•170938-13	0.00000	.10d5dL-13	0.00000	77042E-01	0.00000	23456E+00	0.00000	.28811E-13	0.00000	20276E-12 _0.00000
223648-13	J.00000	.10277e-12	0.00000	64996E-01	0.00000	23760L+00	0.00000	18971E-13	0.00000	.31726 <u>-13 0.00</u> 900
-22326E-13	0.00000	.89153E-13	6.00000_	•64996 <u>C</u> -01	0.00000	.23760L+00	0.00000	43275E-14	0.00000	
-16870E-13	0.00000	1J708c-13	0.00000	.118alL-01	0.00000	.2dJ38E+00	0.00000	.40016E-14	0.00000	44433E-131 0.00000
-56600E-13	0.00000	831221-13	0.00000	11881E-01	0.0000	28338L+ÖÖ	0.0000	28674E-13		.12d04E-13 0.00000
57109E-13	õ.00000	84063E-13	[0.60600	118 ₈ 1E_01	00000	20338E+00	``0.0000	~,67103E-13	`0* 00.0000	. 23769E-13 0.00000
-48490E-13		.91595E-14	ີ່ (ຄໍ ພວວວຍື	i1881E-01	00 Bno. 0	.28338E+00	0.00000	-94705E-13	_ 0.000000	25429E-12 0.00000
502846-13	6.00000	.97196E-13	0.00000	64996E-01	0.00000	-23760£+0 <u>0</u>	0.00000	58040E-14	0.00000	1d1996-13 0.00000
40820E-13	_0,00000	37256E-13		.64996E-01	0.00000	23760E+00	0,00000_	1230gE-13		382346-15 0.00000
45928E-13	~0.00000	110191-12	0.00000	.77042E-01	0.00000	23456£ • 00	~o.აიიბბ	55808E-13	_0:00000	.21194E-12 0.0000J
958128-14	0.00000	12953:-12	0.00000	·77042E-01	0.00000	.234562+00	0.00000	33391£-13	0,00000	57176E-13 0.00000 <u>0</u>
25749E-13	0.00000	25083E-12	_0.00000	12775E+00	_0.00000	92391E-01	'0.0000 <u>0</u>	32610E-14		154 125-12 0.00000
49050E-14	``ō•nouco	-17118E-12	0.00005	" 127 <i>1</i> 5É+00"	0.00000	92391E-0i	0.00000	.33843E-14		.59556E-15 _0.00000
652176-14	0,00000	.62306c-12	0.00000	.103d2E+00	0.00000	132538+00	0.00000	18949[-13	. 0.00000	214481-14 0.000005
520241-14	3.00000	544586-12	0.00000	10382E+00	_0.00000	.13253£+00	0.00000	12175E-13	,ŏ•00ōòō	12305E-13 0.0300 <u>0</u>

TX	TX IHAG	TY	TY IMAG	TZ REAL	TZ Inaĝ	RX	RX I MAG	RY REAL	RY IHAĞ	RÉAL	
-•12895E+00		10112E12									
.12895E+00	0.00000	14050E-12	ี้อั•องออัย	-69733E-12	0.00000		~~02aaaaa	- 11096E+00	0.00000	915016-01	0.00000
-96196E-01	,ò.000u0	10718E-12	0.00000	. +815356-12	0.00000	.90372m-12	0.00000	12843E+00	0.00000	.321788+00	o* <u>.</u> goooji_
-196196E-01	J.00700	13329E-13	0.00000	d3453E-12	0.00000	4u383E-12	0.00000	12843E+00	0.00១១០	32178£.00	0.00000
*50637E-02	0.00000	-72362E-13	0.00000	~50347E-12	0.00000	16360b-11	0.00000	•66254E-01	0.00000		0.00n00
50639E-02	0.00000	.37418E-13	0.00000	.45473E-12	0.00000	.15603ë-11	0.00000	.662548-01	0.00000	22914E-01	. ຼີ ວະດ້ວວດຈີຼີ
*10813E+03	0.00000	.15047E-13	ō.00000	-40269E-12	000000	.1/100E-11	. 0.00000	12479E+U0	<u> 0.00000</u>	38728E-01	0.0000_
t0813E+00	0.00000	25704E-13	0.00000	J\$679E-12	000000	~.15382±~11	~00000	-12479E+00		38728E-01	<u>. 00000</u>
12705E-01	0.00000	309796-13	0.00000	55505E-13	0.00000	165/7L-11	0.00000	+62554E-01	_0.00030	**\$S>S&r**00	~o.oooo_
.12705E-01	•			-46530E-13							
-12705E-01	6.00000	43164E-13	0.0000		0.00000	~ ,190Z0E-11	0.00000	"-,62554E-01		żz52ᣥ00	0.00000
12705E-01	0.00000	.40283E-13	0.00000	143396-12	0.00000	102826-11	0.00000	625546-01	0.00000		0.00000
108135+03	0.00000	717250-13.	0.00000	45769E-12	0.00000	16766L-11	0.00000	* 12474E+00	0.00000	38720c-01	0.00000
.10813E+00	0,00000	10904E-13.	0.00000		_0.00000	17474E-11	_9•áoōؤo	124796.00	0.00000	.38728E-01	0.00000
506396-02	0.00000	999661-14	0.00000	533648-12	0.00000	.160081-11	0.00000	662546-01	0.00000	· 22914c,=01	
•20634E-05	0.00000	436746-14	0.00000	.477696-12	0.00000	151906-11	0.00000	662546-01	0.00000	227146-01	0.00003
96196E-01	0.00000_	.805088-14	.0.00000		_0.00000	636181-12	0.00000	. 1284JE+QU	00000	-32174m+00	0.0000
-96190E-J1	J.00000	·21323E-13	0.00000	85148E-12	ŭ.00000	.60014c-12	0.00000	.1284JE+00	0.00000	~~.32178E,+00	i o. 50090
*12895E+03	0.00000	108194-14	0.00000	706698-12	0.00000	.879456-12	0.00000	-+11094E+00	0.00000	91801 <u>+</u> 91	
120758+00	0.00000	19520t-13	0.00000	.68183E-12	0.00000	911926-12	0.00000	11096E+00	0.00000	91d01c-01	0.00000

HATURAL FREQUENCY = " . 157976E+04"

NATURAL FREUULNCY. .160082E+04

TX Real	TX Imag	TY . REAL	TY	TZ REAL	TZ I HAG	REAL REAL	RX Imag	RY REAL	THAG 4.A	RZ	. RŽ
.113/9E+00	0.00000	.74931E-11	0.00000	.33916E-11	0.00000	.10565d-10	0.00000	10671E+00	0.00000	10949c+00	0.00000
•11379E+00	0.00000	74260E-11	0.00000	.30715E-11	0.00000	-10422L-10	0.00000	-:10671E+00	0.00000	10749E±00	. 0 • 0 20 0 <u>0 .</u>
.16997E+U0	J.90000	202276-11	0.00000	22025E-11	0.00000	.12914e-10	0.00000	.17828E+00	0.00000	1792oE+00	0.00000
.169972+00	0.00000	.20676E-11	0.00000	21862E-11	0.00000	.12581E-10	0.00000	.17828£+00	0.00000	.17926E+00	_0.000007_
-12999E-01	0.00000	.105852-11	0.00000	123335-11	0.00000	276026-11	0.00000	724386-01	0.00000	.24119e+00	0.00000
-12999E-01	0.00000	165528-11	0.00000	145056-11	0.00000	-+304516-11	0.0000	7243dE-01	0.00000	24119E+00	ັດ.ດວັດດວັ
-33454E-01	0.00000	.332551-12	0.00000	.76055 <u>E</u> -12	_0.00000	. +24094E-11	0.00000	60371E-01	_0.00000	105266+00	_0 • 00 0 0 <u>0</u>
-334648-01	0.00000	285571-12	0.00000	. 635366-12	u.00000	.18759E-11	0.00000	.60371E-01	0.00000	10526£+00	_0.00000_
.76644E-01	0.00000	350721-12	0.00000	455246-12	0.00000	.8u360E-12	0.00000	59503E-01	0.00000		0.00000
-766446-01	0.00000	.268116-12	0.00000	546991-12	0.00000	.423956-12	0.00000	59503E-01	a. oo o o o	1950jE+00	0.00000_
.76644E-01	0.00000	.217166-12	0.00000	.15899E-12	0.00000	309050-13	0.00000	59503E-01	Ta. 00000	19501E+00	0.00000
-76644E-01	0.03000	16876E-12	0.00000	16 <u>0</u> 95 <u>F</u> -15_	0.00000	650998-12	0.00000	5950JE-01	_0.0 <u>0</u> 000 <u>0</u>	.19501£.00	0.00000
-,33464E-01	0.00000	-69750L-13	0.00000	228146-12	0.00000	-13421E-11	0.00000	.60371E-01	ú. 0000o	105266+00	0.00000
•33464E-01	0.00000	14072E-13	0.0000.0	<u>T</u> 305ZE-ĽZ	_0.00000	.834856-12	0.00000	[.60371E-01	o • o o o o	. " F,Ô 25 9E + Ó Ď	_0.00000_
-12999E-01	0.00000	.47d99L-12	0.00000	.27913E-12	0.00000	89128E-12	0.00000	72438E-01	_0.0000ò	241198+00	_0.00000
·•12999L-01	0.00000	55d14E-12	0.00000	:4253/E-12	0.00000	12298E-11	0.00000	72438E-01		.Ž4119E+00	
169975+00	0.00000	659115-12	0.00000	.72504E-12	0.00000	.42558E-11	0.00000		0.00000	.179266+00	0•000001
•16997E+00	0.00000	.941138-12	0.00000	.850096-12	0.00000	.420985-11	0.00000	17828E+00	~0.00u00 _.	. - . 17926£+00°	0.0000
.113791+00	ő.00000	.249658-11	0.00000	10853E-11	.0.00000	.35297t-11	0.00000	T+10671E+00	0.00000	.10949E+00	0.00000
·•11379£+05	0.00000	25506E-11	0.00003	10852E-11	0.00000	.35639t-11	_0.00000	106716+00	0.00000	109498+00	

NATURAL FACQUENCY= .1631356+04

TX REAL	TX IMAG	. IY . KEAL	TY THAG	. TZ	TZ I HAG	KX Real	RK Emag	- RY REAL	RY KZ ZZ
-15581E-11	0.00000	,19d05£+00	0.6006 6	848556-01	0.00000	-+27770E+00	0.00000		0.00000154602-11 0.00000
149965-11	9.0000n	•14902F+00	0.00000	"84855E-Q1	0.00000	-+277700+00	0.00000		0.00000 .150536-11 0.00000
235688-11	0.00000	.*70d34E-01	0.60000	.58832L-01	0.00000	334916+00	0.00000	-24368E-11	0.000002450de-11 0.00000
		70834c-01	0.00000	.58832E-01	0.00060	314916+00	0.00000	.24777E-11	0.00000 .235776-11 0.00000
.1694JE- <u>1</u> 2	0.00000	4345LE-01°	0.00000	.33278E-01	0.00000	.7741dE-01	0.00000	97385E-12	0.00000 3.326472-11
15901E-12		+43451E-01	0.00000	•33278E+01	0.00000	.77418E-01	0.00000	94913E-12	U.0000034548E-11 0.00000
42816E-12				18752E-01	0.00000	-+64/946-01	0.00000	.81537£-12	0.00000 .14958E-11 0.00000
+42058E-12	0.00000	-73081E-02	0.00000	187528-01	0.00000	647846-01	0.00000	.803508-12	0.00000149445-11 0.09000
.10383E-11	0.00000	.27128F-05							0.00000 .261526-11 <u>0.0</u> 0000
103636-11	0.00000					5/8546-02			0.00000 261308-11 0.00000
-10787E-11	_					57854E-02			0.0000027566E-11 0.00000
11079E-11	0.00000								0.00000 211-346465.
47542E-12									U- 00U0014051E-11_0.00000
-50736E-12						-+647845-01	0.00000	-88763E-12_	0.00000 .11d14g-11 0.00000
-20276E-12				33274E-01					0.0000033022E-11 0.00000
* -24242E-1 2	0.00000	-43451E-01	0.00000	-33278E-01	0.00000	.7/418E-01	0.000000	_+10215t-11	0.00000 .33984E-11 0.0000
22796E-11	0.00000	.70d34E-01				33491t+00	0.00000	.24025E-11	0-00000 .23357E-11 0.0000a
.23052E-11	•			58832E-01		•			0.0000023068E-11 0.00000
.14751E-11		198056+00	0.00000	.448558-01	0.00000	27770E+00	0.00000	14133E-1 <u>1</u>	0.00000 14478=11 0.00000
15022E-11	0.00000	* 13802E +00	0.00000	.84855E-01	0.00066	27770L+00	0.00000	141381-11	0.00000 -146206-11 0.00000

		NATURA	L FREQUEN	CY= .160187	'L+64			,	are to programme and		
TX REAL	TX 1HAG	TY REAL	TY IMAG	TZ REAL	TZ 1 HAG	RX K£AL	RX IMAG	RY	JHAG	KEAL	RZ IHAG
10050E-L1	0.00000	.19H41E+00	0.00000	.847205-01	0.00000	.270776+00	0.00000	.92087E-12	`0 <u>~</u> 000 <u>0</u> 0	. 90170E-12	0•_ñ,0 0_00_7
-99603É-12	0.00000	19841e+00	ิ ๑ • คภ ๑ ๏๊ วั"	64720E_01	_0.00000	27677E±90	0.00000			96077E-12	_0.0000 <u>0</u> _
15170E-11	0.00000	72294E-01	0.00003	575258-01	0.00000	+33657E+00	0.00000	15461E-11	0.00000	.16461E-11	_0:00000
151748-11	J*0090ō	.7.294E-01	0.00006	575258-01	0.00000	.33657L+00	0.00000	15695E-11	0.00000	100598-11	0.00003
::80841F-13	0.00000	.44741E-0L	0.00000	37526E-01	0.00000	74027E-01	0.00000	582310-12	0.00000	22554c-11	0.00000
68500F-F3	0 • 0 0 0 0 0 0	447416-01	0 • 00 0 0 0	37526F-01_	0.00000	74027E-01	.000000		_ 0* <u>,</u> 00 <u>,</u> 00 0 ñ 0 _	.23055c-11	<u>0.00000</u>
.25461E-12	0.00330	.10>576-01	0.00000	* + 23357L-01	0.00060	.42770= -01	0.00000	~~47287£-12	0.00000	9359/z-12	_ <u>ó-</u> 0900 <u>7</u> .
24083E-12	0.00000,	10557E-01	0.00000	.233578-01	0.00000	.427766-01	0.00000	508418-12	0.00000	``97790£-12_	
-65561E-12	0.00000	1949 3E -01	0,00000		_0.00000	37021Ê-01			0.00000	18379E-11	0.00000
.69732E-12	0.00090	.1.4936-01	0.00000	130275-01	0.00000	.3/0216-01	0.00000	.46193E-12	0.00000	.17310E-11	0.00000
73965E-12	0.00000	.19493E-01	0.00000	13027E-01	0.00000	3/0216-01	0.00000	•61712E-12	u.00000	•17334E-11	0.00000
75891E-12	3.00000	194931-01	0.00000	13027E-01	<u></u>	370216-01	0.00000	58983E-12	_0• òòōoō	<u></u> 197 <u>97</u> E-11	0.00000
•30063E-12	0.00000	10557L-01	0.00000	.233576-01	0.00006	42776E-01	0.00000	604756-12		_88801E-12_	0.00000
39477E-12	0.00000	-10557£-01	0.00000	.23357E-01	0.00000	42776E-01	0.00000	62292E-12	0.00000	88773É-12	ō.00000
13018£-12	0.00000	44741E-01	0.00000	375268-01	0.00000	.74027E-01	0.00000	.693308-12	0.00000	.23152E-11	0.00000
-17854E-12	0.00000	.44741t-01	0.00000	37526E-01	0.00000	.74027E-01	0.00000	-67091E-12		22133 <u>E</u> _li	0.00000
-15443E-11	0.00000	.72294E-01	0.00000	57525E-01	u.00000	33657E+00	0.00000	16388E-11	_0.00000	15991 <u>E</u> -11	ด์รู้ดงจอวี
15350E-11	0.00000		0.00000	>7525E-01	0.00000	33057L+00	0.00000	161568-11	u.00000	.154614-11	0.00000
1007/6-11	3.003 uð	19941.+00	0.00639	.447206-01	0.00560	27677E+00	0.00000	. •95356E-12	0.00060	900000-12	(0.0000)
.102051-11	y. 00500	.1,,41,.00	0.00000	. 347201-01	0.20 000	2/0776+00	0.30000	.976916-12	0.00000	.9009)E-12	0.00000

*	•	NATURA	L FREGUEN	CY=161127	£+04						
. YX Real	X1 DAMI	. TY	TY IMAG	TZ Peal	T Z I mag	KX KEAL	RX IHAG	RY REAL	RY .		RZ IHAG
21807E-01	0.00000	.97755E-13	0.00000	.360828-13	0.00000	.73785E-13	0.00000	.45997E-01	0.00000	.633081-01	0.00000
-21807E-01	0.00000	56s17E-14	0.00000	57438E-13	0.00000	.12605E-13	0.00000	.45997E-01	0.000.00	633085=01	_0.00 <u>505</u>
.1448LE+00	0.00000	158590-12	0.00000	3,5,3568-13	0-00000	.92650E-13	0.00000	16273E+G0	0.00000	16875£+00	
14481L+00	0.00000	25111b-13	0.00000	327896-13	0.00000	56063E-13	0.00000	162736+00	0.00000	.16875E+00	
7_13194E+00	0.00000	-80229L-13	0.00000	.53590£-1J	0.00000	12996E-13	0.00000	-16680E+00	0.00000	+1d476E+00	
-13194E+0J	.0.00000	.1v362E-13	0.00000	37725E-13	0.00000	243486-13	0.00000	~*16680E+00	0.00900	1849 <u>6</u> E±00	0.00000
.23721E-01	0.00000	.292576-13	0.00000	-161338E-13	0.00000	.36620E-13	,0.0000	10410E+00	_ 0• 00 0 0 0 0	8057 <u>2</u> 6-02	0.00000
23721E-Q1	0.00000	40153L-13	0•00000	.44368E- <u>13</u>	0.00000	.42643t-14.	0.00000	104188+00	0.00000	.80572=-02	0.00000
13725E+00	_u.00000	"13371L-12"	0.00000	.00422E-13	_0.00000	-14063E-13	0.0000	17352E+00			<u></u>
-13725E+0u	0.00000	10451E-12	0.00000	567476-13	0.00000	15446E-13	0.00000] +jijjeșe+80	ភិ*១ភិភិ១០	173426+00	0.0000
.13725E+00	0.00000	·12961L-12	0.00000_	8 1651E-13		.39156E-14	0.00000	17352E+00	0.00000	-1734ZE+00	
137258+00	0.00000	-13955E-12	0.00,000	.91369E <u>-</u> 13	0.00000	41763E-13	0.00000	17352E+QU	0.00,00	173425+00	0.00000
237218-01	0.00000	45215E-13	0.00000	£1-3\\$862;	0.00000	76082E-13	0.00000	.10418E+00	0.00000	~80572E-02	0.0000
23721E-01	0.00000	25138E-13		- •						.805724-02	
.13194E+00	0.00000	61301E-13	0.00000	63059E-13	0.00000	66568t-13	0.00000	16680E+00	ñ. 00n00	104966+00	0.00000
13194E+00	0.00000	65736E-13	0.00000	.84710E-13	0.00000	.10522L-12	0.0000	16080E+00			0.0.0000
~.14481E+00	0.00000	-13199E-12	0.00000	.56198E-13	0.00000	-,11558t-1\$	0.00000	.16273E+00	.p• 00 n ở 0	168756+00	.0.0000_
*14481E *03	0.00000	₌75872L-13	0.00000,	94981E-13	_0.00060	.17780L-12	0.00000	.162736+00	กั• อออ อั	.16875L+00	
.21807E-01	0.00000	8-1976E-13	0.00000	.16865E-13	0.00000	•12057E-13	0.00000	45997E-01	_0.00000	63308t-01	0.00000
21807E-01	0.00000	46618t-13	₫•00 <u>0</u> 0ή	-•18299E-13	0.00000	280986-13		45997E_01	_ <u>0</u> .000 u0	63308L-01	

NATURAL FREQUENCY= .162/016+04

TX REAL	TX	YY .	TY I MAG	TZ REAL	TZ Imag	RX KEAL	RX 1HAG	RY REAL	άΥ Îmağ [·	- RZ	RZ THAS
13373E-12	0-00000	.394721-12	0.00000	.00275E-01	0.00000	•233356-Q1	0.00000	15018E-12	0.00000	•15399£ <u>-</u> 15	0.0000 <u>6</u> .
-17266E-12	0.00000	32401E-12	0.00000	80275E-01	0.00000	233356-01	0.00000	-15791E-12	0.00000	14375E-12	0.0000
.22153E-12	0.00000	200921-12	0.0000	.29536E-01	0.00000	.17d68E+00	0.00000	28179E-12	0.00000	.18793E-12	0.00000
24661E-12	0.00000	67654L-14	0.00000	29536E-01	0.00000	174681+00	0.00000	232098-12	0.00000]	29465E-12	0.00000
.17332E-14	0.00000	.16068L-12	0.00000	60646E-01	0.00000	.17818E+00	0.00000	.92291E-13	_0.00000_	255346-12	0.0000
665498-15	0.00000	.127846-13	0.00000	006466-01	0.00000	19818E+00	0.00000	.6666aE-13	_0.00000]	.21944E-12	0.00000
.7675¤E-13	0.00000	. 202156-13	0.00000	.58803E-02	0.00000	.20376£+00	0.00000	95035E-13_	0.00000	12341E-12	_0.00002
68284E-13	0.09000	62183L-15_	0.00000	58803E-02	0.00000	283766,400	0.00000	080336-13]	0 • <u>0</u> 0 0 0 0 0 0	124156-12	0.00000
962b7E~13	0.00000	128058-12	0.00000	.28254E-01	0.00000	. +24383E+00	0.00000		0.00000	- 205856-12	0.00000
-70226E-13	0.00000	34070b-13	0.00000	28254E-01	`0.00000 <u>`</u>	24383E+00	_0.00000	.707856-13	_o` ōơn oo_	-31264E-12	0.00000
64593E-13	0.00000	.154218-12	0.00000	282548-01	0.00000	.293838+00	0.00000	.24800E-13	0.00000	15307E-12	0.00000
.+86314E-13	0.00000	. 41991E-13	0.00000	28254 <u>F</u> -01	0.00060	29383E+00	0.00000_	-40727E-13		12639E-12	0.00000
.27957E-13	2.00000	10853E-12	0.00000	58t03E-02	0.00000	-24376E+00	0.00000	`51271E-13	_0.00\u00_	67209E-14	0.0000
-•94145E-14	0.00000	.14571E-13	0.00000	.58803E-02	0.00000	28376L+00	0.00000	37249E-13	0.00,00,	39219E-13	0.0000
2150oE-13	0.00000	131676-12	0.0000	`60646E-01	0.00000	.190186+00	0.00000	.94805E-13	000000	*1408SF-TS	0.60005
25738E-13	0.00000	. 12663t-13	_0.00000	-60646E-01	0.00000	19818E+00	_0 - 00000	60177E-13_	[0.00000]	~	0.00000
-15210E-12	0_000000	223890-12	`ō•000ōō`	29536E-01	₫•000ò₫			14559E-12	0.00000	22127E-12	0.60000
13707E-12	0.00000	.94881E-14	0.00000	-29536E-01	0.00000	17868E+00	0.00000	14708E-12	0.00000	.17061E-12	0.00000
99578E-13	0.00000	399196-12	0.00000	802758-01	0.00000	.23335E-01	,0.00000	.88147E-13	. 0.00000"	67342E-13	0.00000
-79901E-13	0.00000	.26543E-12	0.00000	.802/56-01	0.00000	233358-01	0.00000	.79753E-13_	"o•ooóóo	89183E-13	0.00000

NATURAL FREQUENCY= .163565E+04

TX REAL	TX Ihag	TY REAL .	TY IHAG ,	T.Z Real	TZ InAG	₹X REAL	RX IMAG	RY REAL	XY ZZ RZ IMAG REAL IMAG	 -
630818-01	0.00000	134116-12	0.00000	.20810E-13	0.00000	692026-13	0.00000	.48103E-01	0.00000 J.55938E-01 0.0000	ĵō .
-630b1E-01	0.00000	-44469E-13	0.00000	313646-13	0.00000	29878E-13	0.00000	-40103E-01	0.0000055938E-01 0.0000	<u> </u>
.96988E-01	0.00000	.805826-13	0.00000	.203658-13	0.00000	.93992E-13	0.00000	64074E-01	0.00000 -148202+00 0.0000	ij
969895-01	0.00000	.108046-13	0.00000	. +99494E-14	0.00000	15910E-12	0.00000	64074E-01,	0.0000014820E+00 0.0000) <u>ō</u> _
.57501E-01	0.00000	67821E-13	0.00000	75338E-13	0.00000	551736-13	0.00000	65180E-01	0.0000032431E+000.0000	0 _
57561E-01	0.00000	30401E-13	0.00000	.10963E-12	0.00000	.18608E-12	0.00000	65180E-01	0,00000032431E+00 _0.0000	ָסַנ פֿנ
17042E+00	0.00000	.67d86r=13	0.00000	10011E-12	0.00000	.91719=-13	0.00000_	.16830£+00	_ 6.00000 [[[46994E-01_ 0:0000	วัฐ
-170421+03	0.90900	-11807E-13	0.00000	70800E-13	0.00000	.60500E-13	0.00000	16830E+00	0.000004699944-01 0.000	ງລ້
94519E-01	0.00000	. 61680g-13	0.00000	10509E_j5_	Õ+00000	60242E-13	0.00000	13947E+00	0.00000 .90037E-01 0.0000	jō
94519E-01	0.00000	22091E-13	0.0000	-98248E-13	0.00000	.180558-12	0.00000	13947E+00_	0.0000000031E-01 0-0550	<u>10</u>
-,94519E-01	~~00000°	-16195E-13	~0.u0000		~o.doooo	-274406-13	0.00000	.13947E+CO	0.00000 .900378-01 0.0000	<u>10</u> _
.94519E-01	0.00000	64d17E-13	`ó*000 <u>0</u> 0	42397E-[13	0.00000	.203328-12	0.00000	13947E+00	[0.00,00]90037E-01 [0.0000)))
.17042E+00	0.00000	205366-13	0.00000	12700E-13	0.00000	09904E-14	0.00000	16830E+00	0.0000046994E-010.0300	<u> 00</u>
17042E+00	0.00000	270398-13	0.00000	-23182E-13	0.00000	.15444E-12	0.00000	16830E+00	0.00000 469946-01 0.0000	ງລົ
57561E-01	0.00000	.571896-13	0.00000	54502E-13	0.00000	•10169E-12	0.00000	.65180E-01	0.00000324316+00 0.0000	<u> 10</u> .
.57561E-01	0.00000	1d621E-13	0.00000	~88369E-13	0.00000	.729416-13	0.00000	-65180E-01	0.00000 ".32431E+00",0.0000	o ó
96983E-01	0.00000	91321E-14	0.00000	43378E-13	0.00000	.23081E+13	0.00000	.64074E-01	0.0000014820E+00 0.000) j
-9698JE-01	0.00000	10232E-12	0.00000	-57987E-13	0.00000	.803676-13	0.00000	.64074E-01	0.00000 -14820£+00 0.0000	00
.63081E-01	0.00000	25485E-14	0.00000	.590186-13	0.00000	705995-13	0.00000	48103E-01	0.00000 .559382-01 0.0000	οġ
63081E-01	0.00000	.32o50£-13	0.00000	41942E-13	0.00000	•1888E-13	0.00000	48103E-01	0.00000 -155438E-01 0.000	CO

NATURAL FREQUENCY= .163588E+04

ŤX Real	TX IHAG	TY .	TY Imaŭ	TZ REAL	TZ 1MAG	⊀X REAL	RX I HAG	RY Real	'RY IMAG "-	
-163466-01	0.00000	.69867E-13	0.00000	•12983C-13	0.00000	.735111-13	0.00000	. +12104E-01	0.00000	.28535k-01 0.00000
.16346E-01	0.00000	'49967E-13	0.00000	45638E-13	0.00000	.27921±-13	. 0.00000	.12104E-01	0.00000	28535E-01 0.00000
+95203E-01	0.00000	620131-14	0.00000	65077E-13	0.00000	.90931E-13	0.00000	11148E+00	0.00000	55046F+000+05050
.95207E-01	0.00000	•85234E-13	0.00000	.36764E-13	0.00000	43657E-14	0.00000	11148E+00	ò•00000	25096±•000.00000
-19275E+00	0.00000	14330E-13	0.00000	41716E-13	0.00000	179651-12	0.00000	-17602E+00	0.00000	768476-01 0.00000
.19275E+00	0.00000	23901E-13	0.00000	.17972E-13	° å•00000	631521-13	_0.00000	17602E+00	.o. 00000	.76847s-01 0.00000
-31666E-01	0.00000	40962E,-13	0.00000	-30839E-13	0.00000	12774E-12	0.00000	60061E-01	0.00000	
316668-01	0.00000	.481616-13	0.00000	26289E-13	0.00000	157878-12	0.00,000	60061E-01	0.00000	291,98£+00 <u>0.0</u> 0000 <u>0</u>
495298-01	000000	26222E-13	0.00000	32489E-13	_0.0000e	14016É-12	. 0.00000	~~.16584E~01	<u>"</u> ʻo, ʻooo <u>ʻo</u> ʻo	.18624E-01 0.00000
495298-01	0.00000	43106E-13	0.00000	.53664E-14	0.0000	11001E-12	0.00000	16584E-01,	0.00000	186248-01 -0.00000
49529E-01	0.00000	659451-14	0.00000	.40413E-13	0.00000	~	0.00000	165848-01	0.00000	
495298-01	0.00000	7,355648-13	0.00000	10389Ê-13		~.40023E-13	,0*0000ò	16584b-01	0.00000	166244-01 0.00000
316666-01	0.00000	14109E-14	0.00000	350J6E- <u>15</u>		13504E-13	_0,00000	90061g-01	0.00000	29198E.00 0.00000
.31660E-01	0.00000	.10644£~1J	0.00000	.16857E-13	0.00000	404078-13	.0.00000	6006LE-U1	0.0000	
.19275E+00	0.00000	- <u>.</u> 2?6336- <u>14</u>	_0.00000	118105-13	0.00000	21333E-13	0.00000	•11605E*ñ0	0.00000	.76447E-01 0.00000
19275[+00	0.00000	10699E-14	0.00000	188301E-14	Ŏ.00000	214958-14	0.00000	-1760ZE+00	0. 00000	76847E-01 0.00000
.95209E-01	0.00000	.832538-14	0.00000	13228E-13	_0.00000	864296-14	0.00000	1114dE+00	0.00000	
.95207£-01	0-00000	219396-13	0.00000	.31523E-13	0.00000	-46257E-13	0.00000	111482+00	0.00000	250966+00 0.000000
.16346E-01	0.00000	891108-14	0.00000	-14840E-13	0.00000	221926-13	0.00000	-12104E-01	n•ó0000	285358-01 0.00000
.1634bt-01	0.00000	-21975E-13	0.00000	21957 <u>L-13</u>	0.00000	.78014E-14	0.00000	.12104E-01	6.00000	.265356-01 0.00000

NATURAL FALQUENCY= .165042E+34

TX Real	TX I HAG	ŢΥ	ŢY .	TZ REAL	ST 1 HAG	k X K E A L	RX IMAG	RY .	RZ RZ RZ
-13586E-01	u.00000	41825E-13	0.00000	752568-13	0.00000	440756-14	0.00000	32178E-02	0.00000 -12070E-01 0.00000
.1358oE-01	_0.00000	84341613	0.00000	.1501ZE-12	0.00000	.80486E-13	0.0000	32178E-02	0.00000 .12070E-01 0.00000
.48406E-01	0.00000	.22148E-12	0.00000	24548L-13	0.00000	726346-13	0.00000	.577208-01	0.0000015572£+00 0.00000
.4840sE-01	0.00000	.143276-12	0.00000	47562E-13	0.00000	.29000L-12	0.00000	.57720E-01	0.000001>572E+00 0.00000
-14031E+00		,17426 <u>5</u> -12	0,00000	.6155gE-14	0.00000	116591-12	0.00000	11021E+00	0.00000 13758E-01 0.00000
.14031E+00	0.00500	15690E-12	0.00000.	287151-13	0.30000	.120596-13	0.00000	11021E+00	0.0000013758E-01 0.00000
.36205E-01	[0.00030	64877E-14	0.00000	.75334E-13	0.00000	~.71635E-13	0.00000	.1714/E-01	0.00000 -316115.00 0.00000
36205E-01	~_o.ooooo_	.8 4425E-13	0.00000	_,75706E-13_	0.00000	78291±-13	0.00000	17147E-01	0.00000 31611E+00 0.00000
.17013E+00	0.00000	.54369E-13	0.00000	406978-13	0.00000	642686-13	0.00000	.141086+60	
•17013E+00	0.00000	•11651E-12	0.00000	.49627E-13	0.00000	93413c-13	0.00000	14108E+00	0.00000 209736+00 0.00000
.17013E+00		-•151j8E-15	0.00000	.916,35E-13	0.00000	42523L-13	0.00000_	14108E+00	0.00000 -209736+00 0.00000
-17013E+00	0.00000	~96366E-13	0.00050	720676-13	~0.00000	"90701E-13	ő.00000°	141088+00	0.00000 T20973E+00 T0.00000
.36205E-01	0.00000	196176-13	0.00000	172236-13	0.00000	.171744-13	0.00000	171476-01	0.0000031011E+00 0.00000
-36205E-01	_0.00000	23096E-13	0.00000	12050E-13	0.00000	20073E-12_	_ 0•00000_	17147E-01	U.00000 -31611E+00 0.00000
-14031E+00	0.00000	.77241E-13	0.00000	.46303E-13	0.00000	.13078E-12	0.00000	.110Ž1E+U0	0.00000 .13758E-01 0.00000
-14031E+00	0.00000	.15108E-12	0.00000	74545E-13	0.00000	32d436-12	0.00000	*11051E+00	0.0000013758E-01 0.00000
.49406E-01	a-o_ouoo	1521 <u>1</u> Ç-1 <u>2</u>	0.00004	18017E-12	0.00000	16436E-13	0.00000	57720E-01	0.00000 15572E+00 0.00000
.48406E-01	0.00000	138001-12	0.00000	•21222E-12	0.00000	72264t-13	0.00000		0.00000 7.155726+00 0.05000
.135866-01	J.00000	•10204E-12	0.0000	.764606-13	0.00000	86366E-13	0.00000	.32178C-02	U.0000012070E-01 0.03000
-13500E-U1	J.00330	-636731-13	9.00000	572126-13	0.00000	.10056E-12	0.00000	.3217dE-02	0.00000 .12070E-01 0.00000

NATURAL FREQUENCY= .165645E+04

TX Real	TX IMAG .	TY Real	TY IHAu	TZ Real	TZ IHAG	KE AL	RX I MAG	RY - REAL	RY IMAG	REAL T	RZ
34292E-01	0.00000	.140631-13	0.00000	15217E-12	0.00000	10777t-12	0.00000	.24287E-01	0.00000	.30767e-01	0.00000
.342925-01	0.00000	.178346-13	0.00000	.63021E-13	0.00000	20778E-13	0.00000	.24287E-01	0.00000	307676-01	
.58672E-01	0.00000	.13594E-13	0.00000	.881436-13	0.00000	340436-12	0.00000	30824E-01	0.00000	.86146E-01	_0.00000_
58672E-01	0.00000	.69727E-13	0.00000	111836-12	0.00000	.48753L-13	0.00000	30824E-01	0.00000	86146E-01	0.00000
-48980E-01	0.00000	75d38t-13	0.00000	.93565E-14	0.00000	7557dE-14	0.00000	60815E-01	0.00000	24713L+00	0.00000
4898JE-01	0.00000	.88602E-14	_0.00000_	57813E-14	0.00000	145176-12	0.00000	60815E-01	0.00000	. 24713c+00	0.00000
· 18432E+00	0.00000	17448E-13	0.00000	•41425Ė-13	0.00000	47d26E-13	0.00000	.15633E+00	0.00000	.62230£_ <u>0</u> 1	
.18432E+00	0.00000	.14325E-13	0.00000_	17161E-14	0.00000	440396-13,	0.00000	.15633E+0 <u>0</u>	. 0:00000	62230L- <u>0</u> 1	0.00000
-11096E+00	0.000,00	.47243E-13	_0.60000	368716-13	0.00000	.20074E-12	0.00000	889758-01	0.00000	.30045 <u>E</u> +00	0.00000
11096E+00	0.00000	.13733L-14	0.00000	-27697E-13	0.00000	.84633k-13	0.00000	889768-01	0.00000	30082E+00	0.00005
-11095E+00	0.00000	.12678E-13	0.00000	~32848E-13	000000	22861E-12	0.00000	88976E-01	0.00000	30082£+00	_0.00000
11096E+00	0.00000	99651E-13	0.00000	14704E-13	0.00000	.24348L-12	0,00000	889768-01	0.00000	*30085F+00	0.00000
1843ZE+00	0.00000	855615-13	0.00000	.327196-13	0.00000	•35607E-12	0.00000	.156338+00	0.00000	62230E-01	0.000000
.18432E+00	0.00000	297466-13	0.00000	22597E-13	0.00000	.14073E-12	0.00000	·~15633E+00	″ oʻ• oʻo oʻoō	e5530E-QF	_ <u>0</u> .000000
-48980E-01	0.00000	.48700E-13	0.00000	69943E-13	_0.93000	.24107Ę-12	0.00000	60815E-01	0.00000	.24713E+00	
48900E-01	0.00000	41569t-13	~o.00000	.189508-13	0.00000	-102216-12	0.00000	60815£-01	0.00000	24713E + 00	
-58672E-01	0.00000	118366-13	0.00000	20915E-13	0.00000	.10006E-12	0.00000	308246-01	0.00000	86146E-01	0.00000
58672E-01	0.20000	40692E-13	0.00000	46039E-13	0.00000	.47266E-13	0.00000	30824E-01	0.00000	.86146E`Ğ1	
342926-01	0.00000	382338-13	0.00000	22474E-13	0.00000	15129c-13	0.00000	-24267E-01	0.00000	3u767E-01	0.00000
.34292E-01	0.00000	.53410c-13	0.00000	.17319E-13	0.00000	35828E-13	0.00000	.242878-01	.0.00000	3u767e-01	0.00000

NATURAL FREQUENCY= .166276E+04

TX REAL	TX IMAG	TY KEAL	TY Imaŭ	TZ Real	TZ IMAG	ĶΕ A L KX	RX IMAG	RY Real	RY. " EHAG	RZ TIMAG
-156268-13	0.00000	14356E+00	0.00000	126278-10	0.00000	47969b-11	0.00000	.256198-13	0.00000	.43639t-14 0.00000
-163615-13	0.00000	14356E+00	0.00000	.125348-10	0.00000	.449256-11	0.00000	20667E-13.	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	44038E-13 _0.00005
-10456E-13	0.00000	.31233£+00	0.00000	118968-11	0.00000	29114E-10	0.00000	12971t-13	0.00000	14128E-12 0.00002
363722-13	0.00000	•31533F+00	0.00001	.1167LE-11	0.00000	•24528E-10	0.00000	602938-13	0.00000	.120198-12 [0.00000]
-•14417E-12	0.00000	22361£+00	0.00000	14946E-11	0.00000	20/42E-10	0.00000	•14439E-12	0.00000	.15066E-12 0.00000
.159 ₀₀ E-12	0.00000	223616+00	0.00000	.147076-11	0.00000	.201d5E-10	0.00000	.13899E-12	0.00000	12098s-12 0.00000°
-161725-12	0.00000	44469£-01	0.00000	•70693E-11	0.00000	25649L-10	0.00000	12438E-LZ	_0.00000	.736722-13 0.00003
<u>-</u> .15125 <u>C</u> -12	3•000°0°	494696-01	_0.00005	_=_;093>E-LL	0,000000	249876-10	ó•00000"	20586E-12	_o.ooooo_	e3673F-13 _0-00000
70616E-13	0.00000	.2d176E+00	0.00000	.82675E-11	0.00000	30607E-11	0.00000	.94827E-13	0.00000	10025E-12 0.00000
.10629E-12	0.00000	-281/6E+00	0.00000	d2406E-11	0.00000	-23360E-11	0.00000	368400-13	ñ• 0 <u>0</u> <u>0</u> <u>0</u> <u>0</u>	.10124t-12 0.00000
14953E-13	0.00000	201768+00	0.0000	.84157E-11	0.00000	•27122É-11	0.00000	-81274E-14	0.00000	.17724E-12 0.00000
.13896E-13	0.00000	-,28176E+00_	0.00000	83469E-11	_0.00000	~.32385E-11	_0.00000"	33294É-13	0.00950	21569E-12_0.00000
-39900E-13.	0.00000	-49469E-01	0.00000	.69924E-11	0.00000	.25408E-10	0.00000	.20174E-13	0.00006	31341E-13 TO.00000T
625958-13	0.00000	.49469E-01	0.00000	-,69529E-11	0.00000	25877E-10	0.00000	22326E-13	0.00000	.46749c-13 0.60000
€32046E-13	0.00000	.22361E+00	0.00000	142968-11	0.00000	.2u778E-10	0.00000	31591E-13	0.00000	11612E-12 0.00000
11604E-14	0.00000	. 22361E +00	0.00000	14314Ê-11	0.00000	20870E-10	0.00000	85037E-L3	_0.00000]	13290e-120.00000
108965-12	0.00000	312335+00	0.00000	131495-11	0.00000	.29100E-10	0.00000	.12892E-12	0.00000	
-109568-12	0.00000	31233E+00	0.00000	.13880E-11	0.00000	29017E-10	0.00000	.10747E-12	`0.000.00	474106-14 [0.0000 <u>0</u>
716156~13	0.00000	-14356E+00	0.00000	12610E-10	0.00000	.40424E-11	0.00000	365681-13	0.00000	.43751E-13 [0.00000]
62352E-13	0.00000	.14356E+GO	0.00000	.12574E-10	0.00000	45797E-11	0.00000	673986-13	0.00000	47721E-13 0.0000J

NATURAL FELOUENCY= .166343E+04

TX REAL	ΤΧ 1μΔG************************************	TY	TY I HAG	T.Z Real	TZ IHAG	RX REAL	kx I mag	RY Real	RY IMAG	- RZ	RZ ÎMAG
10796E-13		135045-10		.13372E+00	U.OUQUO	.49414E-01	0.00000	.54309E-13	0.00000	.22841t-13	0.00000
-13036E-13		13416L-10		133728+00	0.00000	49414E-01	0.00000	30359E-13	~ú.ŏoû√o	19203e-13	0.00000
-425ob£-13	ó.00000	.293048-10	0.00000	.13180E-01	0.00000	.30678E+00	0.00000	32997E-13	0.00000	.25880E-13	_0:00000_
49753E-13	0.00000	.29212E-10	0.00000	13100E-01	0.00000	30678£+00	0.00000	86334E-14	0.00000	12630 <u>e-</u> 13	0.00000
37159E-13	0.00000	20947E-10	0.00000	.15e03E-01	0.00000	.21957E+00	0.00000	15837E-13	ö. 00000 T	63267E-13	0.00000
22042E-13	0.00000	208766-10	0.00000	į5803E-01	0.00000	219576+00	0.00000	40803E-13	0.00000	23264E13	0.00000
.54993E-13		46476É-11				.2/013E+00	0.00000	283188-14	0.00000	10408E-12	0.00000
-,221316-13	ō•00000	40375E-11	0.00000	74560E-01	_0•00ō0o	27013£+00	0.00000	04618E-13	_o•ōċōōō <u>"</u>	.68987E-13	0.00000
928375-13	0.00000	.26435E-10	0.00000	88145E-01	0.00000	.305306-01	0.00000	.247161-13	0.00000	29047E-13	0.30003
•28694E-13	0.00000	.26369E-10	0.00000	-88145E-01	_0.00000	30530k-01	0.00000	.48483C-13	0.00000	.22548E-13	0.00000
14179E-13	0.00000	25389E-10	0.00000	681455-01	0.00000	3u530E-01	0.00000	-,409446-15	0-00000	.17840E-12	
.28824E-13	0.00000	26399L-10	.0.00009	~88145E-01	0.00000	.30530E-01	0.00000	259936-14	.o. <u>0</u> 0000	10636E-12	0.00000
286348-14	0.00000	.465216-11	0.00000	74560E-0İ	0.00000	27013L+00	0.00000	.36567E-13	0.00000	1194ZE-13	0.00000
•79829E-14	0.00000		0.00003	74560E-01	0.00000	2/013E+0Ò	0.00000	~. 26518E-13	‴ถ้ ∙ อั <u>อ</u> ูด oōุ	72532£-13	0-00000
48192E-13	0.00000	.209706-10	0.00000	.15a0JE-01	U.00000	219576+00	0.00000	.83397E-13	0.00000	.14435E-12	
-22473L-13	0.00000	.20940L-10	0.00000	158036-01	0.00000	.21957E+00	0.00000	.34050E-13	0.00000	18488E-12	0.00000
97444E+13	0.00000	29260E-10_	0.00000	13180E-ÓL	0.00000	~.30678E+00	0.00000	65470E-13	. 0 • 00 00 0 0	.58400E-13	0.00000
I.96316E-13	0.00000	272898-10	0.00000	13150E-01	0.00000	.30678L+00	0.00000	10010E-12	0.00000	42099£-14	
13767E-13	0.00000	.13493c-10	0.00000	.133728+00	0.00000	49414E-01	0.00000	.47242E-13	0.00000	263092-13	_0.00000
-141936-13	0.00000	.133861-10	0.00000	13372E+00	0.00000	.49414L-01	0.00000	.18651E-13	0.00000	.92299E- <u>1</u> 3	0•000000

MATHDAL	EREDITENCY *	.1686896+04

. TX REAL	TX Imag	TY	TY IMAG	TZ . Real .	TZ I MAG	KEAL KX	RX IHAG	RY Real	YY	REAL	RŽ
567528-13	0.00000	-33417e-01	0.00000	.10380L-02	0.00000	.371986-01	0.00000	.27183E-13	0.00000	13157 <u>E</u> -1	30.00000_
•14709E-13	0.00000	334176-01	0.00000	.10300E-02	0.00000	.37198E-01	0.00000	13383E-13	.0.00000	.12790E-1	.3 _0. <u>0</u> 00000_
.320a3E-13	0.00000	29133E-01	0.00000	27800E-ul	0.00000	55769E-01	0.00000	. •15265E-13	0.00000_		.20.00000
15423E-13	0.00000	29133E-01	0.00000	278001-01	0.00000	55769L-01	0.00000	•33684E-13	0.00000	177856-1	[20.03050]
.69728E-13	0.00000	525778-01	0.00000	23631E-01	0.00000	204756+00	0.00000	101716-12	0.00000	[149518-1	. 2 <u>. 0 . 0</u> 0 0 <u>0 0</u>
65022E-13	0.00000	.52577t-01	0.00000	236315-01	0.00000	20475£+00	0.00000	76101t-13	0.00000	17544E1	เร _ิดรู้จังดิจุจั
121256-12	9.00000	74249E-01	0.00000	~.12017Ê-01	0.00000	28205C+00	0.00000	.13789E-12	0.00000	-93278 <u>6</u> -1	เราังเยี่ดงดูอั
984756-13	0.00000	.742496-01	0,00000		0.00000	28205E+00	,0*00000	983576-13	0.00000	71819E-	(4 0,00000
-834d1E-13	0.00000	887294-01	0.00000	49463E-02	0.00000	32815E+00	0.00000	10644E-1¿	0.00100	.10052t-	rs <u>o•gg655</u> _
76924E-13	0.00000	.88729c-01	0.00000	49463 <u>6</u> -02	0.00000	32815E+00	0.00000	74601E-L3	0,00000	155230E-	150.00000
.35479E-14	0.00000	887295-01	0:00000	494 <u>6</u> JE-02	0.00000	32d15L+00	0.00000	47654E-15	00000	194466-	1,5 _0 • 00000 <u>.</u>
.12198E-13	0.00000	.80729E-01	0.00000	49463E-02	_0.0000	328156+00	_0•30ŏ0ö	-31535 <u>E</u> -13	0.00000	.12545E-	12 0.0000
340868-13	0.00000	74249E-01	0.00000	.120176-01	_0.00000	23205E+ <u>0</u> 0	0.00000	.98313E-13	_0.00000	.10690E-	12 0.00000
•60c61E-13	0.00000	.74249E-01	0.00000		-0.00000	=. 2d205E+00	0.00000	86989 <u>E</u> -13	_0.000000	14722E-	12 0.00000
.894156-13	0.00000	52577e-01	0:00000	23631E-01	0.00000	204751+00	0.00000	90765E-13	u.00000	36644L-	13 0.00000
796376-13	0.00000	.52577ë-01	0.00000	23631E-01	0.00000	20475c+00	0.00000	102448-12	0.00000	.36678b-	13 0.00000
59528E_13	0.00000	27133E-01	0.00000	.27800E-01	0.00000	557691-01	0.00000	81 <u>0</u> 37 <u>E</u> -13	0.00000	.16215t-	14 0.00000
.53874E-13	0.00000	.291338-01	0.00000	.27800E-01	0.00000	557698-01	0.00000	76121E-13	0.00000	<u>1</u> 9342E-	13 0.00000
.38492E-13	0.00000	.334176-01	0.00000	103806-02	0.00000	•37178E-01	0.60000	18739E-13	0.00000	.51761£-	13 0.000005
342856-13	0.00000	33417e-01	0.00000	10300E-02	å*000 00	.371986-01	0.00000	29515E-13	0.00000	-•37979E	13 0.00000

.169000E+04 NATURAL FREDUENCY= R Z REAL RY ΚY RX REAL RX TZ TZ IHAG ΤY ŤΧ ΤY TX IMAG REAL IMAG IHAG REAL IMAG **LEAL** REAL IHAG . 0.00000 .41912E-13 0.00000 .99613E-14 0.00000 0.00000 -.14741E+00 -.17524L+U0 .15897E-12 0.00000 0.00000 .60789E-14 .23586E-13 0.00000 -.17583E-13 0.00000 -14741E+00 0.00000 .19524E+UO 0.00000 -.17157E-12 0.00000 0.00000 -66994E-14 -.51466E-13 0.00000 -.10059E-12 0.00000 -.22515E+00 0.00000 .18885E+00 0.00000 -.16073E-12 0.000G0 0.00000 -51043E-13 -.67719E-13 0.00000 .55211E-13 0.00000 .22515E+00 0.00000 -.18885E+00 0.00000 .163098-12 0.00000 -.28564E-13 0.00000 .77403E-13 0.03003 .85391E-13 0.00000 -.50557E-01 0.00000 -.u2105t-01 U.00000 -.23160E-12 0.00000 -.60113E-13 0.00000 .86286E-13 0.00000 -.348646-13 0.00000 .50557L-01 0.00000 .62105E-01 0.00000 .25076E-12 0.00000 -97178E-13 0.00000 -.55472E-13 0.00000 30117=-13 0.00005 .60464E-01 0.00000 .21974E+00 0.00000 .10302E-12 0.00000 -.22301r-12 0.00000 -.56528E-13 0.00000 -.14318E-12 0.00000 -.649641-01 0.00000 -.21974t+00 0.00000 .30878E-12 0.00000 --92824E-13 0.00000 .37669E-13 0.00000 _-.22864E-12 0.00000 .19700E+00 0.00000 -.10246E+00 0.00000 -.20876E-12 0.00000 -.293331-13 0.00000 .139216-13 0.00000 .206916-12 0.00000 1-19700E+00 0-00000 -10246E+00 0.00000 .19990E-12 0.00000 0.00000 -.39884E-14 .35412E-13 0.00000 -76449E-13 0.00000 .19700E+00 0.00000 -.86558E-13 [0.00000] .10246E+00 0.00000 -.55409(-)3 0.00000 -.19700L+00 0.00000 .25257E-13 0.00000 .14223E-12 0.00000 -22491E-11 0.00000 _.94138c-13 _0.00000 __.10246C+00 0.00000 .66+64E-01 0.00000 .17462E-14 0.00000 .41941E-13 0.00000 .57962E-13 0.00000 -.44297E-13 0.00000 -.21974E+00 0.00000 --60964E-01 0.00000 --12055E-14 0.00000 --63456E-13 0.00000 .50186E-13 0.00000 _.2/989c-13 0.00000 .21974E+00 0.00000 .30080E-13 0.00000 --11036E-12 0.00000 -.45829E-13 0.00000 -.12231E-13 0.00000 .62105E-01 0.00000 -.50557E-01 0.00000 .50557E-01 0.00000 .28357E-13 0.00000 -.31292E-13 0.00000 -.22533E-13 0.00000 -.30546E-13 0.00000 -.62105E-01 0.00000 -.22515E+00 0.00000 -.50099E-13 0.00000 1.12560E-12 0.00000 .22364E-13 0.00000 __-.18685E+00 0.00000 -.26178E-14 0.00000 .225151+00 0.00000 -.48891E-13 0.00000 121861-12 0.00000 .51396E-14 0.00000 .18885E+00 0.00000 -.424788-13 0.00000 0.00000 .35410E-13 0.00000 _-.740d2E-14 0.00000 -.25372E-13 0.00000 -19524E+00 0.00000 -.14741E+00 .29290E-14 0.00000 .14741E+00 0.00000 .34026E-13 0.00000 --.41756E-13 0.00000 -32720E-13 0.00000 .25793E-13 0.00000 --19524E+00 0.00000

MATHRAL FREQUENCY'S 171349E+04

- TX -	TX	TY	TY IMAG -	YEAL TZ	T Z I H A G	KX KEAL	RX IMAG	RY REAL	REAL IMAG
12605E-13	0.00000	546531-01	0.00000	~29958E-02	0.00000	53974t-01	0.00000	.31688E-13	U.00000 .506712-13 0.0000
.497008-13	0.00000	.54653[-01	0.00000	29958E-02	0.00000	51974E-01	0.00000	.37151E-13	0.00000 - 68564E-13 0.00000
•76792E-13	0.00000	.57d58E-01	0.0000	.4343oE-01	0.00000	.124996+00	0.00000	73966E-13	0.00300950076-13 0.00000
771938-13	0.00000	57858L-01	0.00000	43436E-01	0.00660	.124931+00	0.60000	87969E-13	0.0000020555g-13 0.00003
336458-13	0.00000	.960998-01	0.00000	.18150E-01	0.00000	.32355E+00	0.00000	•1574dE-13	0.00000149978-12 0.00000
12647E-14	0.00000	960996-01	0.0000	.18150E-01	0.00000	•32355E+00	0.00000	.14468E-14	u.00000 16633E-12 0.00000
10102E-12	0.00000	.87622E-01	0.00000	22200E-01	0.00000	.2 15 06E+00	0.00000	.83193E-13	0.00000 .73237E-13 0.00000
.117176-12	0.00000	87622E-01	0.04000	222008-01	0.00000	.21>06E+00	0.00000	.12687E-12	0.00000143276-12 0.00000
.8070dE-13	0.00000	.365801-01	0.03000	42302E-01	0.00000	.11660L+00	0.00000	555508-13	0.00000 .13694E-12 0.00000
100348-12	0.00000	36580E-01	0.00000	42302E-01	0.00000	.116601+00	0.00000	642828-13	0.0000012381E-12 0.00000
-34988E-13	0.00000	365804-01	0-00000	42302E-01	0.00000	11660L+00	0.00000		0.0000015684E-12 0.00003
50596E-13	0.00000	.35580E-01	0.00000	42302E-01	0.00000	11060£+00	0.00000	47973E-13	0.0000022675@-12 0.00000
63677E-13	0.00000	87622E-01	ō*ō0000	22280E-01	0.00000	295062+00	0.00000	-67958E-13	0.0000020953E-L3 0.00000
-62193E-13	0.00300			22280E-01					0.0000061535E-14 0.00000
-20371E-13	0.00000	96097E-01	0.00000						0.00000 [.46215E-13]0.00003
29027E-13	0.00000	10-30000	0.00000	.181506-01	0.00000	~32355E+00	0.00000		0.0000055771E-13 0.00000
.79006E-14	0.00000	5/6598-01	0.00000	- +43436E-01	0.00000	12499E+00	0.0000		0.00000 .21d40E-14 0.00000
3122JE-13	0.00000	.57d58E-01	0.00000	43436E-01	0.0000	12499E+00	0.00000		0.00000 -477978-13 0.00000
58115E-14	0.00000	.540538-01	0.00000	.29958E-02	0.00000	.539746-01	0.00000		. 0.00000 .19780E-13 0.00009
.21539E-14	J.00000	54553E-01	0.00000	.29758E-02	0.00000	.53/74E-01	0.00000	93305E-14	0.00000213516-13 70.00000

NATURAL FREQUENCY= 4172097E+04

TX REAL	F.A. IHAG	Y Y KeAL	TY IMAG	TZ REAL	T1 I mag	K X KEAL	RX THAG ,	RY REAL	RY .	ŘZ REAL	ŘŽ Ímag
30564E-13	0.2000	13789E-14	0.00000	.30928E-01	0.00000	40542E-01	0.00000	.2432dE-13	0.00000	.72502E-14	0.00000
11412E-L3	0.30000	.604531-13	0.00000	30928E-Ő1	0.00000	.4054ZE-01	0.00000	21279E-13	0.00000	11097E-13	
10653E-13	0.00000	50328L-13	0.0000	.14340£+00	0.00000	.23427L+00	0.00000	22809E-13	0.00000	.41307£_13	
.99102E-14	0.00000	16064E-12	0.00000	14346E+00	0.00000	25427£+00	0.00000	60984E-15	0.00000	.237026-13	
112958-13	0.00000	.79705L-13	0.00000	20502E+00	0.00000	.107008+00	0.00000	.45969L-13	0.00000	.35503e-13	
-20172E-13	0.00000	.83275L-13	0.00000	.20502E+0u	0.00000	107UOL+00	0.00000			81655E-13_	
34154E-14	0.90000	646288-13	0.00000	52218E-01	0.00000	.20311E-01,	0.00000			234866-13	
15396E-L3	0.00000	.471666-13	0.00000	522180-01	0.00000	20311E-01	0.00000				
186/7E-13	0.00000	16449E-12	0.00000	22i016+00	0.00000	201751+00	0.00000			8721dt-13	
•57323E-13		.24274t-15				.20195E+00				66661t-13	
_31202E-13	~ 5.00 000	. 21887E-13	[0.00000]	-22101E+00	0.00000	201958+00	0.00000	-			
49997E-13	0.00000	.99346c-1J	0.00000	2.551015+00	0.00000					.1a792E-13	
12415E-12	0.00000	40/65E-13	0.00000	5221BC-01	0.00000	20311E-01	. 0.00000	14511E-12	0.00500	11232516	
98891E-13	0.00000	11108L-12	0.00000	.52213E-01	0.00000	20311E-01	_ 0.00000	_13920£-12	o•_ooo_o		
•12765E-12	0.00000					. •10700L•00					
		172936-12								.15780E-14	
204248-13	0.00000	15156E-12	0.00000	14346E+00	0.00000						
107498-12	0.00000	48640E-13	0.00000	14346E+ÖÖ	.000000	2d427E+00	0.00000	.89326E-13	. 0.00000		u:.ueouo
.30775E-14	0.00000	112181-12	0.00000	30928E-01	0.00000	40542E-01	0.00000	31720E-13	. 6. 00000	_ 6,13436_13 	0.00000
45322E-13	0.00000		0.00000	.30459E-01	. 0.00060	40542E-01	0.000000	334U2E-13	o • _ n n n n o		74474

							0.5	ΨY	٧ د	87
TK REAL	TX Imag	TY .	T f l mag	TZ _ REAL	T Z I MAG	RX Real	RX IHAG	REAL	THAG	RZ ŘZ
	3.00000	.564876-13	0.00000	16574E+00	0.00000	145326+00	0.00000	119626-13	0.00000	32241E-13 0.00000
,••••	0.00000		0.00000	-16574E+00	0.00000	.14532E+00	0.00000	32762E-13	0.00000	.333602-13 0.00000
	0.00000	73227E-13			0.00000	145958+00	0.00000	.24700E-13	0.00000	50775E-13 0.00000
.228445-13				25017E+00	0.00000	.14595£+00	0.00000	.34765E-13	0.00000	.953596-14 0.00000 _
.2315dE-13		193458-12				.212956+00	0.00000	21642E-13	0.00000	.62479E-13 0.00000 _
		.75037E-13				21295E+00	0.00000	36122E-13	0.00000	36660E-14 0.00000
•15792E-13				.70914E-01	=					58346E-13_ 0.00000
.45619E-13				70914E-01						55420E-13 0.00000
•13232L-13	5.00000	.559\1E-13	0.00000							81514E-13 0.00000
.83733E-13	0.00000	.13330e-12	0.0000	112276+00	-0.00000	- 218365+00	0.00000	.574076-13	`0.00000	.29684E-13 0.00000
.10022E-13	0.00000	11907E-12	0.00000	•11227E•00			70.00000	14666f -13	0.00000	16582E-12 0.00000
.38731E-13	0.00000	.10070E-12	0.00000	1155\E+00	0.00000	2103dE+00			່ດ. ດດວິດດ	
124618-13	0.00000	12250E-12	0.00000	.112276+00_	_ 0.00000	.218385+00			 อยักอกกล	-718986-13 0.00000
.10814E-12	_ n•00nn0	.19028E-13	0.00000	70914E-01	ō • ō o o o o	77507E-01	_ 0.00000			2530Zz-12 0.00000
-609598-13	0.00000	`.68271E-13	0.0000	709148-01	0.00000	.77507E-01	0.00000	87003E13	0.00000	27035E-12 0.00000
				43067E-01			0.00000			· ·
-116956-12	0.0000	. 10552E-12	0.00000	143067E-01	0.00000					. 12153E -12 _ 0.00000
26233E-13	1.00000	62218£-13	0.00000		0.00000					197886-12 0.00200
-32643E-13	0.00000	. 16673Ľ-ÏŽ	` <u>0</u> .000 <u>0</u> 0	0 - 25017E+00	0.00000	14595E+00		70700E-13		1 - 12535E - 1Z 0.00000
19915E-13	ō•00000	.83050E-13	0.0000	∪ <u></u> 16574£+Ò∪	0.00000					2 -17300E-13 0.00000
.63250E-14	- 0.00000	10629E-12	0.0000	c - 16574E+00	0.00000	145328+00	0.00000	20538E-13	0.00000	0

" NATURAL FREQUENCY -175117E+04

TX REAL	TX THAG	TY - REAL	TY .	TZ REAL	IZ Ihag	R X KE AL	RK IHAG	RY REAL .	RY RZ RZ
	0.00000	690816-01	0.00000	.94699E-02	0.00000	55798E-01	0.00000	10237E-13	0.0000052647E-15 0.00000 .
-35941E-14	0.00000	.69081E-01	0.00000	1.94699E-02	0.00000	55798E-01	0.00000	20422E-13	0.00000 -16420E-13 0.0000
14590E-13	0.00000	.91704E-01	0.00000	.424636-01	0.00000	.18973E+00	0.00000	.155428-13	0.00000 .417866-13 0.00000
.33879E-13	0.00000	917042-01	0.00000	.42468E-01	0.00000	.18973£+00	0.00000	.60359E-14	0.00000332406-13 0.00005
.24396E-13	0.00000	.11549£+00	0.00000	15792E-01	0.00000	•36559E+00	0.00000	10349E-13	0.00360644396-14 0.30003
3937aE-13	0.00000			157926-01	0.00000	.30559L+00	0.00000	840>2£-14	0.00000 .285102-13 0.00000
44553E-13	0.00000	.10792E-01	0.00000	61098E-01	0.00000	.34367E-01	0.00000	30006E-14	0.00000 -51891E-13 0.00000
-36375E-13	0.00000	107926-01	0.00000	6,109sE=01	0.00000	-34367ê-01	0.00000	324468-13	0.00000233336E-13 _0.00000
			0.00000	319126-01	0.00000	271136+00	0.00000	32274E-13	0.00000" .10410E-12 0.00000
28594E-13	0.00000	102076+00	0.00000	31912E-01	0.00000	27113E+00	0.00000	,383558-13_	0.0000028269E-15 0.00000
- 	0.00000	10207E+00	0.00000						0.00000 54249E-13 0.00000
15986E-13		.102076 +00	0.00000		0.00000	2/113E+00	0.00000	21993E=13	0-00000 - 10710E-12- 0.0000
52828E-13	_0.00000	.16792E-01	0.00000	.61048E-01	0.00000	343676-01	0.00000	88,137E-13	0.00000 .93536E-13 0.00000
-46250E-13	ი. იიაიი	0792 <u>L</u> _01	0.00000		0.00000	.34367E-0L		86851E-13	0.00000 89635E-13 0.00000
	0.00000	F1549E'+00	0.00000	15742E-01	0.00000	*************	0.00000	`55070E-13	0.00000 10150c-12 0.0000
33790E-13		11549e÷00	0.00000	157926-01	0.00000	.30559E+00	0.00000	577210-13	0.00000 72185E-13 0.00000
==24895E-13		-91704E-01	0.00000	42468E-01	0.00000		0.00000	.25871C-13	0.00000 -18465E-13 0.00000
25163E-1-				42468£-01		_	0.00000	~ 24469E~13	0.0000088847E-13 0.0000
.17480E-13	1.00160	690815-01	0.00000	44694E-02	0.00000	50798L-01	0.00000	314GZE-13	u.0000012003E-13 0.00000
-19271E-14	0.00000	.570811-01	0.00000	94699E-02	0.00000	5579dE-01	0.0000	32618E-L3	0.0000027226E-13 0.00000

MATURAL	FREQUENCY=	.175972E+04
MAIUKAL	FKCUUERLI-	************

TX .	TX Īmag	TY	TY IHAG _	T.Z. PEAL	T Z I MAG	ĸEĄĻ ,	RX 1 MAG	RY REAL	THAC	REAL THAG
113926-13		42150E-12				25426E-01.	0.00000	.19759E-13	0.00000	-11550E-13 0.00000
•35113E-13	0,00000	.26979E-12	0.00000	~~.34483É-0,1	0.00000	.25426E-01	0.00000	20470E-13	0.00000	11444E-13 0.00000 _
9620ZE-14	0.00000	78726L-12	0.00000	.1122ŠE+00	0.00000	26563£+00	0.00000	.12948E-13	0.00000	.554688-13 "0.00000"
-15897E-13	0.00000	84146E-13	0.00000	112258+00	0.00000	26563E+00	0.00000	.26541E-13	0.00000	816348-13 0.00000
.41124E-13	0.00000	.13378E-12	0.00000	268551+00	0.00000	.44086£-01	0.00000	333476-13	0.00000	20306=-13 _0.00000
622796-13	0.00000	8d780L-12	0.00000	.26865E+30	0.00000	44o86E-01	0.00000	39715E-13	0.00060	48319E-13 .0.00000
33582E-14	0.00000	•31517E-12	0.00000	.01483E-01	0.00000	24890E+00	0.00000	157750-13	~o.00000	40430E-13 10.00000]
.5097bE-13	0.00000	.25192E-12	0.00000	61483E-01	0.00000	00+100885.	0.00000	.38196E-13	0.00,00	. 7/00d=-13 0.00000
.53520E-14	0.00000	610156-12	0.00000	.60439E-01	0.00000	.314205-02	0.00000	.98426E-15	0.00000	.240956-14 0.00000
•19903E-13	0.00000	.35257L=12	0.00000	60,439E-01	``o.oooco	31420E-02	0.00000	.22809E-14	0.00000	64380E-13 0.00000
322938-13	3.00000	61412E-12	0.00000	60439E-01	0.00000	31420E-02	0.00000	23745E-13	0.00000	31036E-13 0.00000
86227E-14	0.00000	.295286-12	0.00000	60439E-01	0.000000	.31420E-02	0,000,00		"ō•òóooŏo	49314E-13 0.00000
		.36443E-12								35367E-13 _0.000000_
22140E-L3	0.00000		<u>้ จะเด็จจัดดู.</u>	6 <u>14</u> 836_01	_0• <u>0</u> 00000	20870E+00	a•aááð <u>ā</u>	50461E-13	_ ō • ò o ō o o o	57716E-13 0.63000
										109906-12 0.00000
326298-13	0.00000	941852-12	0.00000	+26865E+00	0.00060	.44680t-0ļ	0.00000	25685E-13	0.00000	976526-13 0.00000 "
	0.00000	76857E-12	0.00000	11225E+00	_ 0,00000	26563E+00	_0.00000	128718-13	600000	.42052E-13 0.00000
										54143E-13 0.00000
-1892>E-13		44465L-12								152601-13[0.00000]
554706-13	0.00000	•23673£ -12	0.00000	34403E-01	0.00060	254264-01	. 0.0000Ŏ	-16004E-14	0.00000	158345-13 0.00000

MANAGE STATES STANKED

u .

YX	_TX	TY TY	TY IMAG	TZ REAL	T <i>Z</i> 1 mag	RX . REAL	RX IHAG	RY REAL	. KY 1HAG	ŘŽ KEAL	IMAG
				-10704E+00				.22277E-13	0.00000	L0738EI	3 0.00000
						919558-01	0.00000	.232688-13	0.00000	10780E	3 0.00090
49971E-13		826434-12						.21082E-13	ប៊ុំ . លិចចំបល់	-43644E-1	3 0.00000
•		69855E-LZ				125528+00	0.00000	.22088E-13	0.00100	75136E-1	3 _0.00000
		.83413t-12				33989É+00	0.00000	10679E-12	0.000.00	70377E-L	3 0.00000
		.10823E-11					0.00000	806198-13	0.00000	\$ <u>\</u> \$915F- <u>"</u> 1	3
23579E-13	0,00000	801426-12		. 206878+00		.515086-01	0.00000	.5188/E-13	0.00000	10420=-1	3 0.00000
.32120E-13		75970t-12,				51508E-01	0.00000	.45339E-13	0.00000	15399E-1	20.000000
-:		.36554t-12				.97651E-01	0.00000.	12171E-13	o. 000 a o		3 0.00000
37056E-13	0.00000			.92705E-01		9/651E-01	0.00000	574518-14	_0.00000	15497L-l	2 0.00000
.22720E-13	-					.97651E-01	0.00000	57014E-13	0.00000	11ه556-1	2 0.00000
837058-13						9/651L-01			0.00000	.54727E-1	3 0.00000
11024E-12	0-00000	83239E-12	0.00000	20667E+00	0.00000	.51508E-01	0.00000	.89762E-13	0.00000	21816E-]	3_0.00000
.66300E-13						515086-01			0.00000	.659722-1	3 3 00000
.75894E-13						339898+00		-,72719L-13	0.00000	.14797E-1	rs _0.00030
16204E-13				35278E-01				79409E-13	0.00000	12307E-	rs <u>0.00</u> 0000
		90458E-12					0.00000	.60479E-14	0.00000	1161ŻE-	12 0.00000
-13857E-13		05425[-12		18444£+00			0.00000	1.129378-13	0.0000	29086E-	13 [0.00000]
43593F-14	0.00000			10764E+00			0.00000	.16031t-13	0.0000	31952E-	13 0.00000
-11255E-13							0.00000	.13457E-13	0.00000	.30512Ē-	13 _0.00000_

NATURAL FREGUENCY* .176159E+04

NATI	JRAL	FRE	onëŭci.	٠,	1774	82£+	04
ΓY	•	ΙY		TZ	-	•	TZ.

TX TX TY TY TY TZ TZ TZ	RX RA REAL IMAG	RY RY RZ RZ REAL IMAG REAL IMAG
_15966E-11 0.0000097720E-01 0.00000 .19022E-12 0.00000	.26387E-12 0.00000	.11884E-13 0.00000 .10009E-13 0.00000
-35229E-13 [0.0000097720E-01 0.0000018938E-12 3.00000	215036-12 0.00000	.25462E-13_0.0000026112E-13_0.00000_
19683E-13 0.00000 .25583E +00 0.00000 .61458E-12 0.00000	26507E-12 0.00000	.92429E-14_0.00000 .78612E-15_0.0000
.35879E-14 0.00000 7.255836+00 0.0000053825E-12 0.00000	.44443E-13 0.00000	32982E-14 0.00000025096E-13 0.00000
-18357E-13 0.0000031623E+00 0.00000 -45643E-12 0.00000	91704E-12 0.00000	.15626E-13 0.00000 .25195E-13 0.00000
.40683E-13 0.0000031623E+00 0.0000042794E-12 0.00000	.59846E-12 0.00000	.16100E-13 0.0000031781E-13 0.00000
-34749E-13 0.00000' .25583E+00 0:00000 -37926E-12 0.00000	.85127E-12. 0.00000	16993E-13 0.0000037434E-14 0.00000
20961E-13 0.0000025583E+00 0.0000030965E-12 0.00000	7d259L-12 0.00000	11384E-13 0.0000030689E-13 0.00000
66669E-14 0.0000097720L-01 0.0000058729E-12 0.00000	.28426E-12 0.00000	.21159E-13 0.0000029856E-13 0.00003
.32296E-15 [0.0000097720e-01 0.0000063980E-12 [0.00000	.62435E-13 _0.000 <u>0</u> 0	.55549E-14 0.00000 .98358E-14 0.00000
43102E-14 0.0000097720E-01 0.00000 -17542E-12 0.00000	372226-12 0.00000	23016E-13 0.00000 .93550E-14 0.00000
55235E-14 0.0000097720E-01 0.000002527JE-12 0.00000		
-10745E-13 0.0000025583E+00 0.0000015995E-130.00000	.69775E-13, 0.00000	21939E-14 0.0000057525E-13 0.00000
	-,19746E-12 [0.00000]	19556C-14 0.00000 .48670E-13 0.00000
20464c-13 0.00000316238+00 0.0000057378E-14 0.00000	11178b-12 0.00000	.25477E-13 0.00000 29477E-13 0.00000 T
.58336E-14 0.0000031623E+00 0.0000072922E-14 0.00000	740386-13. 0.00000	.27446E-13 0.0000010561E-13 0.00000
161946-13 0.00000 .25583E+00 0.00000 .991B5E-14 0.00000		12221E-13 0.0000021607E-13 0.00000
880068E-14 0.00900 .25583L+00 0.00000 .57215E-14 0.00000	13657c-12 0.00000	16023E-13 0.00060 .32451E-13 0.00903
-14572E-13 0.000009/720E-01 0.0000020759E-13 0.00000		.22869E-13 0.0000016741E-13 7.00000 T
.66273L-14 0.0000097720E-01 0.0000044023E-13 0.00000	T.28554E-14 0.00000	•544336-17 [0•0000] •3>5486-13 0•0000

,	`	NATUKA	L FREOUS	ACA= *128633	E+04				••	والعامون ومستواسدان الراسور
TX REAL	IX Imag	TY REAL	TY Imag	T/ REAL	T Z I mag	KEAL KX	IHAG	RY REAL	I HAG	REAL IHAG
.16469E-13	0.00000	110416-12	0.00000	.18747E-01	0.00000	135756-01	0.00000	.19412E-13	0.00000	•36506e_13_0•00000
25499c-13	0.00000	.142646-12	ó.00000 <u>.</u>	18747E-01	0.0000	· •135756-01	0.0000	•		270655-14 _0.00003
536506-13	0.00000	.11480L-12	0.00000	.63142E-01	0.00000	-15243E+00	0.00000	.473346-14	0.00000	10549E-13 7.00000
-297176-13	0.00000	218422-12	0.00000	-+63142E-01	0.00000	15243L+00	0.00000	.92015E-14	0.00000	.181525-13 .0.00000
.20612E-14	0.00000	.24d05i-12	0.00000	18849E+00	0.00000	.80491E-02	0.00000			20662 ₅ _13 0.000000
+23785C-13	0.00000	102371-12	0.00000	-18840E+30	0.00000	86491E-02	0.10000	•		12684 <u>m</u> -130-03000
.37575E-13	0.00000	90382E-13	0.00000	.52706E-01	0.00000	30423E+00	0.00000	.17257E-13	_0.00000	33d5b£-140.00000
.154926-13	0.00000	42905E-13	0.00000	527068-01	0.00000	.30423t+00	0.00000	-71011E-13	_ 0.00000	.32606E-14 0.00000
=.39105E-14		16523E-12	0.00000	.22327E+00	0.00000	.20368E+00	0.00000	14802E-14	_ 0.00000	4-194E-13 0.00000
150b6E-14		.205191-12	0.00000	223278+00	0.00000	203686+00	0.00000	87002E-14	. ñ•óoɔōo	
~_46793E-14	0.00000	49752 <u>E-</u> 13	0.00000	22327E+00	0.00000					~.34515E-13 0.00000
53510E-14	0.00000	•13484 <u>6</u> -12	0.00000	22327E+00	_0.00000	20368E+00	0.00000	93854E-14	0.00000	24446E-13 0.00000
20972E-14	_0.00000	.822751-14		52706E-01	_0.00000	304236+00	0.00000		_ō•0οοοό	053316-13 0.00007
.41993E-14	0.00000	177246-12	0.00000		0.00000	.304236+00	0.00000	~ 14905E-13	``v¦ovōoo	-001046-13_0_00000
.129558-13	0.00000	.221,75E-12	ō•0000	18840E+00	á•0ò0c0	86491E-02_	0.00000	- 54363E-14	_ 0 • 0 <u>0 0 0 ñ</u> 0	.30933E-13 0.00000
.6588sE-14	0.00000	=.98407E-14	0.00000	"18840E+00		d6491E-02	0.00000	19520E-14	ń•oò_o o <u>o</u>	
46315E£4	0.00000	32750L-13	0.00000	631426-01	0.00000	.15243c+00	0.00000	92046E-14	. 0.00000	144722-13 0.00000
.16179E-13		13613E-12	0.00000	-63142E-01	0.00000	152436+00	0.00000	18480E-13	0.00000	26039E-13 0.00000
-,43252E-14		125206-13	0.00000	18747E-01	0.00060	135758-01	,0.00004	.27309E-13	0,00000	13923E-13 0.00000
120906-13						13575E-01			0.00000	.19817e-13 0.0000

		NATURA	. FREGUEN	CY= .178690	E+04						
TA REAL	TX IMAG	TY TY	TY	REAL	TZ	RX REAL	RX	RY REAL	THÁG	RZ	RZ I HAG
403441-13	0.00000	.207386-13	0.00000	54197E-01	U.000uu	45 338t -01	0.00006	.60308£-14	0.00000	30541 <u>e</u> _13	`0°0̈000;
10470E-13	J.09J00	63207±-13	0.00005		0.00,000	.453388-01	0.00000	48098E-14		32756E-14	
474838-13	"U.00V00]	.382678-13	0.00000	993606-01	0.00000	74578L-01	0.00000	13098E-13	0.00000	. 6J733c=13	0.0000
66436E-14	0.00000	1216866-12	0.00000	□.99360E-01	0.00000	.74578E-01	0.00000	32842E-14	0.00000	86996E-15	0.00000
<u></u> 39432E-14	U.00000	110108-12	0.00000	45753L-01	0.00000	-24d86E+00	0.00000	.72807E-14	_0.00000	110046_12	0.00000
322858-13	000000	78658E-13	0.00005	45753E-01	[0.00000]	~.24886L+00	0.0000	16466E-13	_0.000000	324336 <u>-1</u> 3	0.00000
41706E-13	0.00000	.179194-12	0.00000	23877E+0J	0.00000	74627L-01	0.00000	59916E-14	0.00000	.92119L-14	0.00000
.19373E-13	0,00000	29a00E-i3_	_0.00000	.23877E+00	_0.00000	74527E-01	0.60000	•356218-14	0.00200	119726-13	0.00000
24808E-13	0.00000	.66879E-13	<u>5.00005</u>	.14785E+00	0.00000	28480E+00	0.00000	-62132E-15	0.00000		0.00000
.32531E-13	0.00000	.848738-14	0.0000	147851+00	0.00000	.234d0£+00	0.00000	*30391E-13	Q•'00160	.49761m-13	_0*00001_
	0.00000	29449E-12	0.00000	.14785E+00	0.00000	.20460t+00	0.00000	* ±85952E-14	0.00000	789051-13	_ 0.00000_
17601E-13	0.00000	169446-14	0.0000	14785E+00	0.00000	28480E±90	Ď*000 <u>9</u> ô	10365E-13	0.00000	86346Ê-13	0.00000
-48859E-13	0.00000	.12249E-12	0.0000	23877E+00	0.00000	.746275-01	0.00000	63308E-13	0.00000	87337E-13	0.00000
450536-13	3.00000	.305848-12	0.00000	.23877E+00	0.00000	74627L-01	0.00000	62940E-13	0.00000	.4364ŌE-13	. 0. 90000
100876-12	0.00000	11428E-12	0.00004	457536-01	0.00000	248861+00	0.00000	•56681E-13	0.00000	150992=15	0.00000
71516E-13	0.00000	~~37431£~12	0.00000	45753E-01	0.00000	~ £24886E+00	0.00000	64450E-13	0.00000	.140036-12	0.00000
-40711E-13	0.00000	.31783E-12	0.00000	. 993608-01	9.00000	.74578E-01	0.00000	36627E-13	0.00000	.98951E-13	0.00000
18310E-13	0.00000	.667782-14	0.00000	99360E-01	0.00000	745798-01	0.00000	39843E-13	0.00000	,34032E-13	0.00000
89380E-1-	0.00000	18635E-12	0.0000	541//E-01	0.00000	.4>338L-01	0.00000	.10666E-14	0.00000	*138986-13	_ o•nəəəə
.283776-13	g.00000	.195252-13	0.00060	.541976-01	0.00000	453381-01	0.00000	.22287E-14	0.00000	17649E-13	0.00000

		NATURA	L FKEGUENC	:18001s	E+04						
TX REAL	TX IHAG	TY Kēal	TY Imaŭ	TZ Real	TZ IHAG	R.K "KEAL	KX 144G	RŸ Keal	LMAG .	RZ RZ REAL IMAG	
.19441E-13	0.00000	¢5o23u-01	0.00000	-14785E-01	0.00000	53013E-01	0.00000	.49440E-13	0.00000	.2d262E-13 0.0000	<u>o</u>
.34395E-13	0-00000	.85623E-01	0.0000	.14785E-01	0.00000	53013E-01	0.00000	11651E-14	0.00030	12905E-14 0.0000	
-121196-13	_	-14144E+00	0.00000	.2707dE-01	0.00000	.23184E+00	0.00000	21080E-13	0.00000	.70764E-14 0.0000	0 -
.27335E-13	0.00000	141446+00	0.00000	.27078E-01	0.00000	.231840+00	0.00000	39192E-13	0.00000	50564E-13 0.0000	<u>0</u>
-699b6E-13	0.00300	.88756L-01		490636-01	0.00000	.16354c+00	0.00000	.26181E-13	0.00000	28376E-13 0.0000	<u>ં</u>
.69261C-14	3.30000	887561-01			0.00000	.16354E+00	0.00000	.24706E-13	0.00000	.2455dE-13 _0.0000	ĮŠ.
•12256E-13	0.00000	127544+00	0.00000	392946-01	0.00000	234876+00	0.00000	52794E-14	0.00000	.57436E-13 0.0000	1 <u>9</u> _
-103395-14				392948-01	0.00000	234876+00	0.00000	.12957E-13	0.00000	28962E-14_0.0000	<u>) j _</u>
• •	_			.46435E-01		20303E+00	0.00000	36684E-13	0.00000	-, 55504E-140.0000	įŌ
.65102E-13	0.00000	.10465_+00				~.20303L+00	0.00000	-,.291998-13	0.00000	12795L-13 0.0000	٠ <u>٠</u> أ
24115E-13		.103652+00		.46495E-0I		_203036+00	0.00000	10250E-L4	0.00000	13835=-13 ⁻⁰ 0.0000	00
882665-14	0.00000	• - · + - ·		46495E-01		. 203038+00				.67840 <u>E-13 0.00</u> 00	
.12081E-13		107536+00	_0.000000_	40204522							
-11030E-13	-					.ZJ487L+00		.19934E-13	6.00000	29003E-13, 0.0000	00_
				39294E-01						-73846E-13 0.000	
-79779E-13	0.00000					1,5354E +00				20348c-13 0.000	
57331E-13	0.00000	.887566-01		49063E-01						8698ZE-13 0.000	
120916-13	0.00000									.45d75E-13 0.000	
80815E-14	0.00000	.141446+00		.27078E-01		•					
508348-13	0.00000			. 14785E-01		_				15515e-13 0.000	
-,566110-14	0.00000	550236-01	0.00000	.14785E-01	0.00000	-5,0136-01	0.00000	.80220E-14	0.0000	* TSC S E = 13 0 000	

NATUPAL FREQUENCY= .184318E+04

TX Real	TX IMAG	TY	TY Inag	TZ REAL	TZ EMAG	. RX Real	RA	RY	. ky Thag	RZ REAL	RZ IHAG
-51710E-13	0.00000	.49469E-01	0.00000	,23563E-13	0.00000	20285E-13	0.00000.	.60362E-14	0.00000	46567£-13	0.00000
:-28790E-15	0.00000	~~.49469E-01	0.00000	- <u>.</u> 183416-13	0.00000	43226E-13	0.00000	.•12449E-13	<u>` 0</u> 00000	60413E-13	0.00000
.75404E-13	0.00000	143566+00	0.00000	71488E-14	0.00000	.14553E-12	0.00000	.14386E-14	0.00000	52341:-14	6.00000
-16332E-13	η·00000_	-,•14356E+,00	0.00000	~48833E-13	0.00000	.96948E-13	0.00000	. 399936,-14	0.00000		0-07000
.15134E-13	0.00000	. *55361E+00	0.00000	62772E-13	U.00000	-31167L-13	0.00000_	79480E-14	0.00000	20678E-13	
-13405E-13	0.00000	.223610+00	0.00000	. 32092E-14	0.00000	.22,086E-12	0.000000	.34412E-14	0,000,00	. 3908 3£ −13	0.03600
-19312E-13	0.00000	201768+00	_0.00000	.73919 <u>6-13</u>	0.00000	-,10556c-12	0.00000	19331:-13	_ 0.0000	51102c-13	0.0000
-82021E-14	0.00000	281766+00	0.00000_	119108-12	0.00006	10038E-12	_ 0.00000	17850E-14	0.00000	76246£-14	<u></u>
7.27891E-13 (0.00000(•31233E+00	0.00000	14354E-13	~0.0000°	51060E-13	0.00000	.552388-13	0.00000	50538£-14	0.00007
•626298-13	0.00000	+31233£+00		• <u>745</u> 32E-13	0.00000	201176-12	0.00000	-45650E-13	0.00000	42104E-13	0.00000
.57759E-13	0.00000	31233E+00	<u></u> 0.00000"	174476-13	.0.00000	.52040L-13	``o.ooooo	16802E-13	00000		<u></u>
32086E-13	0.00000	31233E+00	- ö•öööö ⁻	96574E-13	_0,00000	•195226-12	0•0000	234ilE-13	<u></u>		_0.69650_
د1-1562 و 1562.	.0.00000.	28176E+00	0.00000	[-13245 <u>E</u> -13]	0.00000	153186-12	0.00000	36864E- <u>1</u> 3		23719E-13	0.00000
74957E-13	0.00000	.28176 <u>+</u> +00_	. ŏ•óoooo	86506E-13	0.00000	-236491-12	0.00000	1861 JE-13	<u></u>	.4236ot-13	0.00000
87090E-13	J.00J00	22361E+00	n:00000	36853E-13		48893E-13	0.00000	.35971E-13	ö. 0000°	70430E-13	
-49973E-13	0.00000	223616+00	0.00000	45559E-14	0.00000	17858r-12	0.00000	-34181E-L3	0.00000	\$2649E-13	_0.0000n_
_32189E-13	0.00000		0.00000	76191 <u>E-14</u>	0.00000	14483E-12	0.00000	154790-13	0.00000	.929 <u>68</u> £-13	0.0000
132798-13	0.00000	•14356E+00	0.00000	.465746-13	0.00000	194496-12	0.00000	18144E-13	0.00000	71471E-13	0.00001
125188-13	o • 000 <u>0</u> 00	494691-01	0.00000.	.21974E-13	0.00000	.33375L-13	0.00000	90649E-14	0.00000	.30163e-13	0.00000_
.6179øE-14	0.00000	49467L-01	0.00000	.36454E-14	0.00000	.53534L-13	0.00000	118476-13	0.00000	11417t-14	0.00000

•	NATURAL	FREGUENCY=	.186602E+04

NATURAL FREQUENCY= .186602E+04												
	TX REAL	TX EHAG	- TY .	TY IMAG	T∠ REAL	THAG	RX Real	RX I HAG	RY	HAG T	ŘZ	THÃG
	15333E-13	0.00000	101916+60	0.00000	.16216E-01	0.00000	49039E-01	0.00000	-66442E-14	0.00000	.49670E-13	0.00000
	- <u>.2</u> 9240E-13	0.00000	*10141F+00	0.00000	-16216E-01	_0.00000	48039e-01	0.00000	.26125E-13	0.00000	11539F-13	0.00000
	50994E-13	0.00000	.20656C+00	0.00000	.53920E-02	0.00000	#23347E+00	0.00000	14934E-13	0.00000	20115¢-13	0.00000
	46346E-13	5.00000	20656E+00	0.00000	-,539268-02	0.00000	.23347E+00	0.00000	21781E-13	0.00000	52084E-14]	0.000,00
	21787E-13	0.00000	20272=-01	0.0000	48850E-01	0.00000	20200£-01	0.00000	19441E-13	0.00100	77310E-14	0.00000
	.30577E-13	0.00000	.20272L-01	0.69000	48856E-01	0.00000	262008-01	0.00000,	.10465E-13	0.00000	.70674E-14	
	.44634E-13	0.00000	19b75E+00	0.00000	f8008E-01	0.00060	23610£+00	0.00000	•11251E_13	_0.000 oo	64839E_14	0.0000_
	_28481E-1J	0.00000	19675E+00	0.00000	18608E-01	0.00000	23b10è+00	_0.00000,	828728-14	0.00000	.10684E-13_	3.00000_
	-64810E-13	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	127555+00	6.00000	40779E-01	00.00000	.15371E+00	0.0000	-11238E-14	0.00000	- <u>-</u> 15821E-13	0.0000
	44044E-14	_0•00boo	12/58E:00	0.00000	40779E-01	_0•00000j	.15371L+00	0.00000	502206-14	_0.00000 _	-23159E-13	0.00000
ဝု					40779E-01							
-111			12758E+00	0.00000	407/9E-01	_0.000000	.15371E+00	<u></u>	18563E-13_	0.0000	.94281E-13	0.00000
	309048-13	0.00000	17075E+00	0.00000	19009E-0T	0.00000	23610£+00	0.00000	.46025E-13	0.00000	_•95520e13	0.00000
	.35711E-13	0.00000	-19675E+00	6.00000	18608E-01	·00000	236100+00	0.00000	.4d677E-1J	0.00000	92389E-13	0.00000
	_71190L-13	0.00000	20272E-01	0.00000	• 48856E-01	0.00000	26200E-01	0.00000	58284E-13	0.00000	.65157t-13 [0.0000.
	721966-13	0.00000	.20272[01	0.00000	48d56E-01	0.00000	20200E=01	0.00000	55201E-13	0.00000	3/974±-13	0.00000
	10243E-13	0.00000	.20656E+00	0.00000	53926E-02	0.00000	.233476+00	0.00000	.12814E-13	_ 0.00 po	105436-12 _	0.0000
	10985E-L3	0.00000	20a56E+00	0.00000	539268-02	0.00000	.23347_+00	0.0000	.841648-14	0.00000	.94852E-13	0.0000
	273516-13	0.00000	101918+00	0.00000	162168-01	0.00000	48039t-01	0.00000	.20400E-13	0.00000	,•66858E-14	0.00000
	61085E-14	0.00000	-101916+00	0.00000	16216E-01	0.00000	480396-01	0.00000	.27385E-13	0.00000	33008E-13 _	0.00000

-37407E-13	0.00000	.100286+00	0.00000	13396E-01	0.00000	.37738E-01	0.0000020	636E-13	0.00000	43785E-13 Q-0	00007_
:-14430f-1 i	0,00000	10028£+00	0.00000	13396E-01	u.00000	37738E01	0.0000021	.675 <u>C</u> -13	_o.oovod_	.15040E-13 0.	0.0000
·.26594E-13	0.00000			.93521E-02			0.00000 .30	314E-13	0.00000	.37695E-13 0.	00000
		.24415Ē+00		.435/1E-02			0.00000 .37	813E-13	0.00000	40298E-13_ 0.	000007
		.184446+00		.21627E-01			0.0000035	6211-13	0.00000	38354£-13 0.	υο οο ν <u> </u>
.477578-13	•	•		.21627E-01						21479E-13 0.	
59550E-13										3162 <u>8Ē</u> -13 _0.	
.11517E-13									0.00000		
28083E-13	0.00000	32933t-01		7.324656791	~					38115t-13 <u>0</u> .	00000
19978E-13	0.00000	22247E+00	0.00000	- *12383E-Of	0.0000	-4100235.00	0.00000 " 'i'		. 111111		00000
-32441E-13	0.00000	.22247E+00	0.00000	1538JEQL	0.00000	1d023E+00	0.000005	15096-13	0.00000	05319E-14 0-	
-20355E-13	0.00000		~o.ooooo		0.00000	18023E+00	0.000001.	2755E-13	0.00000	*3380jr-13 0	้จอดด้า
27336E-14	0_00000	1722247E+00	0.00000	15383E-01	0.00000	.14053F+00	0.00000 1	5299L-13	. o o o o o o	50317t-13_0.	00000
.22709F-13	0.00000	32933E-01	0.00000	329656-01	0.00000	203462-01	0.000002	36576-13	0.00000		00000_

КX

KEAL

--33577E-14 0.00000 -32433E-01 0.00000 -32965E-01 0.00000 -26346E-01 0.00000 -18424E-13 0.00000 34133E-13 0.00000 -.50528E-13 0.00000 -.18444L+00 0.00000 .21627E-01 0.00000 -.13021E+00 0.00000 -.23673E-14 0.00000 -.13608E-13 0.00000 31700E-13 0.00000 1.18444E+00 0.00000 1.21627E-01 0.00000 -.15021E+00 0.00000 -.61524E-14 0.00000 1.16046E-13 0.00000 -.10617E-13 0.00000 .24415E+00 0.00000 _.93521E-02 0.00000 .19111E+00 0.00000 .48811E-14 0.00000 _.30336E-13 0.00000 .16277E-13 0.00000 -.24415E+00 0.00000 .93521E-02 0.00000 .19111E+00 0.00000 .51714E-14 0.00000 -.14170E-13 0.00900 .29295E-13 0.00000 -.10029E+00 0.00000 -.13396E-01 0.00000 -.37738E-01 0.00000 .18961E-13 0.00000 .15655E-14 0.00000 --28316E-13 0.00000 .10924E+00 0.00000 --13396E-01 0.00000 --37738E-01 0.00000 -14105E-13 0.00000 --11251E-14 0.00000

NATURAL FREQUENCY=_ .194483L+04

TZ REAL_

ŢΥ

IHAG

TX IHAG

NATURAL FREGULNEY= ".201748E+04

TX	TX ÎHAG	TY REAL	TY	TZ REAL	TE	, KEAL	RK IMAG	RY REAL	. IHÝ <u>C</u>	RZ	RZ IHAG
•18913E-14	0.00000	.76970±-01	0.00000,	890818-02	0.00000	.240474-01	0.00000	18414E-14	0.00000 ·	.82259E-14_	0.00003
.16933E-13	0.00000	76770E-01	0.00000	89081E-02	0.00000	24647E-01	0.00000	40883E-14	0.00000	·242856_15_	0.00000
.74810E-14	0.00000	21570c+00	0.00000	12501E-01	0.00000	129261+00	0.00000	.26086E-13	0.00000	.554946-13	<u>0.0000</u> 5_
-31188E-13	0.00000	.215706+00	0.00000	.12501E-01	0.00000	-:12926E+00	0.00000	.33100E-13	0.00000	-28060E-13	0.00000
435522E-13	9.00000	.27205E+00	0.00000	68942E-03	0.00000	.16689L+00	0.00000	38033E-13	0.00000	.24769E-13	0.00000_
-403636-13	9.00000	27205E+00	0.00000	68942E-03	0.00000	*10689E+00	0.00000	~18742E-13	0.00000.	.43627L-15	0.00000
342578-14	0.00000	221,93E+00	0.00000	10864E-01	0,00000	13600t+00	0.00000	.19631E-13	.0.00000	2d752 <u>E-13</u> _	0.00000
·.56561E-14	0.00000	.22193E+00	0.00000	10854E-01	0.00000	130006+00	0.00000	.191641-13	0.00000	.104876-13	0.00000
·•13304E-14	0.00000		0.00000	17,8486-01	0.00000	.52085E-01	0.00000		0.000'0 <u>0</u>	.23496 <u>E-1</u> 3	0.0000
78403E-14	0.00000	05051E-01	0.00000	.17848E-01	0.00000	•52085E-01	0.00000	10871E-13	_0.00000	.26960 <u>E-</u> 13_	0.00000
-85596E-14	`a`.aaaïaa`	185051E-01	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	17848E-01	00000.0	.520858-01	0.00000	-16604E-13		.59279E-14	0.00000
.26325E-13	0.00000	85051E-01	0.00000	17848E-01		52085E-01	_0.00000	.14268E-13		•56697E-14	0.00000
-639702-14	0.00000	221931+00	0.00000	·10864E-01	~0.00000	136006+00	0.00000	30976E-13	_6.0000a0 ¯ -	16331£ - 13 [0.00009
-161350-13	0.00000	.22193E+00	0.00000	.10864E-01	0.00000	13600E+00	0.00000	29942E-13	0.00000	232856-13	0.00000
81881E-14	0.00000	.27205E+00	0.00000	.68942E-03	0.00000	.10689E+00	0.00000	-929771-14	0.00000 -	59659E-13	0.0000
.318115-13	0.00000	27205E+00]	0.03000	68942E-03	~00000°	-16689E+00	0.00000	.98701E-14	0.00000	.25330E-13_	0.00000
•12644£-13	0.00000	215700+00	0.00000	i2501E-01	0.00000	129266+00	0.00000	126635-13	0.00000	.25625c-15	0.00050_
. -22 605E-13	G.00000	215706+00_	0.00000	12501E-01	0.00000	12926E+00	0.00000	13123E-13	_0.00000	.77490E-14.	0.00000
87732E-14	0.00000	.76970E-01,	0.00000	490816-02	_0.00000	.24647£-01	0.00000	· 11413E-13	0.00000	15362L-11	0.0000
·.30938E-13	0.00000	76970E-01	0.00000	.890s1E-02	0.00000	.24647É-01	0.00000	.16220E-13	0.00000	-102756-13	0.00000

		HATURAL	. FKEQUEN	.Y=205683	E+04						
TX Real	FX Imag	TY KEAL	TY IMAG	TZ KĒĀL	TZ I HAG	KF A L K X	RX IHAG	RY	HAG	RZ KEAL _	RZ IHAG
.32840E-13	0.00000	41038E-01	0.00000	.435996-02	0.00000	11944E-01	0.00000	106196-13	_o• ôoooo	919816-14	0.00000_
-1781oE-13	0.00900	.4103dE-01	0.00000	.435998-02	0.00000	11344L-01	0,• 00000	.33577E-14	n*00000	29948E_14	_ 0.00000_
.160791-13	0.00000	.125300+00	0.00000	79334E-02	0.00000	.64334E-01	0.00000	74487E-14	0.00000	3702de-13	· o. 00000
123275-11	0.00000	12>30++00	0.00000	79334E-02	0.00000	.643846-01	0.00000	103721-13	U.00000	24u68c-13	""๑.อิบออิง"
40262E-14	0.00000	14778E+00"	0.00000		_ 0.00000	10342E+00	0.00000	.22047L-13	0.00000	.75055E-14	0.00000_
.22031E-13	0.00000	.19778E+00	0.00000	~60912E-02	0.00000	10342E+00	0.00000	.31748E-13			• <u>0•0</u> 0000
.903d3E-14	0.99000	.25043c+60	0.0000	38382E-02	0.20000	.13087L+00	0.30000	1/025E-13	0.00000	2491dt-13	3 0.00003_
177654-13	0.00000	25 <u>0</u> 491+00	0.00000	<u>-</u> -38383E-05	_0*00.00	_ 13087E+00	.0.00000	17966E-13		-59478E-1	4 0.00030
						14532E+00	0.00000		_0.00000	.46750E-1	4 0.00000
*11997E=13		.278201+00				14532£+00				12602 <u>r_</u> -1	
.11076E-13	0.00000	.27820±+00	0.00000	.13205E-02	0.00000	.14532E+00	0.00009	106306-13	0.00090	32864 <u>E</u> _1	40*_630000_
85928E-14	0.00000	27820£+00	0.00000	. 13205E-02	<u>0.00000</u>	<u>+</u> 14532 <u>++00</u>	0.00000	- <u>-95791</u> E- <u>14</u>	0.00000	80217E-1	4 0.00000
i0548E-13	0.00000					13087E+00				15251E1	
-115538-13	0.00000	.250431+00		38302E-02				.23591E-13	0.00000	19072E-1	4 _ 0.00000_
.12350F-14	0.00630	.19778E+00	0.00000	.60912E-02	0.00000	.10342E+00	0.00000	18378E-13		.12115t-1	3 0.00000
· 17032E-14	១០០១០០	~19778£+00	000000		00000.0	10 34ZE+00	````````````````	10088É-1	0.00000	14269E-1	4 0.00000
36122E-14	0.00000			79334E-02	0.00000	043846-01	0.0000	13334E-1	0 . 00000	13904E_1	.ă _ o <u>. j</u> ó o <u>o j</u> j
19951E-13	0.00000	.125301+00	0.30000	79334E-02	0.00000	64384E-Ô1	0.00000	12227E-1	a 0.00000	, <u>•19</u> 056£ <u>-</u> 1	30_3000å
42160E-14	0.00000	.4103st-01	0.00000	.43599E-02	0.00000	.11944E-01	0.00000	.11125E-1	0.00000	13050ē-1	5_0.00000
.132178-13	J.09J99	410342-01	0.00000	.435478-02	0.00000	.11944E-01	0.00000	.582188-1	4 0.00000	.15049E-1	.3 0.00000

Mental Mander Street, 14 - 31

APPENDIX H

MODE SHAPES OF THE NATURAL FREQUENCIES FOR THE SPLIT-BEAM

NATURAL FREGUENCY= _ .668129E+02

RX ... RX RY 1HAG RZ THAS REAL -.33831E+00 0.00000 -.11278E-12 0.00000 .13014E-12 0.00000 -16719E-13 0.00000 --15071E-12 0.00000 --10454E+00 0.00000 5-33831E+00 0.00000 -.95724E-13 0.00000 -.11619E-12 0.00000 -.12233E-12 0.00000 -.12233E-12 0.00000 -.10454E+00 0.00000 --13026E+00 0.00000 --12079E-12 0.00000 .15358E-12 0.00000 -.39354L-13 0.00000 -.14340E-12 0.00000 -.98263E-01 0.00000 --13026E+U9 0.00000 --12703E-12 0.00000 -18942E-12 0.00000 --22974E-15 0.00000 --15891E-12 0.00000 --98263E-01 0.00000 -53843E-GL 0.00000 --10571E-LZ 0.00000 -12595E-LZ 0.00000 --19140E-L3 0.00000 --10158E-LZ 0.00000 --78569E-01 0.00000 .53843E-01 0.00000 -.11567E-12 0.60000 ..13111E-12 0.00000 -.21333E-13 0.00000 -.10136E-12 0.00000 -.78569E-01 0.00000 .18333£ +00 _0.00000 _-.121416-12 _0.00000 _.70055E-13 _0.00000 _-.1501E-13 _0.00000 _-.52133E-13 _0.0000 _-.44482E-01 _0.00000 -18333E+00 0.00000 -.12119E-12 0.00000 .72999E-13 0.00000 30601E-14 0.00000 -.60226E-13 0.00000 -.4448ZE-01 0.00000 .23140E+00 _0-00000 -.14202L-12 0.00000 .59322C-13 0.00000 .46184E-14 0.00000 -.20236E-13 0.00000 .15760E-13 0.60000 -23140E+00 0.00000 -.13191E-12 0.00000 .55959E-13 0.00000 -23140E+00 0.00000 -.14165E-12 0.00000 .85078E-13 0.00000 .23140E+00 0.00000 -.13213E-12 0.00000 .71762E-13 0.00000 .34727E-14 0.00000 -.24020E-13 0.00000 .17492E-12 0.00000 -19334E+00 0.00000 -13737L-12 0.00000 .66345E-13 0.00000 -11886E-13 0.00000 -62317E-13 0.00000 4448ZE-01 0.00000 -18333E+90 0.00000 --13076E-12 0.00000 -67510E-13 0.00000 --19026E-13 0.00000 --60672E-13 0.00000 -44482E-01 0.00000 \$53843E-01 0.00000 -14472E-12 0.00000 12633E-13 0.00000 -222284E-13 0.00000 -89674E-13 0.00000 78569E-01 0.00000 -53843E-01 0.00000 -13850E-12 0.00000 -11851E-13 0.00000 -.42649E-13 0.00000 -.87159E-13 0.00000 78569E-01 0.00000 -13026E+00 0.00000 -.1315E-12 0.00000 -.31148E-13 0.00000 -.13883E-13 0.00000 -.16595E-12 0.00000 -.26595E-12 -13026E+00 0.00000 -.156416-12 0.00000 -.27060E+13 0.00000 -.74889E-14 0.00000 -.16459E-12 0.00000 ...98263E-01 0.00000 -33831E+U0 0.00000 -.13010E-12 0.00000 -.42010E-13 0.00000 -.44625E-14 0.00000 -.20394E-12 0.0000 -10454E+00 0.00000 -33831E+00 0.00000 --14949E-12 0.00000 --36979E-13 0.00000 --39404E-14 0.00000 --20442E-12 0.00000 -10454E+00 0.00000

NATURAL FREQUENCY=	115108E+03	

TX TX TY TY TZ TZ RX RX RY RZ RZ RZ RZ REAL IMAG REAL IMAG REAL IMAG REAL IMAG REAL IMAG
-28561E-12 0.0000060966E-01 0.0000032482E+00 0.00000 .88918E-01 0.00000 .25201E-12 0.00000 .13095E-12 0.00000
21446E-12 .0.00000 .80966E-01 0.0000032482E+00 0.00000 .8d918E-01 .0.00000 .22682E-12 0.00000 .10571E-12 0.00000
.4319JE-13 0.0000074478E-01 0.0000013380E+00 0.00000 .87149E-01 0.00000 .1862JE-12 0.00000 .91213E-13 0.00000
-34739E-12 0.00000 .74475E-01 0.00000 -13380E-00 0.00000 .87149E-01 0.00000 .19979E-12 0.00000 .70835E-13 0.00000
=.18760E-12 0.00000 =.58482E-01 0.00000 .46558E-01 0.00000 .72083E-01 0.00000 .12942E-12 0.00000 .79177E-13 0.00000
43326-12 0.00000 .58482E-01 0.00000 .465586-01 0.00000 .72083E-01 0.00000 .11580E-12 0.00000 .39062E-14 0.00000
37662E-12 0.0000032607E-01 0.00000 .17966E+00 0.00000 .42041E-01 0.00000 .46762E-13 0.00000 .71690E-14 0.00000
41510F-12 0.00000 .32607E-01 0.00000 .17966E+00 0.00000 .42041E-01 0.00000 .29894E-13 0.00000 .11014E-13 0.00000
=.23700E-12 0.0000015152E-12 0.00000 .23240E+00 0.0000016767E-12 0.0000041406E-13 0.0000014166E-12 0.00000
46987E-12 0.0000037519E-12 0.00000 .23240E+00 0.00000
1095>E-12 J.0000010162E-12 0.00000 .23240E+00 0.00300
-228656-12 0.00000 -20549E-12 0.00000 -23240E+00 0.00000 .19598E-12 0.00000 -33916E-13 0.00000 .52447E-13 0.00000
.26583E-13 0.00000 .32607L-01 0.00000 .17966E+00 0.0006042041E-01 0.0000015436E-12 0.0000 33202E-14 0.00000
.29056E-12 0.0000032607E-01 0.00000 .17966E+00 0.0000042041E-01 0.0000013468E-12 0.0000062424E-14 0.00000
11671E-12 0.00000 .58482E-01 0.00000 .46558E-01 0.0000072083E-01 0.0000020235E-12 0.0000070247E-13 0.00000
.26047E-12 0.0000058482E-01 0.0000946558E-01 0.0000072083E-01 0.0000072083E-01 0.00000 .22642E-13 0.00000
-35689E-12 0.00000 -74478E-01-0.00000 -13380E+00 0.00000 -87149E-01 0.00000 -28835E-12 0.00000 12593E-12 0.00000 -12593E-12 0.00000
** +07545-12 0 00000 ** 744786-01 0 00000 ** +133K0F+00 0 00000 ** +071495-01 0 00000 0 00000 0 00000 0 00000 0 00000
-14/1/2-12 0.0000 -1/4/10-10 0.0000 11/10-10-10 11/10-10 11/10-10 11/10-10 11/10-10 11/10-10 11/10-10 11/10-10 11/10-10-10 11/10-10-10 11/10-10-10 11/10-10-10 11/10-10-10 11/10-10-10 11/10-10-10 11/10-10-10-10-10-10 11/10-10-10-10-10-10-10-10-10-10-10-10-10-1
64941E-12 0.00000 .80966E-01 0.0000032482E+00 0.0000088918E-01 0.0000035794E-12 0.0000081814E-13 0.0000081814E-13 0.0000033344E-12 0.0000033344E-12 0.0000081814E-13 0.00000

NATURAL FREQUENCY -1406378+03

TX REAL	T K I M A G	TY REAL	TY IMAG	TZ REAL	TZ LHAG	R.A NEAL	RX IMAG	RY REAL	RY 1MAG	RZ	RZIHAG
+.23596E+00	0.00000		0.00000	58598E-13	0.00000	.12967E-13	0.00000	23101E+00	0.00000	97879E-02	~~ ö.00005 <u>~</u>
423596E+0J	0.00000			48481E-i3	0.00000	.203666-13	0.00000	23101E+00	a•_aؤؤؤ <u>ō</u>	<u> 97879È-02</u>	0.00000
20366E+00	J-00000	.21953L-13	0.00000	47705t-13	0.00000	.351586-13	0.00000	å00+3€å00S.∸	"v. 00000	162046-01	0.00000
•20366L+0D	0.00000_	.47614E-13	0.00000	19035E-13	0.00000			20069Ê+00			
14999£+00	0.00000	.32768E-13.	0.00000	<u></u> 23957E-13	0.00000	•		14799E+00			
-14994E+00	U.00000°	.310716-13	0.00000	44383E-13_	0.00000			14799E+00			
811GoE-01				672586-14		65592E-14					
±#1100E-01	0.000001	(.61057E-13)	0.00,000	402388-14	0.00000	45668Ē,-14	0.00000	793228-01	0.000,00		0.0000
						.29530E-14	"o • º º º º º º º º	15003E-15	0.00000	- <u>-16653E</u> -01	3,00003
				.21162b-14							
1665JE-01		524 <u>1</u> 2E-13	0.00000	127796-13		<u>,</u>				ense mag om grejen ja	
1605 JE-01	v.00000 <u> </u>	.56687£-13	0.00000	-81047E-14	0.00000	62059E-14_	0,000,00	11398E-12	0.00000	1665 JE-0	0.00000
81100E-QI	0.00000	.64070È-13	0.00000	228816-13		13108E-13_		79322E-01		251 <u>11E</u> -0	0.00000
8110oE-01	0.00000 -	.57389E-13	0.00000	14674E-13	_0.00000	~.45192E-14	0.00000	.79322E-01	0.000.00		: 0.0000 -
149976+00	_0.00000	.71936E-13	0.00000	14896E-13	0.00000	.13865E-13	0.00000	14799E+00	_ 0.00000		
1499)E+00	_0.00000 _	56915E-13	0.00000	579296-14	0.00000	54571E-Ï5	0.00000	.14799E+00	. 0.00000		1 0.00000
20366E+00	0.00000					16669E-13					
203662+00				~15777É-13							
						13171E+13 90092b-14					
23595£ +00	0.00000	* 24.42.4r ±1.3	0.00000	313036-13	3,00000	4 100 IEE = \$4	,,,,,,,,				, -

MATERIAL	COFULIATE A	. 1534514403

TX REAL	TX TY	TY TZ	TZ IMAG	RX REAL	RK RY KY RZ RZ IMAG REAL IMAG REAL IMAG
+25389£+00	9.00000182746-13	0.00000 .96531E-13	0.00000	.52532E-14	
.25389E+00	0.00000	0.00000 1.14809E-12	~00000	17830a-15	0.00000 .670756-12 0.00000 .154926.00 0.00000
47750E-01	0.00000677598-15	0.00000	0.00000	24348£-13	0.00000 .59703E-12 0.00000 .12594E+00 0.00000
47750E~01	0.00000531646-15	_0.0000013805E-12	0.00000	.415726-13	0.00000 .55634E-12 0.00000 .12594E+00 0.00000
243396+00	0.00000 .337896-13	0.0000036341E-13	0.00000	3J670:-13	0.00000457146-12 0.00000528226-01 0.00000
;•24339E+00	0.0000025280E-13_	0.00000 36603E-13		144,78E-13	0.00000 .40857E-12 0.00000 .52822E-01 0.00000
25630E+00	0.90000 .39257E-13	0.000001877uE-13	0.00000	36728E-13	0.00000 .15347E-12 0.0000036860e-01 0.00003
256306+00	0.00000 .297746-14	.0.0000029621E-13	0.00000	239111-13	0.0000015952E-12 _0.0000036660L-01 _0.00000
97708E-01	.0.00000 .29117E-13	0.0000089227E-13	0.00000	1075 LE-13	0.0000090725E-13 0.0000097708E-01 0.60000
97708E-01	0.00000 .136078-13	0.00000 784246-13	0.00000		
-97708E-01	0.00000 .291521-13	0.0000097947E-13	0.00000		
.97703E-01	0.00000 .11965E-13	0.0000011401£-12		14285E-13	0.0000098762E-13 0.0000097703E-01 0.00000
-25630E+00	0.00000 .17548E-13	0.0000011019E-12	0.00000	.23981E-13	0.0000032113E-12 0.0000036860E-01 0.00000
.25630E+00	0.00000 .28436E-13	0.0000010160E-12	0.00000	.15129E-14	0.0000031538E-12 0.0000036860E-01 0.00009
-24334E+00	0.00000 .464720-14	0.00000656468-13	0.00000	.44767E-13	0.0000042658E-12 0.00000 .52822E-01 0.00000
24339E+00	_0.0000047008E-13	_0_000000532156-13	0,00000	36592Ē-13	3 0.0000043629E-12 0.00000 .52822E-01 0.00000
-47750E-01	0.00000,827256-14	0.0000021020E-13	0.00000	.32463L-13	0.00000507326-12 0.00000 1.125948.00 0.0000
.47750E-01	0.00000 .57548E-13	- 0.00000 .35782E-13	0.00000	•60219E-13	3 0.0000050884E-12 _0.00000 .12594E+00 _0.0000
-+253896+00	U.00J0077791s-14	0.00000 .12405E-12	0.00000	.35338E-13	3 0.0000053198E-12 0.00000 .15492E.00 [0.05000]
253896+00	0.00000 .68390L-13	0.00000 .112446-12	2.00000	.454661~13	3 0.60000521686-12 0.60000154926.00 0.00000

		NATURA	L FREQUEN	CY= .233056	E+03						
. TX REAL	TX IMAG	. TY	TY IMAG	TZ REAL	TZ I HAG	. RX Real	RK I MAG	. RY . REAL .	IHAG	REAL	IMAG
.120548-12	0.00000	-103060+00	0.00000	.23574E+00	0.00000	12953E+00	0.00000	.15304E-12	0.00000 -	~44499E~13	_0.00000
-19768E-12	0.00000	108965.00	0.00000	•23579E+00	_o•ooóōo_	12953E+00	0.00000	.14403E-12	0.00000 -	85854E-13	0000000
.11833E-12	~0.00000°	.87124E-01"	0.00000	50067E-01	~0.00000°	11181E+00	0.00000	.95655E-13	0.00000	• 29080E-13	0.00000
•23848E-13	0.00000	87124E-01	0.00000	500676-01	0.00000	11181E+00	0.00000	•69256E-13	0.00000 -	•54016E-13	
.74272E-13	0.00000	44439E-01	6.00000	,24715E+00	0.00000	50209(-01	0.00000	26504E-£4]	0.00000	-41065 <u>E-11</u>	0.00000
708136-13	0.00000_	44 437E-01	0.00000	24715E+00	0.00000	50209E-01	0.00000	11913E-14_	<u>0.000</u> 00	106198-13	0.00000
.424568-13	0.00000	4d312E-02	0.00000	25628E+00	0.00000	-29481E-01	0.00000	376878-13	_0.00n00	-26488E-13	
-44201E-15	0.00000_	.48312É-02	o , 00000	"-•5299€+00.	0.00000	29481E-01	ō•0000ō	23086E-13		_37 <u>075</u> k-13_	0.00003
.41496E-13	0.00000	37508E-01	_0.0v00 <u>0</u>	83410E-01	_000000	-83410E-01	_0.00000	17565E-13_	0.00000 =	216451-13	0.00000
-85705E-14	0.00000	.37508E-01	0.00000	83410E-01	0.00000						
-10775E-12	0.00000	37503E-01	0.00000	83410E-Q1	0.00000						
				d3410E-01							
-107256-12	0.00000	~.48312E~QZ	0.0000บี	25628E+00°_	0.00000	~~29481E-01	0.00000	59829E-13	0.00000	.16830E-14	0 <u>.0</u> 00000
.57073E-13	0.00000	.48312E-Q2	0.00000	-25628E+00	.o.oooo	=29481E=01	0.00000	[65709E-13]		.324286-13	0.00000
-12692E-12	0.00000	-44439£-01	0.00000	24715E+00	0.00000	50209E-01	ō• òoooo	65214E-13		·17835£-13	000000
•56496E-13	0.00000	444394-01	0'•30000	24715E+00	0.00000	50209E-01	_0.00000	57832E-13	0 .000 000	°5120i€-1 <u>3</u>	0.00000
		- •	•	50067E-01							
:28303E-13	0000000	07124£-01	0.00000	-50007E-01	0.00000	11181E+00	_0.00000	12867E-13	u . 000 00	.260846-13	_0,00000_
.14605E-12	0.00000	.10#96L+0G	0.00000	23577E+00	0.00000	12953t+00	0.00000	.80921E-13	` 0. 00000,	.62689c-13	0.00003_
•13320E-13	0.00000	104066+00	0.00000	23579E+00	0.00000	12953E+00	0.00000	76493E-13	0.00000	.14d46E-14	0.00002

NATURAL FREQUENCY= -252664E+03 TX TX TY TY TZ TZ RX RX RY RY RZ RZ RZ REAL IHAG REAL IHAG REAL IHAG REAL IHAG REAL IHAG REAL IHAG REAL IHAG ~23355E+00 0.00000 -.11666E-13 0.00000 -.12106E-12 0.00000 .48373E-13 0.00000 -21894E+00 0.00000 -31406E-01 0.00000 -23355E+00 0.00000 .72457E-13 0.0000 -13718E-12 0.00000 0.03493E-13 0.0000 0.031406E-01 0.00000 -31406E-01 0.00000 -13305E+00 0.00000 -.64628E-15 0.00000 -.24875E-13 0.00000 .52284E-13 0.00000 .12783E+00 0.00000 .46474E-01 0.00000 -13305E+00 0.00000 ...32822E-13 0.00000 -.29016E-13 0.00000 .27737E-13 0.00000 .12783E+00 0.00000 -.46474E-01 0.00000 --83790E-02 0.00000 --10880E-13 0.00000 .66532E-13 0.00000 .32057E-13 0.00000 --66988E-02 0.00000 -53259E-01 0.00000 [83790E-J2 | 0.00000 | .41036E-13 | 0.00000 | .50437E-13 | 0.00000 | .14144E-13 | 0.00000 | .41036E-02 | 0.00000 | .53259E-01 | 0.00000 -14429E+00 0.00000 -.17324E-14 0.00000 .79246E-13 0.00000 .30743E-14 0.00000 -.13479E+00 0.00000 .39454E-01 0.00000 14427E+00 0.00000 .22571E-14 0.00000 .93364E-13 0.00000 -.29511E-14 0.00000 -.13479E+60 0.00000 -.39454E-01 0.00000 -21393E+00 0.00000 -37603E-15 0.00000 44173E-13 0.00000 -21559E-13 0.00000 -20528E+00 0.00000 34187E-13 0.00000 -21393E+03 0.00000 -.16210E-13 0.00000 .41289E-13 0.00000 --21393E+00 0.00000 -42974E-14 0.00000 -12589E-14 0.00000 21391E+00 0.00000 -17569E-13 0.00000 -74542E-14 0.00000 -21007E-13 0.00000 -2052EE+00 0.00000 34696E-13 0.00000 -.14429E+03 0.00000 -.12850E-13 0.00000 -.67879E-13 0.00000 -.68961E-14 0.00000 -.13479E+00 0.00000 -.39454E-01 0.00000 "".14427E+00 0.00000 -.21341E-13 0.00000 "-.55521E-13 0.00000 +.17462E-13 0.00000 -.13479E+00 0.00000 39454E-01 0.00000 -83790E-02 0.00000 -.38935E-13 0.00000 -.83830E-13 0.00000 .94822E-14 0.00000 -.66988E-02 0.00000 -.57259E-01 0.00000 . 83790E-02 0.00000 -.17697E-13 0.00000 -.73616E-13 0.0000 18396E-13 0.00000 -.86986E-02 0.00000 53259E-01 0.00000 13305E+00 0.00000 -.57124E-13 0.00000 -.84106E-14 0.00000 .39587E-13 0.00000 .12783E+00 0.00000 -.46474E-01 0.00000 -.1330>E+UO 0.00000 -.29182L-14 0.00000 -.33933E-13 0.00000 .32195E-13 0.00000 .12783E+UO 0.00000 .46474E-01 0.00000 ____23355E+00 0.00000 -.66165E-13 0.00000 -.57651E-13 0.00000 .45603E-13 0.00000 .218946+00 0.00000 -.31406E-01 0.00000 -233550000 0.00000 275166-14 0.00000 .689376-13 0.00000 .377656-13 0.00000 .218948+00 0.00000 .314068-01 0.00000

		na tura	L FREGULAC	y= .305250t	.+03						· · · · ·
TX REAL	X X DAHI	TY REAL	T Y I HAG	TZ REAL	IZ IHAG	RX REAL	RX Imag	RY REAL	THAG _	. REAL	
.17055E+00	0.00000	215201-12	0.0000	.48836E-14	0.00000			108708-11		.20595E+00	
•17055E+00		22557E-12	0.00000"	.23008E-13	0.00000						
19774E+u0		1d821E-12	0.00000,_	.93598E-14	0.00000	.91383E-14	0.00000			10711E+00_	
197748+00	0.00000	17385E-12	0.00000	.90410E-14		.25543E-13	0.00000			107 <u>1</u> 16+00	
23536E+00	0.00000	135716-12	0.00000	60705E-14	0.00000					60691E-01	
		130498-12				.1d675t-13				60691E-01	
32839E-01	0.00000	674316-13	0.00000_	.35444E-14	0.00000	53256E-14	0.00000	.266946-12	_0.0000 <u>0</u> _	-12248 <u>6.00</u>	0.00000
-32b3uE-01	0.00000	72893E-13	0.00000	. 25422E-14	. b • 00000	45692E-14	0.00000	76783E-12_	_ 0.00000 <u>0</u>	12248E+00	0.00000
.229718+00							0.00000	./80/16-12	0.00000	.24780E-13	<u> </u>
	0.00000					•					
-229/1E+00	ŏ•00000	.19307E-13	0.00000	34487E-14	0.00000	Same as	0.00000		ີ້ດີ. ດີດ ໂດດີ	1620dE-12	0.00000
	0.00000	.135780-13	0•00000	64917E_1.4	0.00000	52965E-14	_ จิ•ดดดัดัด -	143446-12	` 0.00000	1620dE-12	0.0000
32836E-01	0.000,00	.73858E-13	0.00000	467515-14_	0.00000	. 34/91L-14		-1457E-12	0.00000	12248E+00	0.0000
32838E-01	0.00000	70e70E13	0•005 <u>00</u> _	36870E-14		_ 031235=1 <u>7</u>		33)19E-12	0.00000	-60691E-01	0.00000
23536E+00							0.00000	33631E-12	0.00000	.60691E-01	0.30000_
2353oE+0J		.14437c-12	0.00000	34726E-14	0.00000					10/i1E+ <u>0</u> 0	
			0.00000		ທູ່ ບຸດບຸດ ທີ່ ດຸດດຸດດຸດ	105608-13	0.00000	48983E-12	000000	10711E+00	0.00000
19774E+00				.170456-14	0.00000	423598-14	0.00000	44167E-1Z	0.00000	-,20595 <u>:+0</u> 0_	0.00007
17055E+00		.21761E-12								20595E±00	

NATURAL_FREQUENCY = .324055E+03

TX REAL	TX TY INAG REAL	TY TZ TREAL	TZ _IMAG	RX	RX IHAG	REAL	RY	RZ RÊAL	RZ THÁG
-210788-13	0.00000328276+00	0.00000 .15454E-12	0.00000	57795E-13	0.00000	-45190E-13	_ 0.00000_	7050 <u>eE=13</u>	0.0000
99160E-13	0.0000032827E+00	0.00000 154856-12		63060F_ <u>_</u> _13	0.00000	393 <u>11</u> E-13	0.00000	97536 <u>E-13</u>	0.00000
•91544E-L3	0.00000288688+00	0.0000022701E-12	0.00000	39734E-13	0.00000	1244/E-L4	0.00000	~33259E-13	0.00000
~58351E-13	0.00000Z8868E+00	0.00005 .24630E-12		.45657E-14	0.00000	35207E-1J	0.00000	56325 <u>E-</u> 13	0.00000
•29685E-13	0.0000021426E+00	0.00000150596-12	0.00000	20653t-13	0.00000	44007E-15		59440b-15	0.00000
-67800€-13	0.00000 21426£ 700	0.00000 1.145726-12	_ o•oooo´_	49202E-13		21415E-13	<u></u>	30850E-13	0.00000
- - 68828E-13	.0.0000011401E+00	0.00000127288-12	0.00000	42066E-13	0.00000	34521E-13	0.00000	.568 80E-13	0.00000
.71490E-14	0.00000114011+00	0.00000143038-12	0.00000	71356E-13	0.00000	39784E-13	_ 0.00000_	37205Ē-13	0.00005
118316-12	0.0000040486E-14	0.00000 20643E-12	0.00000	58944E-13	_0.00000	16424E-13	_0.00000	15536E-13	0.00003
90017E-13	0.00000 -679016-13	0.0000020192E-12	000000	ant					
37363E-13	~_0.00000 \ .35887E - 15	0.00000 -192856-12	0.00000	**					
.401750-13	0.00000916838-13	0.00000205396-12	`` <u>`</u> 0•00000_	74216E-13	_ <u>0</u> .000ò <u>0</u>	28680E-13	0.00000	.77720E-14	0.00000
94903E-14	0.00000 ".11401£+00	~ 0.00000` .97564£-13	0.00000	-10978E-12	~°0.0000	Z1072E-Li	0.000000	13198E-13	0.0000
.53724E-13	0.00000 .114016.00	0.00000	_0.00000_	110776- <u>1</u> 2	0.00000	21246E-13		10093E-13	0.00000
•53076E-13	0.00000 .214266+00	0.00000 .305126-12	0.00000	•55832E-14	0.0000		0.00000	3623 JE-13	0.00000
.74618E-13	0.00000 -21426E+00	0.00000 7.316818-12	, 0.00000	38929E-14	0.00000	66546E-14	0.00000	26123 <u>E-</u> 13	0.00000
-513798-13	0.00000 .28868E+00	0.0000018483E-12	_0.00000	131346-12	0.00000	14920E-1	_0.00000	3>857E-13	0.00000
.179o5E-13	0.00000 .288685+00	0.0000020008E-12	0.00,000	12956E-12	0.0000	.52617E-14	U.00000	18485E-13	0.00000
-29317E-13	0.00000 .32827E+00	0.0000022950E-12	0.00000	201308-12	0.00000		``G.00000	.40054E-13	0.00000
,÷,439456E−13	0.00000328276+00	0.0000022705E-12	, 0.00000	218376-12	0.00000	36207E-14	0 • 0.000 0.00	.26636 <u>E</u> -13	0.00000

*	٠
HX	,
Σ	i
•	
•	
Z	
*	

_ NATOR	RAL FREGULNCY= .384,5	72L+03				
TX TX TY REAL IMAG KEAL	TY TZ	TZ IHAG	KX Real	RX RY THAG REAL	THAG	REAL THAS
76092E-13 0.00000 L3198L+00	o_ 0.00000 .ĭ4991E+0	o	16540E+00	0.0000059373E-1	0.000 <u>00</u>	61285E-13 0.00000
		o "o.ooooo -	16540E+00	0.00000 -:80005E-1	_0.00000]_	23200E-13 0.00000
.53983E-14 0.00000 .87323E-01			992658-01	0.0000013005E-1	0.00000	14206E-13 0.00000
58069E-13 0.000008/323E-01			49265Ê-01	0.0000021277E-13	ก•้_0๋.0ฺวงฺ0๋อั	-20461E-13_ 0.00005_
			.31961Ē-01	0.00000 .30251E-1.		61013E-15 0.00000
68645E-13 0.0000020042E-01						.46266E-130.00000_
34450E-13_0.0000016275E-01				0.0000050148E-1	0.00000_	23583E-130.0000 _
15036E-12 0.00000 .16275E-01			.91664E-01	0.00000 .733L3E-1	o. 00000 _	-46646E-14 0.00000
			,55530E-13	0.00000 .477206-1	1 "ñ• òonoo".	.23713E-14 0.00009
- 12943E-13 0.0000074033L-13	3 0.00000 .249761.0	0.00000				
46787E-13 0.0000013430E-16			<i></i> .			
1062dE-13 0.0000017918L-13	3 0.00000 .24976E+8	000000 0	.36782Ê-13	0-00000 "-43051E-1	3 0.000 <u>00</u>	44588E-13 0.0000
630576-13 0.00000 .16275E-0	1 0.00000 -297092-0	0.00000 -	91664E-01	0.0000044731E-I	0.00000	.41761E-13 0.00000
-54170E-13 0.0000010275E-0	1 0.00000 .29709E-0	0.00000	91664E-01_	0.0000049025E-1	30.00000	69256E-14 0.00000
	1 0.0000023758E+0					
14433E-13 0.0000087323c-0	1 0.0000019181846	0.00000	.992656-01		3 0.00000_	49781E-13 0.00000
.16492E-13 0.00000 .87323E-0			.99265E-01	0.0000012201E-1		.19441E-13 0.00000
.10654E-12 0.0000013188E+0		0.00000	.10)40E+00			51237c-13 0.00000
_	0 0.00000 .1499EE+0	00 0.0 0000	.1o540E+00	0.0000u .98103E-1	3_0.00000	.43392E~13 0.00000

		HATURA	F Ł45005W	CY= .407336	£+03			•			
TX REAL	TX IHAG	TY REAL	TY IHAG	TZ Real	TZ I HAG	KX Real	RK IHAG ,	RY Real	THAG	RZ - REAL -	
21324E+U3	0.00000	763346-14	0.00000	251546-13	0.00000	642845-14	0.00000	18405E+00	u • ó0000	76321E-01	0.00000
•21324£+00	0.00000	51135£-14	0.00000	38082E-13	0.00000	665840-14	_0.00000	•		76321E0 <u>1</u>	
-128895-01	0.00000	719876-14	0.00000	48020E-13	0.00000	.828486-14				84010E-01	
12889E-GI	0.00000	.232036-13	0.00000	21631E-13	0.00000	.13208E-13	0.00000	. 80321E-02			_
.2.0422E+00	0.00000	768618-14	0.00000	20531C-13	0.00000	.49495E-14				39319E-0I	
20422E+03	0.00000	21557£-14	0.00000	.54768E-14	0.00000						
20828E+00	0.00000	.15430E-13	_ 0.00000	18842E-13	_ o•ōoooo	73592E-15	o ∙ 00000	18186E+00	0000 <u>0</u> 0	<u>_3</u> 0528E <u>_</u> 0 <u>1</u>	0.00000
20828L+00	0.00000	326168-14	0.00000	.937938-14	0.00000	647676-14	0.00000	- 18186£+00	0.00000	30528±-01	0.03000
52271E-01	0.00000	~ .22474E-14	0.00000	.20424E-14	`0.00000	30580E-14	0.00000	.63014E-13	0.00000	•522716 <u>-01</u>	0.00000
522716-01	0.000,00	84796E-14									
52271E-01				20496E-14						- "::	
52271E-01	0.00000	97443 <u>E-1</u> 4	์ ០∙ ភូ០០ភិក្ខ	13676E-13	0_00000	10443t13	0.00000	-63569E-13	0.000.00	<u>5</u> 227 <u>i</u> E-UI	0.00000
Z0828E+00	.0.00000	.103371-13	_ 0.00000	19512E-13	0.00000	.16408E-13	0.00000	18186E+00	. 0.00000	30258F-01	o.nonini
208286+00	0.00000	826556-14	0.0000	63209E-14		3>385E-14	0.00000	18186E+00	0 • 000000	30528E <u>0</u> 1	0.00000
204226+00			_ 0.00000		_0.00000	15663E-13	0.00000	18I13E+00	0.00000	393 <u>1</u> 9 <u>E_0</u>	C 0.00000
204226+00	0.00000	~1d551E-13	0.00000	11263E-14	0.00000		0.0000	18113E+00	0.00000	.39319E_0;	r _0*00000
- 128896-01	0.00000	-63400Ê-14	0.00000	.21230E-13	_0.00000	13621E-13	0.00000	80321E-02	· 0. 00000	84010F-0	<u>า "ถ∙ักกด์ดี</u>

-12889E-01 0.00000 -.10006E-13 0.00000 .31796E-14 0.00000 -.64755E-14 0.00000 -.80321E-02 0.00000 -.84010E-01 0.00000 -.21324E+00 0.00000 -.40767E-14 0.00000 .43198E-14 0.00000 -.27329E-14 0.00000 -.18405E+00 0.00000 -.76321E-01 0.00000 -.21324E+00 0.00000 -.21239E-13 0.00000 .12353E-13 0.00000 -.61990E-14 0.00000 .18405E+00 0.00000 .76321E-01 0.00000

NATURAL FREQUENCY* .4293636+03
TX TX TY TY TZ TZ RX RX RY RY RZ RZ REAL IMAG REAL IMAG REAL IMAG REAL IMAG REAL IMAG
-11901E+00 0.00000 .40735E-13 0.000007204ZE-14 0.0000053296E-13 0.0000013813E-11 0.00000 -22907E+00 0.00000
-11901E+00 0.0000029395E-13 0.00000 -36285E-11 0.0000062662E-13 0.0000014040E-11 0.0000022907E+00 0.00000
2427oE+00 0.00000 35800E-14 0.00000904525-13 0.0000067069E-13 0.00000 18750E-13 0.00000 556443E-01 0.00000
24276E+U0 0.00000 .19218E-13 0.0000052401E-13 0.00000 .25839E-13 0.00000 .21777E-13 0.00000 .56443E-01 0.60000
82824E-01 0.00000 .20342E-13 0.0000060572E-13 0.00000 .44334E-13 0.00000 .1272TE-11 0.0000013708E+00 0.00000
-82824E-01 0.00000 308416-13 0.0000029792E-11 0.0000031133E-13 0.00000 12637E-11 0.0000013708E+00 0.00000
24933E+00 0.0000022785E-13 0.0000051045E-14 0.00000 \ .80511E-14 0.0000012715E-11 0.0000062697E-01 0.00000
.24933E+00 0.00000 .1366E-13 0.00000 .3471dE-13 0.00000 .34511E-14 0.00000 .12645E-11 0.0000062697E-01 0.00000
-14231E.00 0.00000 .15981E-13 0.00000 .30684E-13 0.0000012630E-13 0.00000 .41906E-14 0.00000 .14231E.00 0.00000
[.14231E+00 0.00000 23688E-14 0.0000020517E-13] 0.00000
14231E+00 0.00000 .16639E-13 0.0000026072E-14 0.00000
14231E+09 0.0000025349E-14 0.00000 13028E-13 0.0000065901E-14 0.00000 .23472E-14 0.00000 .14231E+00 0.00000
2493JE+00 0.0000061531E-14 0.0000021894E-13 0.0000015960E-13 0.0000012200E-11 0.0000062697E-01 0.00000
24933E+00 0.0000028762E-13 0.0000017330E-13 0.00000121414E-14 0.0000012115E-11 0.0000062697E-01 0.00000
82824E-01 0.00000 .31384E-14 0.0000019583E-13 0.00000 .34209E-14 0.0000012261E-11 0.0000013708E+00 0.00000
-82824E-01 0.0000018204E-13 0.0000026705E-13 0.0000030486E-14 0.0000012273E-11 0.0000013708E+00 0.00000 -
.24276E+00 0.0000011882E-13 0.00000 .13646E-14 0.00000 .77059E-14 0.0000067353E-13 0.00000 .56443E-01 0.00000
-24276£+00 0.0000041989E-13 0.6000028044E-14 0.00000 .64924E-14 0.0000062948E-13 0.00000 .56443E-01 0.00000
11901E+00 0.0000015478E,-13 0.00000 .20295E-13 0.00000 .43532L-15 0.00000 .12244E-11 0.00000 .22907E+00 0.00000
11901E+00 0.0000026027E-13 0.0000025530E-13 0.00000 .13611E-14 0.00000 .12182E-11 0.00000 .22907E+00 0.00000

	NATURAL FRED	ULNCY = '50427	2E+03						
TX TX TX	TY TY	TZ REAL	TZ" 1NAG	RX REAL	RX 1 THAG	RY REAL		REAL	ZŞ THAĞ
20518E-12 0.00000	.17153£+00 0.000	00 - 39656E-01	0.00000	18145E+00	0.00000	14170E-12	0.000.00	.14041E-12	0.00000
.71614E-13 0.00000	17153E+00 0.000	0039̃666E÷01	0.00000	18145E+00	0.00000	.97754E-13	0.00000	31525E-13	0.00000
107836-12 0.00000	-11488E+00 0.000	0023721E+00	0.00000	60363E-01	0.00000	78988É-ÎĴ	_ 0.00000	.10517c=12	
,90733E-13 0.00000	11488E+00 0.000	00, 237,21E+00	0.00000	60363E-01	0.00000	41747Ë-13	0.00000	63490E-13	0.00000
.15453E-12 0.00000	.60701E-01 0.000	0ù j - 67233E-01	. 0.000a	.65742E-01	0.00000	12870E-12	0.00000	17456E-13	0.00000
.85911E-13 0.00000	60701E-01 0.000	00 ≟.57233E-01		657426-01	ó.oo'ao'j	12856E-12	~ o. aooooo	1543dE-14	0.0000
29054E-13 0.00000	.723636-01 0.000	00 -241>16+00	0.00000	./d242E-02	0.00000	4013dE-13_	_0,00000.	-169157E-13_	0.00005
17925E-17 0.00000	72363g-01 0.000	002415 <u>1</u> E+00	~ 0.0000 0	.78242L-02	0.00000	37192E-13	0.00000	•45343 <u>E-13</u>	0.00000
101866-12 0.00000	11589E+00~ 0.000	ó <u>0,</u> -13053E+Õò	[0.00000	13053E+00	0.00000	10651E12	_o•øo•øo_	54829L-14	0.00000
61024E-13 U.00000	11589£+Q0 _0.600	00 <u> </u>	0.00000						
656265-13 0.00000	115892 00 0.000	00130536+00		• •				·	
173058-12 0.00000	11587E+00 0.000	0013053E+00		i3053E+00	.0.0000	.10852E-12		.30536E-13	0.00000
85052E-13 0.00000	.72363E-01 0.000	00'24151E+09	_0.00000		0.00000	3680ïE-13	.0.00000	.13123E-13	_0.00000_
11573E-12 0.00000	72363E-01 0.000	00241518+00	ă0000.0	.7d242E-02	0.00000	34590E-13	~00000.0°	405966-13	
125041-12 0.00000	.60701E-01 0.000	0 <u>0</u> 57233E-01	_0.00000	.65742E-01	0.00000	79716E-13	0.00000	44987E-13	0.00000
.10220E-12 0.00000	60701E-01 0.000	0057233E-01	0.00000	.657428-01	_0.00000	79258E-13	0.00000	787386-13	
93133E-14 0.00000	.11488£+00 0.000	00 •23721E+00	.0.00000	60363E-01	0.00000	45699E-13	0.00000	39732£-13	
.10604E-12 0.00000	11488E+00 0.000	00 .23721E+00	0.00000	60363E-01	0.00000	47675E-13	_0.00000	-5593014	0.00000
12649E-12 0.00000	.17153E+00 _ 0.000	00 <u>=</u> .39666E-01	0.00000	181451+00	0.00000	.98640E-13	0.00000	3963 jb-13	0.00000
.93256E-13 0.00000	17153E+00 0.Q00	003966E-01	0.00000	18145E+00	0.00000	.85397E-13	0.05000	.96693E-13	0.00000

NATURAL	FKLOUENCY=	•	.5095741+03
		•	

- TX REAL .	TX THAG	TY	TY Imag	TZ REAL	TZ 1HAG	KX KEAL	XX DAHI	ŘÝ REAL	THAG	RZ REAL	T IHAG
		12292L-12			0.00000	.14720b-12	ó•000ón				
19612E+00	0.00000	.12623E-12	o. 60000	32319E-13	0.00000	13182E-12	0.00000	16009E+0) 0 0 <u>0</u> 0 <u>0</u> 0 0		0.00000
.10960E+00		697796-13								-~.89681E-01	
						[.52282E-13					
23063E+0u						63740E-13					
23063E+00						15158F-13					
						.57449E-14					
•						16047E-13					
1777dE+00	0.00000	67040E-13	0.0000	123498-12	0.00000		0.00000	~ 160'44E +(jó" u. ọòo ợặ <u>"</u>		
-17778E+00	0.00000	. •11175E-12.	0.00000	11200E-12	0.00000	• •					
		862331-13				•	•				
						10296F-ÏZ_					
						15793E-13					
						111890-13					
						602491-13					
					•	71366E-13					
*10960E+00	0.00000	11078E-12	0.00000	19160E-12	0.00000	.41514E-13	0.00000				
10960£+03	0.00000	-78512L-13	0.00000	19373£-12	0.00000	.57097£-13	0.00000			896818-01	
196121+00	0.00000	159115-12	0.00000	-29297E-13	0.00060					.11107E+00	
.19612E+uJ	0.00000	•11776E-12	0.00000	.31547E-13	0.00000	.14652t-12	0.00000	160076+	0.00000	11109E+00	0.00000

Ę
ť

TX	NATURAL FREQUENCY=021946E+03	
.91448E-01 0.0000	TX TX TY TY TZ TZ RX RA RY RY RZ RZ REAL IMAG REAL REAL REAL REAL REAL REAL REAL REAL	<u>G</u>
.22535E+00 0.00000		
.22535E+00 0.000010733E-13 0.00002595E-13 0.0000037585E-14 0.00000 .34581E-12 0.0000040947E-01 0.00000 .31283E-13 0.000002593E-13 0.000005293E-14 0.00000 .253E-12 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.000001098E-00 0.0000020815E-13 0.0000017623E-13 0.0000017628E-13 0.000001784E-12 0.000008003E-13 0.000001098E-00 0.000002099E-00	.51498E-01 0.0000042638E-13 0.0000052578E-13 0.0000010624E-13 0.0000028725E-12 0.00000 .24856E+00 0.00	0000
.18032E+00	22535E+00 0.00000 .6171E-13 0.00000 .26224E-13 0.00000 .25276E-13 0.00000 .34568E-12 0.0000040947E-01 0.00	ก่องกุ๋
.18413E+00 0.000003666LE-13 0.0000026825E-13 0.000002683E-14 0.0000014259E-13 0.0000030887E-12 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+00 0.0000011848E+13 0.0000011848E+10 0.0000011848E	22535E+00 q.6006010733E-13 0.0000025965E-13 0.0000037585E-14 0.00000 .34581E-12 0.0000040947E-01 0.0	<u></u>
-18413E+00	-18032E+00 0.00000 []-31283E-13 0.00000 -27628E-13 0.0000052936E-14 0.00000 -23316E-12 0.0000013098E+00 0.00	<u> </u>
.18413E+00 0.000025829E-13 0.0000020615E-13 0.0000017623E-13 0.0000030402E-12 0.0000080036E-13 0.0000019060E-10 0.0000020070E-10 8032E+00 0.0000036661E-13_0.00000 _57331E-13_0.0000014259E-13_0.0000025036E-12_0.0000013098E+00_0.00	<u>j</u> oo <u>5 0 _</u>	
19060E+00 0.0000	-18413E+00 0.00000 .40611E-13 0.00000 -28867E-14 0.00000 -31645E-13 0.00000 -30887E-12 0.00000 1.11648E+00 70.00	<u>, 0</u> 00 <u>0</u>
19060E+00	.18413E+00 _0.00000250276-13 _0.0000042830E-14 _0.0000017623E-13	00000_
-19060E+00 0.00000 -17498E-13 0.0000094613E-14 0.00000 -19060E+00 0.00000 -14818E-13 0.0000013074E-13 0.00000 -31107E-14 0.0000011591E-12 0.00000 -26451E-12 0.00000 -18413E+00 0.00000 -3628E-13 0.0000027280E-13 0.0000026219E-14 0.00000 -42904E-12 0.0000011848E+00 0.00000 -18032E+00 0.00000 -3528E-13 0.0000010756E-13 0.0000020496E-13 0.00000 -44157E-13 0.00000 -13098E+00 0.00000 -18032E+00 0.0000051466E-14 0.0000012334E-13 0.0000024097E-14 0.00000 -47193E-13 0.00000 -13098E+00 0.00000 -22535E+00 0.0000026182L-13 0.0000028813E-13 0.0000028097L-14 0.0000026993E-12 0.00000 -40947E-01 0.00000 -22535E+00 0.0000074717E-14 0.0000034712E-13 0.000002205E-14 0.0000027355E-12 0.0000040947E-01 0.00000	19060E+00 0.00000 -19016E-13 0.0000020615E-13 0.00000 -94375E-15 0.0000011784E-12 0.0000080036E-13 0.0000	00000
19060E+00	·.19060E+00 0.00000150836-13 _0.0000019344E-13 _ 0.00000	
.18413E+00 0.0000 .14921E-13 0.0000 .22477E-13 0.00000 .12048E-13 0.00000 .42904E-12 0.000011448E+00 0.0000	-19060E · NO 0.0000017408E -13 0.00000946L3E-14 0.00000	
.18413E+00 0.0000036282E-13 0.00000 .27280E-13 0.0000026219E-14 0.00000 .42073E-12 0.0000011848E+00 0.00000 0.00000 .13539E+13 0.0000010756E-13 0.0000020496E-13 0.00000 .44157E-13 0.00000 .13698E+00 0.00000 .13698E+00 0.000002834E-13 0.0000028697L-14 0.00000 .47193E-13 0.00000 .13698E+00 0.00000 .13698E+00 0.00000 .13698E+00 0.00000 .22535E+00 0.0000026182L-13 0.0000028813E-13 0.00000 .61401E-15 0.0000026993E-12 0.00000 .40947E-01 0.00000 .22535E+00 0.0000074717E-14 0.0000034712E-13 0.00000 .22205E-14 0.0000027355E-12 0.00000 .40947E-01 0.00000	19060E+00 0.00000 F.14818E-13 0.00000 F.13074E-13 0.00000 F.1107E-14 0.00000 F.11591E-12 0.00000 F.26451E-12 0.00000	00050
.18032E.00 0.00000 .13539E-13 0.0000010756E-13 0.0000020496E-13 0.00000 .44157E-13 0.00000 .13698E.00 0.00000 .13698E.00 0.0000012334E-13 0.0000026097L-14 0.00000 .47193E-13 0.00000 .13098E.00 0.0000026182L-13 0.0000028813E-13 0.00000 .61401E-15 0.0000026993E-12 0.00000 .40947E-01 0.0000022535E+00 0.0000074717E-14 0.0000034712E-13 0.00000 .22205E-14 0.0000027355E-12 0.00000 .40947E-01 0.00000	.18413E+00 0.00000 .14921E-13 0.00000 .22477E-13 0.00000 .12048E-13 0.00000 .42904E-12 0.000001148E+00 0.000	00000
.18032E+00 0.0000051466E-14 0.0000012334E-13 0.0000028097L-14 0.00000 .47193E-13 0.00000 .13098E+00 0.0000026182L-13 0.0000028813E-13 0.00000 .61401E-15 0.0000026993E-12 0.00000 .40947E-01 0.0000022535E+00 0.0000074717E-14 0.0000034712E-13 0.00000 .22205E-14 0.0000027355E-12 0.00000 .40947E-01 0.00000	.18413E+00 0.000003628ZE-13 0.00000 .27Z80E-13 0.0000026219E-14 0.00000 .42073E-12 0.0000011848E+00 0.0	00000
22535E+00 0.0000026182L-13 0.0000028813E-13 0.00000 .61401E-15 0.0000026993E-12 0.00000 .40947E-01 0.0000022535E+00 0.0000074717E-14 0.0000034712E-13 0.00000 .22205E-14 0.0000027355E-12 0.0000040947E-01 0.00000	•18032E•09 0.00000 .13538E-13 0.0000010756E-13 0.0000020496E-13 0.00000 -44157E-13 0.00000 .13698E+00 0.0	0.0000
22535E+00 0.0000074717E-14 0.0000034712E-13 0.00000 .22205E-14 0.0000027355E-12 0.0000040947E-01 0.00000	.18032E+00 0.0000051466E-14 0.0000012334E-13 0.000002d097L-14 0.00000 .47193E-13 0.00000 .13098E+00 _0.4	บอดอด
	22535E+00 0.0000026182L-13 0.0000028813E-13 0.00000 .61401E-15 0.0000026993E-12 0.0000040947E-01 _0.00000	ก่องอัง
	22535E+00 0.0000074717E-14 0.0000034712E-13 0.00000 .22205E-14 0.0000027355E-12 0.00000 .40947E-01 0.00000	0000
.51498E-01 0.0000020392E-13 0.00000 .32048E-13 0.00000 .32134E-13 0.00000 .53895E-13 0.0000024456E+00 0.00000	.51498E-01 0.0000020392E-13 0.00000 .32048E-13 0.00000 .32134E-13 0.00000 .53895E-13 0.0000024656E+00 0.00	00000
.51498E-01 0.00000 .58241E-14 0.00000 .33227E-13 0.00000 .23461E-13 0.00000 .44663E-13 0.0000024856E+00 0.00000	.51498E-01 0.00000 .50241E-14 0.00000 .33227E-13 0.00000 .23461E-13 0.00000 .44663E-13 0.00000 -24856E+00 0.00	00000

			•
NATURAL, FREQUE	NCÝ=	.576674E+	03

NATURAL FREUUENCÝ= 576674E+03
TX TX TY TY TZ TZ RX RX RY RZ RZ REAL THAG REAL THAG REAL THAG REAL THAG REAL THAG
-86448E-14 0.0000030075±+00 0.0000060498E-13 0.0000014687E-13 0.0000024803E-13 0.0000048916E-13 0.00000
39882E-14 0.00000 .30075E+08 0.0000008100E-13 0.000001956be-13 0.0000031324E-14 0.0000028752E-13 0.00000
.20220E-13 0.00000 .10587E+00 0.0000070553E-14 0.00000 .37128E-13 0.00000 .19176E-13 0.00000 .16587E-13 0.00000
28673E-13 0.00000 18587E+00 0.00000 -28931E-13 0.00000 87174E-14 0.00000 64763E-14 0.00000 47550E-14 0.00000
.33845E-14 0.00000 .43743E-13 0.00000 .33177E-13 0.0000068413E-14 0.00000 _99123E-14 0.0000021308E-14 0.00000
.38259£-13 0.0000097780E-14 0.00000 .24732E-13 0.0000011153E-13 0.0000069902Ê-15 0.0000020432E-14 0.00003
.262b9E-13 0.0000018587E+00 0.000009194bE-15 0.0000018592E-13 0.0000025159E-13 0.0000013673E-13 0.00000
.38518E-13 0.0000018587E+00 0.0000076673E-14 0.0000011905E-13 0.0000012376E-14 0.0000022887E-13 0.00000
.13577E-13 0.0000030075L+00 0.00000 .48338E-15 0.00000 .27359E-13 0.0000018219E-13 0.00000 .17469E-13 0.00000
.57323E-13 0.0000030075E.00 0.00000 1.13553E-13 0.00000
13182[-13 0.0000030075E+00 0.0000064375E-13 0.00000
28308E-13 0.0000030075E+00 0.00000 3-06741E-13 0.00000 222098E-13 0.00000 3-25769E-13 0.00000 311624E-13 0.00000
.62977E-14 0,0000018587E+00 0.00000 .17590E-12 0.0000013660E-13 0.00000 .17088E-13 0.00000 .67176E-15 0.00000
.71707E-11 0.0000018587E+00 0.0000014955E-12 0.0000047487E-14 0.00000 .83072E-14 0.00000 .12047E-13 0.00000
-77179E-14 0.0000025285C-13 0.0000024652E-13 0.0000062852E-13 0.0000018200E-14 0.0000078159E-14 0.00000
.13815E-13 0.00000 .54927E-13 0.0000016196E-13 0.0000042639E-13 0.0000015841E-14 0.0000024544E-13 0.00000
.16757E-13 0.00000 .18587E+00 0.0000022373E-12 0.00000 .43544E-13 0.00000 .24157E-14 0.00000 .59642E-14 0.00000
\$504000-13 0.00000 .185876+00 0.00000224986-12 0.00000 .524636-13 0.00000 .11951E-13 0.00000 .82578E-14 0.00000
.39272E-14 0.00000 .30075E+00 0.00000 .57494E-13 0.00000 .17875E-12 0.00000 .11324E-13 0.0000031477€-13 0.00000
.1820/E-13 0.00000 .30075E+00 0.00000 .46860E-13 0.00000 .13910E-12 0.00000 .21068E-13 0.00000 .32236E-14 _0.0000

· · · · · · · · · · · · · · · · · · ·	RAE FREQUENCY	- ,,						
TX TX TY TY	TY TZ	L TZ	RX KEAL	RX THAG	RY	I HĄG	KEAL	RZ IMAĞ
.13646E-13 0.00000 .23417E+0	-							0.00000
-33662E-13 0.00000 23417E+0	0 0.00000 7665	<u>e_o† </u>	17911E+00	0.00000	55861E-13	0.00000	.43155E-13	0.00000
~.18685E-13 0.0000015599L+0	0 0.000001494	7E+00 ~ 0+00000	719656-02	0.00000	.32677E-14	0.00000	.12407E-13	0.00000
-11016E-13 0.0000015599E+0	0 0.00000 1494	7E-00 0.00000	71965E-02	0.00000	15390E-13	_0.00000	27690E-14	0.00000
	1 _ 0 . 000000 2004	8E+000.00000	•223556-01	0.00000	57223E-14_	0.000000	19848E-13	0.00000
16514E-13 0.0000099824E-0	1 0.60000 -2004	86+00 0.00000	•22355E-01	0.00000	22916E-13	0.00000	19769E-13	0.00000
14354E-13 0.00000 .75571E-0	0.00000	4É+90 0.00000	97273E-01	0.00000	28573E-13	_o•óòōò; _	10304 <u>5</u> -1 <u>3</u>	0.0000
.8141a6-14 0.0000075571E-0							,	
72936E-13 0.0000025555E-1	2 0.000001378	9E+00 0.00000	10694E-12	0.00000	.12222E-13	0.0000	13240E-13	<u>0</u> • <u>0</u> 0000_
12397E-13 0.0000079437E-1	3_0.00,0001378	AE+00 0.00000						
40001E-13 0.0000023494E-1	2 0.000001378	(9E+00, , , , , , , , , , , , , , , , , , ,)					
2858iE-13 0.00000 .90579E-1							.57904E-14	
	1 0.00000 1.1635	4E+00, 0.00000	972736-01	0.00000	77051E-14	_0.00000	26637E-13	0.00000
75571E-0								•
33360E-13y.000009/824E-0	0.00000200	49Έ+00 <u></u> 0,€00000	22355E-01	_0*00000		0.00000	.30330E-14	0.00000
10204C-13 0.00000 799824E-0								
-71051E-14 0.00000015599E+0								
17620E-13 0.00000 15599E+0	- • • • • • • • • • • • • • • • • • • •							
20862E-13 0.00000]23417E+0								
-47128E-13 0.00000 -23417E+0	0.00000766	2.00000	0+17911E+00	_o.oōoóò	11950E-1 <u>3</u>	<u>_0.00000</u>	40207E-13	<u> </u>

MATURAL FREQUENCY= .667464E+03 RY RZ REAL IMAG IHAG .64468E-13 0.00000 .10980E+00 0.00000 .15409E+00 0.00000 .16389E-13 0.00000 114679E+00 0.00000 -.74219E-13 0.00000 .61581E-13 0.00000 .10980E+00 0.00000 -.15409E+00 0.00003 -14679E+00 0.00000 .39866E-13 0.00000 .51664E-14 0.00000 .10469t-13 0.00000 -.16732E+00 0.00000 .50934t-01 0.00000 -21155E+00 0.00000 --46053L-13 0.00000 -86751E-13 0.00000 .73145E-14 0.00000 -.16732E+00 0.00000 -.50934E-01 0.00000 -21155E+00 0.00000 ".17456E-13 0.00000 ".77511E-13 0.00000" .73664E-01 0.00000 -.45175E-13 0.00000 -.24619E-13 0.00000 -.22497E-13 0.00000 -.58085E-01 0.00000 -.10300E+00 0.00000 .12433E-13 0.00000 _-.21833E-13 0.00000 -.15739E-13 0.00000 -.58085E-01 0.00000 .10300E+00 0.00000 .12005E-13 0.00000 .18596E+00 0.00000 -.37264E-01 0.00000 .23531E+00 0.00000 -.23221E-13 0.00000 -.68727E-13 0.00000 -235311+00 0.00000 .238321-13 0.00000 -.692426-13 0.00000 .210581-13 0.00000 .18596E+00 0.00000 .37264E-01 0.00000 .14984E-13 0.00000 -.58575E-13 0.00000 .87815E-01 0.00000 .87815E-01 0.00000 -.68162E-14 0.00000 -26267E-14 0.00000 .23473E-13 0.00000 -.50156E-14 0.00000 .87815E-01 0.00000 .87815E-01 0.00000 -.66474E-14 0.00000 .27910E-13 0.00000 .87815E-01 0.00000 .23499E-13 0.60000 .27457E-13 0.00000 .12718E-13 0.00000 -.63996E-13 0.00000 -.87815E-01 0.00000 .36043E-13 0.00000 -.11806E-13 0.00000 .56647E-14 0.00000 -.18596E+00 0.00000 -.37264E-01 0.00000 .23531E+00 0.00000 -.78545E-14 0.00000 -.19445E-13 0.00000 -.17571E-13 0.00000 -.18596E+00 0.00000 -37264E-01 0.00000 .29595E-13 0.00000 -.47831E-13 0.00000 .13772E-13 0.00000 .58085E-01 0.00000 -.10300E+00 0.00000 .73663E-01 0.00000 -73668E-01 0.00000 -.68446E-14 0.00000 -.40160E-13 0.00000 -.28472E-14 0.00000 .58085E-01 0.00000 10300E+00 0.00000 -2115>E+00 0.00000 -39218E-13 0.00000 -30130E-13 0.00000 -.11097E-13 0.00000 .16732E+00 0.00000 .50934E-01 0.00000 221155E+00 0.00000 -.24804E-13 0.00000 -28757E-13 0.00000 -.83111E-14 0.00000 .16732E+00 0.00000 -.50934E-01 0.00000 .14679E+00 0.00000 .57784E-13 0.00000 .16858E-13 0.00000 -.35395E-13 0.00000 -.10980E+00 0.00000 .15409E+00 0.00000 -14679E+00 0.00000 -.50073E-13 0.00000 .15338E-13 0.00000 -.30279E-13 0.00000 -.10980E+00 0.00000 -.15409E+00 0.00000

	11, 23, 11, 21, 11, 11, 11, 11, 11, 11, 11, 11		-						
TX TX	TY TÝ	REAL	I I DAMI	RX	RX'	RY	RY IHAG	₹Z KÉAL	RZ 1 MAG
123636-12 0.00000	012503E+000.000	00 186976+00	0.00000	12634E-01	0.00000	84217E-13	0.00000	80421E-13	0.00000
*13630E-12 0.00000	12503E+00 0.000	0018697E+00		12634E-01	_q.00000 <u>_</u>	13061E-12	0.00200	.19289E-12	0.00000
.10535E-12 0.00000	15386L+00 0.000	00 .10112E+00		~.58393Ë-02.	_0.00000 <u>_</u>	+15564E-12	0.00000	320136-13	0.00000
.23633E-12 0.00000	15386E+00 0.000	00 . TOTISE +00	0.00000	~.5d393E-02	0.00000	~ .11539E-12	0.00000	.44237E-13	0.00000
-88622E-13 0.0000	. 20402E+00_ 0.000	0092495E-01	0.00000	13195E+00		.65231E- <u>1</u> 3	0.00000	.42964E-13	0.00000
.55123E-13 0.000Ô0	20402E+00 0.000	00 924956-01		13195E+00	0.00000	29134E-13	0.00000_	118446-12	<u></u>
\$14561E-12 0.00000	20038E+000.000	00 <u>-</u> 15156E+00	[0.00000]	io2126+0ò	_0.00000_	18507E-12		49429E-13	0.00000
.21870E-12 0.00000	20038E+000.000	0015156E+00		To212£+00	0.0000		<u>0.</u> 000 <u>00</u>	30678E-14	<u> </u>
-91554E-13 0.00000	.16206E+00 0.000	0017825E-01	_0.00000_	.17825E-01	0.00000	347316-13	0.00000	57543t-13	0.00000
.654362-13 0.00000	16206E+000.000	00178255-01	0.00000						
-6906sE-11 0.000go	.162066.00.000	00 -17825E-01	_0.00000						
71691E-13 0.00000	1º50ef +00 . 0 °000	00 .17825E-01	000000		0.00000	134138-13	0.00000	.51564c-13	0.00000
-24633E-12 0.00000		00 -15156£+00	0,00000	10212E+00		-17007E-12	0.00000	.57212E-13	0.00003
19176E-12 0.00000	2003dE+00 0.000	00 .15156E+00	[0.00000	10212E+00	0.00000	.18ó15E-i2	0.00000	223366-13	0.00000
.70929E-13 0.00000	2040 <u>2E+000.000</u>	00 <u>"92495</u> 5-01	_`o`ooo`oo_	13195E+00	_0.00000	51573E-13	0.00000	-94038E-13	0.00000
.299508-13 0.00000	20402E+00 0.000	0092495E-01		13195E+00	0.00000	~~.57065Ë-13	0.00000	85675E-13	0.00000
-17500E-12 0.00000	15386£ .00, _0.000	00010i12 <u>E</u> +00	_0.00000	58393E-02	0.00000	13681E-12	0.00000	20219E-13	0.00000
.17361E-12 0.00000	15386E+00 0.000	0010112E+00	0.00000	58393E-02	້ ວິ.ວວວວົນ	15662E-12	,0.00000	.40207E-13	0.0000
13465E-12 5.00000	,.125036+00,0.000	18697£+20	0.00000		0.00000	.11244E-12			0.0000

NATURAL FREQUENCY - 657913E+03

NA TURAL	FREQUENCY=	.7464848+03

TX REAL	TX	. TY .	TY IMAG	T/ REAL	T Z I MAG	R X REAL	R.K IHAG	RY REAL	RY	RZ RZ REAL IMAG
12239E-01	0.00000	.14906E-13	0.00000	51851E-13	_0.00000 <u>0</u>	.37961E-13	0.00000	23456E-12.	<u> </u>	25843 <u>e.00 0.0000</u>
12239E-01	0.00000	.148966-13	0.00000	53616E-13	0.00000	.17454E-13	0.00000	304798-12	_0.000000	25843£+00 0.00000
.17402E+00	0.00000	.59213E-13	0.00000	.50088E-13	0.00000	.93059E-14	0.00000	44834E-12	0.00000	-95880E-01 0.00000
•17402E+00	0.00000	~.51299E-13	0.00000	29941É-14	0.00000	357936-13	0.00000	51282E-12	0.00000	95880£-01 0.00000
27552E+00	0.00000	.7496JE-14	0.00000	.54271E-14	0.00000	21482E-13	0.00000	.1203¤E-12	0.00000	-40324E-01 0.00000
27552E+00	0.00000	32194E-13	0.00000	35227E-13	0.00000	23560E-L3	0.00000	135136-12	û.000 ao "	.403246-01 0.00000
.63539E-01	0.00000	54395E-14	0.00000	68947E-14	0.00000	.139816-13	0.00000	.38108E-12	0.00200	12909E+00 0.02000
-63539E-01	0.00000	21357E-13	0.00000	35810E-14	0.00000	.10974E-13	0.00000	-36843E-12	~ 000 óọ_	15909£+00 0.00000
.15993E+00	0.00000	228468-13	0.00000	.62985E-13	0.00000	48546E-14	0.00000	31278E-12	0.000,00_	154936.00 0.00000
15993E+00	0.00000	81335E-14	_0.00000	57248E-13	. 0.00000					
	0.00000									
=:15993E+00	0,00000									.15993E+00 0.00003
<u>-</u> .63539E-01	0.00000	40179E-13	0.00000	62480E-13_	0-00000	87267E-14	0.00000		_0*00000	159096+00 0.00000
=-63539E-01	0.00000	.3305ÖE-1Ï3	0.00000	``-•59095E-13	000000	14965E-13	_0.00000 <u>_</u>	.37070E-12	0.000.00	15909E+00 0.00000
.27552E+00	0.00000	60635E-13	0.00000	12369E-13	0.00000	-19616E-13	0.00000	•Í8315E-15	0.00000	.40324E-01 0.00000_
-27552E+00	0.00000	•e1305E-13	0.00000	18679E-13	0.00000	269358-13	0.00000	19331E-12	0.00000	40324E-01 0.00000
=.17402E+00	0.00000	~~. 41279E-1,3	_0.00000	-48400E-13	0.00000	17217E-14		38009E-12	<u>, jō•</u> aoʻno <u>jo</u>	.95880E-01 0.00000
17402E+00	0.00000	.540411-13	0.00000	.50521E-13	0.00000	70394L-14	0.00000	38374E-12	0.00000	.95380E-01 0.00000 _
.12239E-01	0.00000	195376-13	0.00000	42773E-13	0.00000	226986-14	0.00000	.14832E-12	0.00000	25843E+00 0.00000]_
1223 PE-01	0.00000	39615E-13	0.00000	37139E-13	0.00000	31256t+14	0.00000	14608E12	``o•oōñōó	25843E+00 0.00000

TX TY TY TY THAG REAL IHAG	TZ REAL	TZ IHAG	RX Keal	RX IHAG	RY REAL	YY RZ RZ IMAG REAL IMAG
.45345E-14 0.00000 .12978E+00 0.00000	-,19132L+00	0.00000	•52269E=01	0.00000	27400E-14	0.00000 .250746-13 0.00000
-36492E-14 0.0000012978E+00 0.00000		0.00000	~~.52269E-01	0.00000	19079E-13	0.00000 .54987E-13 0.00000
\$30979E-14 0:00020 .16471E+00 0:00000	.2043840\$	0.00000	33167E-01	0.0000	.32543E-13	0.00000 .195154-13 .00000
-29467E-13 0.0000016471E+00 0.00000	-20863E+00	0.00000	33167E-01	0.00000	.80492E-14	0.00000143498-13 0.00000
-41576E-13 0.00000 .17823E+00 0.00000	16535E-01.	0.00000	15749E+00	0.00000	26191E-13	0.00000946026-14 0.00000
-68445E-13 0.0000017823E+00 0.00000	16535E-01	0.00000	15749E+00	0.00000	65467E-13	0.0000031817E-14 0.00000
.61767E-13 0.00000 .88189E-01 0.00000	17327E+00	0• 00000	.23950E-02	0.00000	.33323E-13	_0.0000011416E-140.00000
-36455E-13 0.0000088189E-01 0.00000	173276+00	0.00000	-23950E-02	0.00000	• 35655E-13 _.	0.0000000 491896-13 20,000000
.2156JE-13 0.00000 7.229326-12 70.00000	".17245E+00"	0.00000	41417E-13	0.00000	24818E-13	0.00000 .238316-13 0.00000
:.47630E-11 0.0000016695E-12 0.00000	•1/245E+00	0.00000				
24417E-13	.17245E+00	0.00000	• •			
.66018-13 0.00000166618-12 0.00000	-17245E+00		,37322E- <u>13</u>	0. 00000_	46782E-13	0.0000058848E-13 0.00000
	1,732_15,00	0.00000	239506-02	0.00000	30201E-13	0.00000 .516434-14 0.00033
-74814E-13 0.00000 88189E-01 0.00000	17327E+00	0.00000	23950E-02	``0•0000_	25026E-13	0.00000 .48670E-13 0.00000
.51493E-14 0.0000017823E+00 0.00000	16535E-01	'_ò.00000 .	. 1.5749E+00	0.00000_	29396E-13	0.00000
-11416E-12 0.00000 11/823E+00 0.00000	16535E-01	~ Ø.000òō	-15749E+00	0.00000	53379'E-L3"	0.000,00 .79246E-14 0.00000
-111197E-13 0.00000 -116471E+00 0.00000	208648+00	, o. oo oo o	_ +33167E-01_	0.00000		0.0000015440e-13 0.00000
.435Z2E-13 0.00000164712+00 _0.00000	- 20864 <u>2</u> +00	_0.00000	331676-01	_ 0.00000_	81479E-14	0.000001048dE-13 0.00000
.22346E-13 0.0000012978L.00 0.00000	19132E+00	0.00000	52269E-01	0.00000	56598E-13	0.00000 .43922E-13 0.0000
.181816-11 0.00000 12978L+00 0.00000	19132E+00	0.000000	,522696-01	0.0000_	-27089E-13	U. 000 00 60404E-13 0.0000

"NATURAL	FREQUENCY	.767238E+03
NAIUKAL	FKEUULNUT=	*1017306*0

TX REAL	TX IHAG	TY	TY	TZ	TZ .	R X RE AL	RÆ IMAG	RY REAL	LHAG	RZ RZ	RZ IMAG
11308E+00	0.00000	320158-13	0.00000	18766L-13	0.00000	.36119L-13	0,00000	78687E-01	_ a. oón ao	17268£÷00	0.00000
_i130at+00	0.00000	.97524E-14	0.40000	30934E-13	0.00000	.30607E-13	0.00000	78689É-01		.17268E+00	0.00000
+23103E+00	0.00000	124894~13_	ិច•ពភិច្ចច	.45918E-13	0.00000	12916E-14		18184E+00			
23163E+00	0.00000	- <u>+</u> 37030E-13	0.00000	56303E-13	0.00000	.141186-13		-18184E+0Ö			
-75811E-01	. 0° 00 00 00	~ 29268£-13	. 0 <u>. 00 000</u> _	37198E-13	_o.aoooo	14632b-13	0.00000	7185TE_01	_0.000 <u>00</u>	.10514E+00	0.00000
.75811£-01	0.00000	388446-13	0.00000	47540E-13	0.00000	_84735b-14	0.00000	71851E-01	0.00000	10514E+00	0.00000_
19004E+00	0.00000	~.37721E-13	0.00000	-•21797E-13	0.00000	.23529E-13	0.00000	10882£+00	0.00000	55475E-01	0.00000
-19004E+00	0.00000	34593 <u>E</u> -13_	0.00000	759736-14	0.00000	124116-13	_o+o√óōo	16885E+00	_ 0.00000_	55475E-01	0.0000
-14730E+00	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	.59157E-13	0.00000	.44433E-13	_0.00000	28104E-13	0.00000	•13755E+00	0.00000	.21577E-12	0.00000
14730E+0J	_ñ•00ñ0ō	219241-13	0.00000	27808E-1J	_û•000 <u>0</u> 0						
				10584E-13							
<u></u> 14730E+00				33941E-14							
190048+00				68192E-14							
				125166-13							
				52865E-13							
				- `.52773E-13							
				41102E-14							
23163E+00	0.00000	.21158E-13	0.00000	46895E-14	_0.00000	50943E-14		18184E+00	0.00000	94522E-02	0.00000
11308E+Ju	0.00000	631340-13	0.00000	427356-13	0.00000			- - 78689E - 01			
•11308E+09	0.00000	.32820t-13	0.00000	40233E-13	0.00000	.156502-13	0.0000	78689E-01	_u_00000	17268E+00	0.0000

ROCH
\$6 PHISOR
POSSITIL I
¥
¥

		1141,000		*******	E; 42						
TX REAL	TX Imag .	. TY REAL	TY	TZ REAL :	TZ ITAG	RX Real .	RX IMAG	RY REAL	THAG	REAL	RZ THAG
-189558-13	0.00000	20116E+00	0.05000 ~~	-43425E-01	0.00000	.17456È+00	0.00000	24274E-13	0.00000	.7707[E=13	0.00000
E-33234E-13	0.00000	.201166+00	0.00000	434256-01	0.00000	+17456E+00	0.00000	.460658-13	0.00000	41094E-14	0.00000
==44830E-13	0.00000	77023E-01	0.00000	~93062É-0Ī	0.0000-0	32350E-01	0.00000	48307E-13	0.00000	249542-13	0.00000
174C8E-13	0.00000	.77023E-01	0.00000	.93062E-01	0.00000	32350E-01	0.00000	-165199E-13	9-00.000	5g574E-14	0.00000
-20204E-13	0.00000	.29088E-01	0.00000	• 26056E • 00	0.00060	30303E-01	0.00000	.41781E-15	0.00000	23499e-13 <u></u>	[0.00000]
-63163E-13	0.00000	290886-01	0.00000 -	.2605uE+00	0.00000	30303E-01	0.00000	.21108E-13	0.00000	32219E-13_	<u></u>
50403E-13	0.00000	.11390E+00	0.00000	-11908Ê-01	0.00000	+3d266E-01	0.00000_		0.00000	142336-13	0.00000_
- -91949E-13	0-00000	11370E+00	`@.0600 <u>0</u>	.1190aE-o£	0.00000	-38266E-01	0.00000	.71464E-13	0.00000	11643 ₆ -13	0.0000
i2395E-13	0.00000 <u>_</u>		0.00000	-14465E+00		14465t+00	0.00000	<u>650936-13</u>	0.00000	.16226k-13	0.00000
15843E-13	0.00000	-:21905E+00	0.00000	.14465E+00	0.00000	··					
F-209716-13	0.00000	~.21905E+00	0.00000	·14455E+00	0.00060	• •					
_99363E-13	0•00000	*\$1A02F+00,	0.00000	- <u>.]</u> 4465 <u>E</u> +00	_0.00000_ 0.00000	14465EF00	0.000000	46770E-13	00000	7.12516E-13	0.00000
_18775E-13	<u></u>	.11390L+00`	0.00000	1190åE-01		38266E-01	0.00000	-41524E-13	ō. 00 0 0 0	10328E-14	0.0000
=-96952E-13	0.00000	11390(+00	0.00000	.11908E-01	, o. 00000°	-34266E-01	0.00000	.46802E-13	ŏ•0000ŏ	.449416-13	0.00000
25209E-13_		. 29088E-QT	0.00000	<u>. Z</u> <u>6</u> 05.6E.00		30303E-01	_0.00000		<u></u>	306124-13	0.00000
=.23472E-13	0.00000]29038E-01	0.00000.	.26056 <u>F.</u> 00_	.0.0000	30303E-01	ັ 0 • 0000 ເນຼື	- 29216E-13	^ @. 00000		0.00000_
75462E-13	0.00000	77023E-01	0.00000	93062Ē-0Ī	_0.00000	32350E-01	0.00000	64250F-13	0.00000	~48469E-13	_0.00000
97503E-13	0.00000	.77023t-01	0.00000	93062E-01	0.00000	32350L-01	0.00000	51687E-13	ó• aoooío	.974096-14	<u>0</u> .000 <u>0</u> 0
29726E-13	0.00000	201164+00	_0.00000]	-43425E-01	_0.00000	.17456E+00	0.00000	95853E-1.5		"62236t- <u>1</u> 3	0.00000
40148E-13	0.00000	.20116E+00	0.00000	43425E-01	~.ōōōōo~	.17456E+00	0,00000	.15212E-13	~ ó.öööőo	-52667 <u>E-13</u>	0.00000

THE TOTAL I REDUCTION - 17274226-03	NAT	URAL	FREQUENCY=	.4174i1E+03	
-------------------------------------	-----	------	------------	-------------	--

TX TX TY TY REAL HAG KEAL	TY TZ	TZ RX IMAG REAL	RX Z RY Z KY	RZ RZ G RÉAL IMAG
REAL IMAG _ KEAL	I MAG REAL			
-64013E-01 0.00000 -52910t-13	0.00000639148-13	0.00000 .63021E-13	0.00000 32672E-01 0.0	0000 -181526+00 0.00000
64013E-01 0.0000054168E-13	0.00000,64139E-13	0.0000043817E-13	0.00000 [.326728-01] 0.0	0000 +.13152E+00 0.00000
19244E+00 0.00000 167584E-13	0.00000 130998-12	0.0000011365E-13	0.00000154316+00 0.0	000049635E-01 0.00000
.19244E+00 0.0000053661E-13	.59608E-13	0.0000053777E-13	0.000001543LE+00 0.00	0000 .49635E-01 0.00000
-23516E+00 0.00000 .26722E-13	0.0000099880E-13	0.00000300476-13	0.00000 - 2167 E+00 0.0	000015861E-01 0.00000
23516E+00 0.0000058134E-13	0.0000067232E-13	0.00000327956-13	0.00000 .21671E+00 .0.00	000015861E-01 0.0000J
13774E+00 0.0000026199E-13	.0.0000064851E,-14	0.00000 .4u561E-13	_0.00000920b7E-01 \0.00	00000.010.058686.00.0000
	0.00000	0.00000 "34806E-13	0.00000 ~92067E-Q1 0.00	0000 99498E-01 0.00000
10743E +00 0.0000018432E-13	. 0:00000 . :20e17E-17	0.00000 `20899E-13	0.00000500645-13	0000 10748E+00 0.0000
.10748E+00 0.00000 .27049E-13	0.0300048549E-13	0.00000		
-10748E+00 0.0000025696E-13	[0.00000][10137E-13	0.00000		
			_0.0000010726E-12_0.0	0000 .10748E+00 0.00000
-13773E+00 0.0000022444E-13		_ 0.0000028870L-13	0.00000 -92067E-01 0.00	0000 " .99898E-01 0.00000
13778E+00 0.00000 .48449E-13	0.0000041048E-13	0.00000 .37135E-13	0.00000 .92067E-01 0.0	000099698E-01 0.00000
23516E+00 0.0000016965E-14	0.00000 -40910E-13	0.00000 .11134E-13	0.00000 21671E+00 0.0	0000 1586 E-01 0.0000
-23516E+00 0.00000 -33215E-13	. 0.00000 .40696E-13	0.00000 .15375E-13	0.0000021671E+00 0.0	9300 <u>.</u> •12461 <u>E</u> -01 0.00000
-19244E+00 0.00000		0.0000020011E-13	0.00000 -15431E-00 0.00	000049635E-0[0.00000
-,19244E+00 0.0000011122E-13	0.0000031241E-13	0.0000090338E-14	0.00000 1.15431E+00 0.0	0.00 .49635E-01 0.00000
64013E-01 0.0000021933L-14	0.00000 .155246-14	0.00000 -24804E-14	0.00000326728-01 0.00	0000
.64013E-01 0.0000020656E-13	0.0000045732E-14	0.00000256326-14	0.00000326728-01 0.00	00 <u>00 18125 - 00 0.000</u> 00

TX REAL	XT Dari	TY KEAL	TY IMAG	TZ Real	TZ I MAG	RX REAL	RK IHAG	RY REAL	RY IHAG	REAL YMAG
-36878E-01	0.00000	.135941-12	0.00000	14130f-13	0.00000	31553[-13	0.00000		•	24507E+00 0.00000
-36878E-01	0.00000	45652E-13	0.00000	31286E-13	0.00000	.14528E-13	0.00000			24507E+00 0-00000
•53519E-01		.24100F+13	0.00000	.255686~13	0.00000	97411E-14	0.00000			_12083E+00_ 0.00000
•53519E-01		822546-13		•99554E-13	0.00000	296801-13	0.00000			12083 <u>+00</u> 0.00000
		80229E-13		25457E-13]		112556-13	0.00000	26056E-10]	0.00000	11441E+00 0.00000
				88410E-13		.15476E-13	0.00000	. +26406E-10	0.00000	11441E+00 0.00003
				.63461E-13.		•28229F-13	_0.00000_	11289E-10	0.000,00	25J18E-010.00000
_ •29143E+0)	0.00000	29064E-14	_0*000ûg _	45571E-13		•32188E-13	0.00000	11061E-10	_ 0 • 0 0 0 0 0 0	25318E-01 0.00000
14518E+00	0.00000	43 <u>208</u> E-1 <u>j</u>	_0•0000 7	<u>{</u> 1087E-14_		59169E-14]	0.00000	187846-13	_0.000 <u>00</u>	13025E-10 0.00000
				50784C-14						
				80237E-14						
	0.00000	53184E-13	0.00000	62926C=14	_0,00000_	203i7 <u>E_1</u> 4	0.00000	-12487E-12	0.000.00	.12977E-10 0.00000
-271436+00 -271436+00	_0*00000	24312E-14	0.00000	40161E-14	<u></u>	3 ₂ 762 <u>6</u> -13_	0.00000	-11008E-10	0.00000	.25318E-01 0.00000
	0.00000	*12060t -12	0.00000	16585E-13	0.00000	28098E-13	0.00000	11115E10]	_0.00000_	.253186-01 0.00000
==21665E+00	0 000 00_		. 0.00000 i	-406696-13	0.00000	11705£		262246-10	_0.00000_	-11441E+00 0.00000"
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	A 00000	_ *01/375=13 `= '0/3/44	0,00000			12644E-13	0.60000	26146E-10	_0 • 005 00 <u>_</u>	-114416+00 0.00000
53519E-01	0.00000	147461 13	0.00000	47854E-13_	ó*auôãa_	-14538E-13	0.00000	.18620E-10	ò∙ oō cío cí	- <u>12083</u> +00 0.00000
		<u>.</u>	0.00005	, =+51742L=13	0.00000	40007L-14	0.00000	-18703E-10_	0.00000	12083=+00 0.00000
•36878E-01	.ย. ออกกกา โย. ออกกกกา		0.00000	<u>+03</u> 753E- <u>14</u>	0.00000	338826-13	_0.00000 <u>`</u> _	39824E-11	[0.000 <u>0</u> 0]	-24507E-00 0.00000
<b></b>	-200000	-4300715-13	0.100000	*22056E-13	0,00000	.21267E-13	0.00000	39118E-11	0.00000	.24507E+00 0.00000

NATURAL FREGUENCY=

-916203E+03

## NATURAL FREQUENCY= _.929122E+03

TX REAL	TX IMAG	- TY REAL	TY Imag	TZ RLAL	TZ IHAG	R X RE AL	RX IMAG	REAL T	THAG .	RZ REAL	RZ 1 MAG
255378-13	0.00000	*15613E+00'	0.00060	14467E+00	0.00000	•4J207t-01	0.00000		ີ່ ບ <b>ຸ</b> ດດວ້ວວີ	-10965E-1	3 0.03003
+19993E-13	0.00000	15613E+00	0.01000	14467E+00	0.00000	. 432074-01	0.00005	24714E-11	0.000000		3 0.00000
-4853bE-13	ั้ง . ข้ออออ	.13307c+00	0.00000	.25504E+00	0.00000	//583E-01_	0.00000	25407E-Li	_ ი•ეთენი_		3 0.00000
228G8E-13	0.00000	13307E+00	0.00000	.25504E+00	0.00000	7/5d3E-01	0.00000	24421L-11	0.0000 <u>0</u>	-14765E-1	3 0.0000
6B464E-13						36558E-01					
3459dE-13											
-39059E-13											
22414E-13							_0.000 <u>0</u> 0	•22319E-11	0.00000	.25230E-1	0.00000
18798E-13						-					
31239E-13					•						
29851E-13											
15246E-13						•					
69185E-14											
-44014E-13				,							
16429E-13											
36408E-13											
2359eE-13											
26410E~13						-43207E-01					
17920E-13	0.00000	15613E+00	0.00000	.14467E+00	0.00000	.43207E-01	0.00000	20513E-11	0.00000	·22694E-13	0.00000

NATURAL FREQUENCY= .933079E+03

TX REAL	TX Imag	REAL .	TY IHAG	T.Z Real	T Z I HAG	KEAL Keal	RX I HAG	RY REAL	SA ZA	RZ RZ
180316-14	0.00000	.11655£+00	0.00000	.14660E-11	0.00000	4d202E-12	0.00000	.224101+00	0.00000	le041É-12 0.u0000
.+207636-13	0.00000	.116555+00	0.00600	•147d2E-11	0.00000	47013E-12	0.00000	22410E+00	0.0000	84574E-13 0.60600
.70526E-13	0.00000	13543E-11	0.00000	26240E-11	0.00000	.81035E-12	0.00000	.22410£+00	0.00000	-51997E-13 0.00000
F•23068E-13	0.00000	.13840E~11	0.00000	264556-11	0.00000	.80127E-12	0.00000	22410E+00	0.00000	-69835E-13 0.00000
154868-12	0.00000	116556+00	0.00000	*50503F-11	0.00000	.36692t-12	0.00000	.2241UE+UO	0.00000	5973213 _0_000000_
682436-13	0.00000	11655E+00	0.00000	20018E-11	.00000	.37558t-12	0.00000	22410E+00	0.00000	55083E-13_0.00000
17151E-12	_ 6 <u>*</u> 00000	- <u>.</u> 11635 <u>E</u> +0 <u>0</u>	_o <u>•</u> oo o ŏ o	15261F-11	_ Ö•00ó00	12412b-11	0.00000	.22410E+00	0.00000	27685E-13 0.00000
•1427dE-12	0.00000	11655E+00	0.60000	15046E-11	0.00000	125506-11	0.00000	22410E+00	. 0.00000	-32127E-14 0.00000
-61144E-13	0.00000	15617E-11	0.00000	34839E-12	0.00000	-43232E-12	0.00000	.22410[+00	0.00000	-20165E-13 0.00000
7-14537E-12	0.00000	160241-11	0.00000	37052E+12	0.00000	<del>-</del>				
11871E-12	0.00000	153835-11	0.00000		0.09000	•				
72953E-L3_	_0.00000_	15990L-11	0.00000	.500∠7Ě-12	0.000[0	43216E-12		22410E+00	0.00000	53874E-14 0.00000
	0.00000	•11055E+00	6.00000	12470E-11	0.00000	12732E_11	0.00000	.22410E+00	ñ• òonoo	29335E-13 0.00000
17733E-12	0.00000	``.11655E+00	0.0000	-12189E-11		125198-11	0.00000	22410E+00	0.00000 <u></u> 0	.40237E-13_0.00000
32525E-13	0.00000	.11655E+00	0.00000	17810E-11	0.00000	. 440054E-12		.22410E+00		.65477E-13 0.00000
-20021E-12	_o•oóooo_	11655E+00_	020000	1788dE-11	0.00000	40035E-12	0,00000	22410E+00	0.00000	.67635E-13 0.00000
28044E-13	0.00000	13132E-11	0.00000	¿5210E-11		.74281E-12	_0.00000	22410E+00	្ត្រស់លំពេលប្	
781358E-13	0.00000	.131742-11	0.00000	.248548-11	~0.00000	~~.75208E-12	0.00000	224106+00	0.00000	89743E-13 0.00000
347685-13	0.00000	11655E+00_	~o•oooo	14659E-11	_ 0.00000	390276-12	. 0.00000	~~.Ž2410E+00	~å.00000	
123528-14	0.00000	110556+00	0.00000	144145-11	0.00000	3J71dE-12	0.00000	2241GE+00	0.00000	- *51539E-15 _0*00000_

ş	
š	
10.10	
÷	
24.44	
ž	

TX	NATURAL FREQUENCY - 47749146+03												
-33464E-14 0.0000	TXREAL	TX,	TY	TY	TZ REAL	TZ I HAG	RX	RX [HAG]	RY	THYR	RZ ŘEÁL	HZ 1HAG	
-20393E-13 0.00000	32308E-13	0.00000	17756E-01	0.00000	50200E-01	0.00000	.12920E+00	0.00000	14072E-11	ó <u>• 000 00</u>	35455E14_	0.00000	
-32785E-13 0.0000075281E-01 0.0000014850E+00 0.0000096335E-01 0.0000010937E-11 0.0000030581E-15 0.0000030580E-15 0.0000030580E-15 0.0000042460E-02 0.000005028E-12 0.0000040195E-14 0.0000027930E-14 0.0000042460E-02 0.0000042460E-02 0.0000043033E-12 0.0000030580E-14 0.0000042460E-02 0.0000042460E-02 0.0000043033E-12 0.0000043033E-13 0.000004085E-01 0.0000030447E,00 0.0000012268E-01 0.0000027982E-12 0.0000015488E-13 0.000004085E-01 0.000001394E-00 0.0000012268E-01 0.000007555E-13 0.0000012268E-13 0.000001394E-00 0.0000000000000007555E-13 0.000007555E-13 0.000001398E-01 0.000001398E-01 0.00000000001398E-01 0.000001398E-01 0.000001398E-13 0.000001398E-13 0.000001398E-13 0.000001398E-13 0.000001398E-13 0.000001398E-13 0.000001398E-13 0.000001398E-13 0.000001398E-13 0.000003298E-13 0.000003	334648-14	0.00000	.177566-01	0.00000	50200E-01,	0.00000							
-61563E-13 0.00000 .72219E-01 0.0000026832E+00 0.00000 .42460E-02 0.0000050028E-12 0.00000 .40195E-14 0.00000 .279300E-14 0.00000 .4260E-01 0.00000 .4260E-01 0.00000 .2793E-12 0.00000 .1268E-13 0.00000 .1268E-13 0.00000 .1268E-14 0.00000 .7793E-13 0.00000 .1268E-14 0.00000 .7793E-13 0.00000 .1268E-14 0.00000 .7793E-13 0.00000 .7793E-13 0.00000 .7793E-13 0.00000 .7793E-13 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7793E-14 0.00000 .7	+20395E~13	0.00000	.752818-01	0.00000	-14850E+00	0.00000							
.62975E-13 0.0000072219E-01 0.000002683ZE+00 0.00000 .42460L-02 0.00000 .43033E-12 0.00000 .2798ZE-12 0.00000 .2798ZE-12 0.00000 .2798ZE-12 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-13 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14 0.00000 .2798ZE-14	32785E-13	0.00000	75281E-01	0.00000	14850E+00	0.00000							
-21388E-13 0.00000 .40855E-01 0.00000 .30987E+00 0.00000 .12268E-01 0.00000 .75595E-12 0.00000 .12488E-13 0.00000 .30987E+00 0.00000 .12268E-01 0.00000 .75595E-12 0.00000 .21765E-14 0.00000 .21765E-14 0.00000 .30987E+00 0.00000 .00000 .75595E-12 0.000000 .21765E-14 0.00000 .22765E-14 0.000000 .22765E-14 0.00000 .22765E-14 0.00000 .22765E-14 0.00000 .227	61563E-13	0.00000	.72219t-01	0.00000	-+26832E+00	0.00000	.42460E-02	0.00000					
-55871E-13 0.0000040355E-01 0.0000013984E+00 0.0000060918E-13 0.0000014816E-12 0.000001195E-14 0.0000010203E-12 0.0000013984E+00 0.0000060918E-13 0.0000075595E-12 0.0000021755E-14 0.0000042204E-13 0.0000071252E-13 0.0000013984E+00 0.0000042204E-13 0.0000071252E-13 0.0000013984E+00 0.0000034422E-13 0.000001132E-12 0.0000013984E+00 0.0000027929E-13 0.0000040855E-01 0.0000013984E+00 0.0000059499E-13 0.0000081721E-12 0.0000042997E-14 0.0000027391E-13 0.0000040855E-01 0.00000 .30947E+00 0.0000012268E-01 0.00000 .30395E-12 0.0000093193E-14 0.0000027391E-13 0.00000 .40855E-01 0.00000 .30947E+00 0.0000012268E-01 0.0000085154E-12 0.0000013436E-13 0.0000095509E-14 0.00000 .72219E-01 0.00000 .30947E+00 0.0000042460E-02 0.00000 .6664E-12 0.0000011989E-13 0.0000082660E-14 0.00000 .72219E-01 0.00000 .14850E+00 0.0000042460E-02 0.0000069337E-12 0.0000019999E-14 0.0000081757E-14 0.00000 .75281E-01 0.00000 .14850E+00 0.00000 .90335E-01 0.0000032721E-12 0.0000042301E-13 0.0000060337E-12 0.00000 .75281E-01 0.00000 .14850E+00 0.00000 .90335E-01 0.0000032721E-12 0.00000 .21593E-13 0.00000	.62975E-13	0.00000	722196-01	0.00000	26832E+00	0.00000	.42460L-02	0.00000	.43033E-12	_ú.000000_	993006-14	0.62000	
-88182E-14 0.0000010203E-12 0.0000013984E+00 0.0000060918E-13 0.0000075595E-12 0.0000021755E-14 0.0000013984E+00 0.0000059204E-13 0.0000071252E-13 0.0000013984E+00 0.0000059204E-13 0.0000001721E-12 0.0000042997E-14 0.00000059209E-13 0.0000001721E-12 0.0000042997E-14 0.00000059209E-13 0.0000001721E-12 0.0000042997E-14 0.0000012268E-01 0.0000001721E-12 0.0000040855E-01 0.000001268E-01 0.0000012268E-01 0.0000085154E-12 0.0000093193E-14 0.0000029395E-12 0.0000012268E-01 0.0000085154E-12 0.0000013436E-13 0.000004266E-13 0.0000004266E-13 0.000000													
-15105L-14 0.00000 -1006E-12 0.00000 -13984E+00 0.00000 -13984E+00 0.00000 -342204E-13 0.00000 -71252E-13 0.00000 -13984E+00 0.00000 -59199E-13 0.00000 -81721E-12 0.00000 -42997E-14 0.00000 -27929E-13 0.00000 -11192E-12 0.00000 -13984E+00 0.00000 -59199E-13 0.00000 -81721E-12 0.00000 -93193E-14 0.00000 -27929E-13 0.00000 -12268E-01 0.00000 -12268E-01 0.00000 -85154E-12 0.00000 -93193E-14 0.00000 -27391E-13 0.00000 -12268E-01 0.00000 -12268E-01 0.00000 -85154E-12 0.00000 -13436E-13 0.00000 -12268E-01 0.00000 -85154E-12 0.00000 -111928E-13 0.00000 -12268E-01 0.00000 -12268E-01 0.00000 -12268E-01 0.00000 -12268E-12 0.00000 -111928E-13 0.00000 -12268E-01 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12 0.00000 -12268E-12													
-42204E-13 0.0000071252E-13 0.00000[3984E+00] 0.0000059199E-13 0.0000081721E-12 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.0000042997E-14 0.000004299	*88182E-14	_0.00000	102038-12_	0.00000	, 13984E+00_	0.00000	60918E-13	0.00000	7559 <u>5</u> E_ <u>_</u> 12	0.00000	.21765E-14	0.00000	
-34422E-13 0.00000 .11132E-12 0.0000013904E-00 0.0000059199E-13 0.0000081721E-12 0.0000042997E-14 0.00000 -27929E-13 0.0000040855E-01 0.00000 .30987E+00 0.0000012268E-01 0.0000085154E-12 0.0000093193E-14 0.00000 -27391E-13 0.00000 .40855E-01 0.00000 .30987E+00 0.0000012268E-01 0.0000085154E-12 0.00000 .13436E-13 0.00000 -39509E-14 0.00000 .72219E-01 0.0000026832E+00 0.0000042460E-02 0.00000 .67664E-12 0.000001928E-13 0.00000 -82660E-14 0.00000 .72219E-01 0.0000026832E+00 0.0000042460E-02 0.0000069337E-12 0.0000019069E-14 0.00000 -81757E-14 0.0000075281E-01 0.00000 .14850E+00 0.00000 .90335E-01 0.00000 .31307E-12 0.0000042301E-13 0.00000 -86750E-14 0.00000 .75291E-01 0.00000 .14850E+00 0.00000 .90335E-01 0.0000032721E-12 0.00000 .21593E-13 0.00000	151056-14	0.00000	1107046-12	0.00000	13984E+00	0.00000							
.27929E-13 0.0000040855E-01 0.00000 .10947E+00 0.0000012268E-01 0.00000 .90395E-12 0.0000093193E-14. 0.0000027391E-13 0.0000093193E-14. 0.0000012268E-01 0.0000085154E-12 0.00000 .13436E-13 0.0000026832E+00 0.0000042460E-02 0.0000067664E-12 0.0000011928E-13 0.0000012268E-14 0.0000012268E-14 0.0000026832E+00 0.0000042460E-02 0.0000067664E-12 0.0000011928E-13 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E-14 0.0000019069E													
27391E-13 0.00000 .40855E-01 0.00000 .30987E+00 0.0000012268E-01 0.0000085154E-12 0.0000013436E-13 0.0000013436E-13 0.0000013436E-13 0.0000013436E-13 0.0000013436E-13 0.0000013436E-13 0.0000013436E-13 0.0000013436E-13 0.00000013436E-13 0.0000013436E-13 0.00000013436E-13 0.0000013436E-13 0.0000013436E-13 0.00000013436E-13 0.0000013436E-13 0.00000013436E-13 0.0000013436E-13 0.0000013	_34422E-13	~	.11132E-12	0.00000	13984E+00	`ō.60000	59199E-13	0.00 <u>0</u> 00	-,81721E-12	0.00000	42997E-14	0.00000	
-95509E-14 0.0000072219E-01 0.0000026832E+00 0.0000042460E-02 0.00000 .67664E-12 0.0000011928E-13 0.00000 .82660E-14 0.00000 .72219E-01 0.0000026832E+00 0.0000042460E-02 0.0000069337E-12 0.0000019069E-14 0.00000 .81757E-14 0.0000075281E-01 0.00000 .14850E+00 0.00000 .96335E-01 0.00000 .31367E-12 0.0000042301E-13 0.00000 .66750E-14 0.00000 .75281E-01 0.00000 .14850E+00 0.00000 .96335E-01 0.0000032721E-12 0.00000 .21593E-13 0.00000 .21593E-13 0.00000 .21593E-13 0.00000 .21593E-13 0.00000 .32875E-13 0.00000 .32875E-13 0.00000	27929E-13	~ <b>5.</b> 00000°											
-82660E-1+ 0.00000	27391E-13	0.00000	.40855E-01	0.00000	.30987E+00	0.00000	12268E-01	6.00000	85154E-12	0.00000			
-81757E-14 0.0000075281E-01 0.00000 .14850E+00 0.00000 .90335E-01 0.00000 .31307E-12 0.0000042301£-13 0.00000 .6675aE-14 0.00000 .75281E-01 0.00000 .14850E+00 0.00000 .90335E-01 0.0000032721E-12 0.00000 .21593E-13 0.00000 .21593E-13 0.00000 .22546E-14 0.00000 .17755E-01 0.00000 .50200E-01 0.0000012420E+00 0.00000 .24513E-13 0.00000 .32875E-13 0.00000	<u>-</u> -95509E−14	0.00000	~.72219E-01	0.00000	26832E+00	0.00000	42460E,-02	0.00000	67664E-12	0000000_	11928E-13	0.00000	
.6675aE-14 0.00000 .75291E-01 0.00000 .14850E+00 0.00000 .45335E-01 0.0000032721E-12 0.00000 .21593E-13 0.00000	-82660E-14	0.00000	.72219E-01	,0.00000	-+2683ZE+00	0.00000	424502-02	0.00000	69337L-12	[0.00000]	- <u>-</u> 19069 <b>£-14</b>	0.00000	
-12546E-14 0.00000 -17755E-01 0.0000050200E-01 0.0000012420E+00 0.00000 -24513E-13 0.00000 -32875E-13 0.00000	-81757E-14	0.00000	752818-01	0.00000	14850E+00	0.00000	.90335E-01	0.00000	-31369E-12	0.00000	42301£-13	0.00000	
· ·	.66750E-14	J.00000	.75281E-01	0.00000	.14850E+00	0.00000	.40335E-01	0.00000	327216-12	6.00000	•21593 <u>€</u> -13	0.00000	
.36711E-14 0.0000017756E-01 0.0000050200E-01 0.0000012920E+00 0.0000060261E-14 0.0000056336E-13 0.00000	-12546E-14	0.00000	.17755E-01	0.00000	50200E-01	0.00000	129205+00	0.00000	.245138-13	_ 0.000000	.32875E-13	0.0000	
	.36711E-14	0.00000	17756E-01	0.00000	50200E-01	0.00000	129202+00	0.00000	60261E-14	0.00000	56336E-13	0.00000	

NATURAL FREQUENCY= .951748E+03												
TX	TX Inag	. TY REAL	TY Imag	TZ REÁL	TZ I MAG .	RX RLAL	RX I MAG	RY RY RZ RZ RZ RZ REAL THAG				
337678-14	0.00000	-387458-12	0:00000	147GdE-12	0.00000	1J414E-12	0.00000	32827E+00 0.00000 .49106E-13 0.00000				
201846-13	0.00000	17469E-12	0.00000	18040E-12	0.00000	113186-12	, 0*00000	.32827E+00 0.0000042276E-13 0.00000				
46318E-13	0.00000	-10657£-12	0.00000	.17541E-12	0.00000	•32428E-13	0.00000	2886E+00 0.00000 -17621E-13 0.00000				
+45363E-15	0.00050	91839E_13	0.00000	-20533E-12	0.00000	.41153E-13	0.00000	.28868E+00 0.0000030043E-13 0.00003				
76042E-14		171486-12	_ a•ŏnoōo <u>, </u>	.12697t-12		62074E-13	0.00000	21426E+00 0.00000 .10780E-13 0.00000				
-1265 sE-13	*0.00000	46559L-13	0.00000	15036E-12	0.00000	830318-13	o•óaaaộ	.21426E+00 0.0000012958E-13 0.00000				
41488E-13	0.00000	320776-12	. 0,00000	10979E-12		.12088E-12	0.00000	114016+00 0.00000 .38081E-14 0.00003				
65023E-13	0.00000	.11834E-12	0.00000	32152 <u>E</u> -12	0.00000	12376E-1 <u>2</u>	0.00000	.11401E+00 0.00000 .15896E-13 0.00030				
,17561E-13	0.00000	276276-12		Ž69.j0E-12	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	64650E-13	0.000000	47824E-12 0.0000022492E-13 0.00000				
48473E-13	<u>_0</u> -00000			-28276E-12								
-94414E-14	0.00000	260326-12	_0.00000	15665 <u>E-1</u> 2								
28840E-13	g*.qóo.oo]	.207016-12	0.00000	•16,147E-12	0.00000	52723E- <u>13</u>	0.00000	.49380E-12 0.0000013360E-13 0.00009				
35076E-13	์ ดั•ูขอดัอง	36150E- <u>_13</u>	_0,00000°	68740E-12	0.000000		_0.000000	.11401E+00 0.0000045458E-14 0.00000				
3109iE-13	0.00000	.31008t-12	0.00000	72934E-12		24010E-12	0.00000	11401E+00 0.0000013109E-13 0.00000				
13441E-13	0.00000	.28679L-12	0.00000	.707061-12	0.00000	74463E-13	0.00000	.21426E+00 0.00000 .18155E-14 0.00000				
59411E-13	0.00000	34876L-13	0.00000		``o•`oooōo	47518E-13	0,60000	21426E+00 0.0000019740E-14 0.00000				
	<u></u>	.32947E-12		62860E-12	<u>_0</u> • <u>0</u> 00000	256-13E-12	0.00000	.28868E+00 0.00000 .46572E-14 0.00000				
596728-11	0.09000	31440E-ÎZ	`0.00000	607o5E-12	0.00000	2d194E-12	0.00000	28868L+00 0.00000 .13706E-13 0.09000				
109516-13	u.00000	.647205-13	0.00000	.322998-12	0.0,0000	-22906E-12	0.00,000	.328278+00 · 0.00000 .117906-13 0.00000				
_+.12213E-13	0.00000	352958-12	0.000000	30117E-12	0.00000	-27683L-12	o•00 <u>0</u> 00	,32827E+00 U.00000,51965E-13 0.0000				

				=	• •						
TX	TA	TY REAL	TY . Imag .	T Z R E A L	TZ IHAG	RX KEAL	RK THAG	RY Real	RY THAG	RZ	THAG
39211E-01	0.00000	.314121-13	0.00000	198916-13	0.00000	113466-12	0.00000	10720Ê-0	` "0.000b0" <u>"</u>	15229 <u>E</u> +	00 0.00000
39211E-01	0.00000	25223E-13	0.00000	44596E-13	0.00000	505446-13		-			<u>໐ບ</u> ຼຸດ້ວດວັດ <u>ວ</u> ້
				38010E-13		.419516-13					oro•_oʻ2003_
13113E+00				29910E-13		.23436E-13	0.00000	10918E+0	ີ້ 6.00000	57038E-	01000000
<u>-</u> -21678E+UJ	0.00000	173115-13	.0.00000	58173EL3_	0.00000	.44447E-13	0.00000	19851E+0	0.000,00	2961 <u>LE</u> -	01 0,00000
_21898E+00	5.00600	.224591-13	0.00000	. 39213Č-13	0.00000	.42574E-13	0.00000	19851E+0	ຼຸດ. ດວບເຫຼົ	. 29611E-	01 0.30000
.22378E+03	0.00000			52075E-13		851296-15	0.00000	.21374E+0	oʻ_0•'00°'0 <u>o</u>	39217E-	oio.o.o.o.o
						23216 <u></u> =14	0.00000	21374E+0	0.00000	3 92 I ŽĘ-	01 0.00000
				188956-13		82587±-14	0.00000	11370L+0	00.00000	.45981 <u>E</u> -	13 0.00000
				32928E-14		•					
				.785148-15							
96721E-01	_0.00000_	.62946 <u>L-14</u>	0.00000	18599E-13	0.00000	5al00 <u></u> -14_	∵o•ãoóão	11370E+0	0_00000	.59141Ē~	13 0.00000
2237dE+00	<b>~0.00000</b>	.52071 <u>E</u> -13	0.00000	-279288-14	0,00000	40377E-13	0.00000	.21374É+0	0 0.00000	.39217E-	01 0.00003
22378E+00	`0.00000	11610E-13	0.00000	-,97341E-14	0.00000	94659E-15	0.00000	,21374E+Ò	0_00000	39217E	<u>01_0</u> 00000
Z1898E+00	0.00000	.499931-13	0.00000	.25264E-13	0.00000	816454-14	0.00000	198518+0	0 0.00000	-29011E-	-01 , 0 • 0 • 30 0
.21895E+00		,462326-14	0.00000	21651E-13	_0.00000	65678L-15	0.00000	,1985iE+0	0000000_	29611E-	01 0.00000
	0.00000		-0.000000	-+10324E-13	0.00000	-32771E-14		. 10918E+U	ó 0.0000 <u>0</u>	57038E-	01 0.00000
						803776-14			0.00000	.57033E-	-010.00000
				115196-13					1 0.00000	.15229E+	00_0*09300
•											000 (0000

39211E-01 0.00000 -.80061E-14 0.00000 .64394E-14 0.00000 .8d674E-14 0.00000 -.10720E-01 0.00000 -.15229E+00 0.00000

NATURAL FREQUENCY= .984405E+03

NATURAL FREQUENCY= .1044796+04												
TX REAL	TX EMAG .	TY REAL	YT Dami	TZ REAL	T Z I mag	. KK	RK IHAG .	RY	THAG	REAL	RZ IMAĢ	
81345E-01	0.00000	.581018-13	0.00000	30729E-13	0.00000	23973E-13	0.00000	35101E-13	0.00000	.27086E.00	<u>_0.0000</u>	
81345E-01	0.00000	759051-13	0.00003	2044.7E-14	9.00000	856231-13	0.00000	•27719E-13	0.00000	_+2708ab+00	0.00000	
59051E-01	0.00000	905108-14	0.00000	.52400E-13	0.00000	.53475E-13	0.00000	85180E-13	0.00000	i0252E+00	. 9 • 600 6 6	
_+59051E-01	0.00000	.60655E-13	0.00000	24874E-13	0.00060	.24960E-13	0.00000	97394E-13	0.00000	10252E+00	0.00000	
74947E-01	0.00000	809516-13	0.00000	26744E-13	0.00000	, .49821E-13	0.00000	.422243E-12	n. 000000 <u>.</u> .	17124E+00	0.00000	
74947E-01	0.00000	.973796-13	0.00000		0.00000	.52680E-13	(0.0000)	23111Ei2	_0.00000	.171244 00	0.00005	
19734E+00	0.00000	923041-13	_0.00000_	52385E-14	0.00000	.277236-13	0.00000	21546E-12	0.00000	9d791c-01	0.03000	
7.19734E+00	( <u>_0.0</u> 00000	.3739,16-113				43696E-i3	'ŏ•ō∪ooö	21683 <u>E</u> _1,2		98/91E-01	0.00000	
Z2530E+00	_ n* 0,0g00 []	24784 <u>L</u> -13	<u>_0.0</u> 0005_			. 12730L-14	0.00000	.12191E-12	0.00000	.22530c+00	0.0000	
	0.00000	160946-13	0.00000	288938-13	0.00000	-						
22530E+00	0.00000	24199E-13	_0.0000	18866E-13	_0.00000	• ••						
22530E+00	0.000000	ia7036-13	_ัง •ัด <u>์ ช</u> ี ย, จัด ั	27505E-13		89510L-15			0.00000	.22530E+00	0.00000	
19734E+00	0.00000_	54086E-13	0*0000	35425E+13		1930SE-13	j. 00000	21993E-12	0.00000	98791c-01	0.0000	
19734E+00	000000 <u></u>	48618E-13	0.00000	-23874E-13			_0,000000_		0.00000	98791E-01	0.00000	
74947E-01	0.00000	. <u>8</u> 7243E-13	0.00000	27022E-13	p.00u00	216156-13	0.00000	.18834E-12	ŭ• ġosoo ]	- <u>i</u> 71246•00	0.00000	
74947E-01	0,000,00	-:101466-13	0.00000	-55665E-16		169586-13	_0.00000	.19159E-15	0.00000	.17124E +00	0.00000	
-159051E-01	0.00000	.125345-13	` o \$ou o no	31-937E-13	0.00000	.30923L-14	0.00000	956,97E-13		-10252L+00°	_0.00000_	
59051E-01	2.00000	.470911-13	~00°00°	. 23341E-13	_0.00000	-83404E-14	.0.00000	98119E-13	0.00000	102526+00	0.00000	
	0.00000	109858-12	0.00000	33773E-13	0.00000	.54901E-13	0.00000	.16801E-13	0+00000	.27086E+00	0.00000	
81345E-01	0 • 0 0 0 0 0 0	-43982E-13	0.00000	[-7,23694E-13	0.00000	.54874E-13	_0.00000	16042E-14	_0.000000	.27086E.+00		

#### NATURAL FREQUENCY= .990994E+03.

_ TX _ REAL	TX IMAG	. IY REAL	TY .	TZ REAL	TZ I HAG	kx Real	RX	REAL		TRÝ THAG	KEAL.	R Z I HAG
~15385E-13	0.00000	219281-13	0.00000	.21010E-12	0.00000	40993E-12	0.00000					
2627aE-14	0.00000	.97677E-14	0.00000	-16962E-12	0.00000	41041E-12	0.00000	.3323	É FÓ Q	0.00000	64944 <u>E</u> -	13 0.00000
69847E-13	0.00000	26234E-12	0.00000	61083E-12	0.00000	.36965E-12		2053	E + oo	0.00000	10610 <u>E</u> -	13 0.00000
-64807E-13	0.00000	31681E-12	0.00000	56428E-12	0.00000	.38726E-12	0.00000	2053	Ē+ĢŌ_	0.00000	759 39E-	14 0.00000
.78852E-13	0.00000	165758-12	0.00000	.10190E-11	0.00000	36469E-13	0.00000	2927	E-12	0.00000	.164846-	14_0.00000
88854E-13	~~o.oooo	16578E-12	0.00000	103476-11.	0.00000	[-:81169E-13	_ 0.00000	-40440	15_	_o • o o o o o o	57 <u>956</u> E-	13 0-00000
10909E-12	0.00000	24089E-13	0.00000	109676-11	ó•00000	11895E-12		20536	£.+00	0,000,00	2345 <u>TÉ</u> -	13 0.40000
-53311E-13	. 0 . 0 0 0 0 0	21705E-13	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	111016-11	0.00000	117076-12	0.00000	2053	BE + 00 _	_u_ŏou oo	14105E-	13 0.0000
-74275E-13	0.00000	41045E-13		-49430E-12	00000		0_00000	.3323	E • 00_	0.00000	• Z Z Z 46Ē-	13 0.0000
42135E-13	0.00000	61407£-13	`0*0000	.505468-12	0.00000	<b></b>						
-34726E-13	0.00,000	41856E-13	0.00,000	512556-12	ÿ•ŏoōoo							
265216-13	_0.00000	25614E-13	_0.00000	.52147Ê-12	0.00000	.83431E-14	_ ō•ōooóo	3323	E+00	0.00000	1d267E-	13 0.00000
91021E-13	_0.00000]	78620E-13	_ 0̂•00 <u>0</u> 00_		0.00000		0.00000	2053	E+VO	0 <u>•00000</u>	40369E-	13 0.00000
-10629E-12	0.00000	`84876E-13	0.00000	11012E-11	0.00000	-7413ZE-13	00000	-2053	E +00.	0 <u>.0</u> 00000	13441 <u>E</u> -	13 0.00000
_69570E-13	0.00000	-19366E-12	0.0000	.96412E-12	0.00000	.50007E-13	_ o • <u>0</u> 000 <u>0</u> 0	3794	E-12	00000	263506-	13 0.0000
56114E-13	0.00000	16906E-12	0.00000	.97012E-12	0.00000	.418710-13	0.00000	2402	E-12	0.00000	.271344-	14 0.00000
43810E-13	ý• 00000	.20411E-12	0.00000	585566-12	0.00000	327641-12	0.400000	2053	5E+60°	0500000	.210441-	13 0.00000
-3178aE-13	0.00000	265540-12	0.0000	58991E-12	0.00000	3401dE-12	0.00000	•2053	3E+00	0.00000	319326-	13 0.0000
-15610E-13	0.00000	15835E-13	0.00000	.21246E-12	0.00000	.41686E-12	0.00000	3323	LE + 00	~ <b>0</b> ~ 00000	98215E-	13 0.00000
·•11775E-13	0.00000	483986-13	0.00000	22808E-12	0.00000	.404395-12	0,00000	.3323	E+00-	0.00000	.81971 <del>2</del> -	13 _0.00000

		112.01			T. 3						
TX	TX	TY	YY (	TZ REAL	TZ	RX REAL	RK IHAG	RÝ RÉAL	LHAG	RŽ RÉAL	I HAG
-56861E-14	0.00000	23074E+00	0.00000	•96435E-01	0.00000	*13996E+00	0.00000	246] 0E-1J	0.00000	299426-13	0.00003
		.23074E+00				.13996E+00	0.00000	24419E-11	0.00000	1126ZE-13	0.00000
						27662E-01	0.00000	-14095E-12	0.00000	4565ZE-13	0.00000
						2766ŽE-Ö1					
						84102E-01					
						84102L-01					
						13909E+00					
						13909E+00					
779998-13						6>937E-13					
621370-13	0.00000	.98129E-14									
		.992226-13									
						29826E-13	0.0000	18367E-12	0.00000	.642196-13	0.00000
						.13409E+00					
						84102E-01					
88570E-14				.30248E-01							
30740E-13	0.00000	13598E-01	0.00000	17617E+00		2/662E-01	_ 0.00000		_0.00000	22049E-13	0.0000
						.27662E-01					
•23348E-13					_	13996E+00					
	•	•									

.27776E-13 0.00000 -.23074E+00 0.00000 _.96435E-01 0.00000 -.13996E+00 0.00000 _.2036JE-11 0.00000 .92637E-13 0.00000

NATURAL FREQUENCY= 107160E+04

		`HĄTURA	L FKLQUEN	NCY=107813	3E+04 ]						
TX REAL	TX .	TY - REAL -	TY IMAG _	TZ REAL	TZ THAG	RX REAL	RX I MAG	RY REAL	RY	RZ	RZ IMAG
42223E-13	0.00000	.21564E-11	_0.00000	74956E-12	0.00000	116376-11	0.00000	•28868E+0Õ	0.00000	-48251E-13	0.00005
15830E-13	0.00000	151946-11	0.00000	74492E-12		120106-11	0.00000	28868£*00		-40522E-13	0.00000
-33831E-13	0.00000	265076-12	0.00000	134156-11	0.00000	.25976E-12	0.00000	34005E-13	0.00000	13504E-13	T0.00000
.42537E-13	0.00000	•46078E-14	0.00000	13098E-11	0.00000	.20613E=12	0.00000	~.33445E-13	0.00000		0.00000
6488)E-14	0.00000	22759£-11	6.00000	,117476-12	0.00000	.65320E-12	0.00000	28868E+00	. 0.000000	95322E-14	
	0.00000	.14716E-11	0.00000	13809E-12	0.00000	.64931E-12	0.00000	28866E+00	_0.00000	18489E-13	
49984E-14	0.00000	20656E-11	0.00000	18618E-12	_0.00000	,.10993E-11	0.00000	28868E+00	_ 0.00000_	75055E-13	0.00000
.47563E-13	0.00000	182516-11	0.00060	15667E-12	0.00000	-111386-11	0.00000	_ 288681+00		47822E-13	0.00000
35639E-13	0.00000	.33473E-12	-ò.0000ō	35741E-12	0.00000	.114848-13	0.00000	~~.14261E-12	_0:,000 <u>0</u> 0	-21890E-13	
43330E-13	0.00000	29554L-12	0.00000	305828-12	0.00000						
-12777E-13	0.00000	· .31628E-12	0.00000	3217dE-12	0.00000						
[24953E-14	0.00000	-243486-12	0.00000	27294E-12		.8.3546E-14	0.00000	10000e-12	0.00000	25778E-13	0.00000
•132962-13	0.00000	.18651E+11	0.00000	14071E-12	.0.0000	114931-11	0.00000	.28868E+00	0.00000	23352E-14	_0.00000
<u>=</u> 435394E−13	.0.00000	21153E-11	jo. joo o o o	16197e_12	_0.00000	117/21E_11 ,		28868£+00	<u></u>	15969E-13	0.00000
•17434E-13	0.00000	-14958E-11	0.00000	15693E-12		657918-12	00000.0	~ 28868E+00	0.00000	27607E-13	0.00000
.15655E-13	3.00000	225631-11	0.00000	17839E-12	0.00000	65916=-12	0.00000	28868E+00	0.00000	•12359 <u>E</u> -13	0.00000
<del>-</del> -26975E-13	0.00000	54856E-15	0.00000	-14022E-11	0.00000	26284E-12	0.00000	.67637E-13		12731E-13	0.00000
13956E-13	0.00000	21768E-12	0.00000	.13947E-11		24176E-12	0.00000	10350E-12	0.00000	.70751 <u>F</u> -14	0.00000
-26705E-13	0.03000	154698-11	0.00000	775316-12	0.00000	-116426-11	0.00000	28868E+00	0.0000	.1>480c-12	0.00000
.90%5E-14	0.00000	.22175E-11	0.00000	773716-12	.0.00000	.11350E-11	0.00000	-28868E+00	0.00000	411376-13	0.00000

		•		CY= 1096901							
TX PEAL	INAG	TY	TY ÎMAG [	TZ REAL	TZ	RX REAL	RX 1HAG	REAL	HAG T	REAL	RZ IHAG
.382226-13	0.00000 "-	25583E+00	0.00000	*•10322E-I2	0.00000	.67417E-13	0.00000	~~.44144E~12	0•,00000	.98734E-14	0.00005
	0.00000	25583E+00	0.00000	-31525E-13	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	72460E-13	0.00000	~.55430E-1Z		· I0299E-12	0.0000_
10525E-L3	ŭ.00000°	.97720E-01	0.00000	~.71625E-13	0.00000	333958-13	0.00000	-120248-12	0.00000	.48102E-13	0.00000
17322E-13	n• <u>0</u> 009000	.97720E-01	0.00000	13024E-12	00000.6	-24131E-14	0.00000	11273E-12	0.00100	247976-13	0.00000
24508E-13	0.00000	.31623E.00	0.00000	29320E-14		61891E-13	0.00000	296368-12	0.00000	72308E-14	0.00000
74115E-14	0.00000	.31623E+00	0.60000		0.00000	271306-13_	0.00000		_ ŏ. ŏocoo ¯ -	.27570t-13	0.00000
•17199E-13	0.00000	.97720E-01	0.00000	•33464E-14	0.00000	860821-13	0.00000	42696E-12	_0.00000	.45090E-13_	0.0000
58835E-13	0.00000	.97720E-01	0.00000	.j0949E-1 <u>j</u>	0.00000	72609E-13	0.00000	47128E-12		.64787E-13	o. <u>.</u> 00000
45928E-13	0.00000	25583E+00	0.00000	i21756-13]	0.00000		0.00000	11085E-I2	_0.000 <u>00</u> 0	.564436-13	0.00000
329808-13	0.00000	25583E+00	0.00005	.25793E-13	-0:00000	_					
-284u7t-13	6.00000	25583E+00	0.00000	191936-13	_0.00000	••					
-80953E-13	0.00000	25583E+Ó0	0.0000	.5 <u>348</u> Ĭ£- <u>I</u> )	0.00000	.23478E-13	0.00000		0.00000	34055E-13	0.0000
±•73242E-13	0.00000	.97720E-01	ិច ១០១០១ភ្ន	8540QC-13-	_0.00000	70659L-13	_0,000000	55980E-12	0.00000	.52619c-13	0.0000
-34350±-15	0.00000	.97720E-01	0.00000	.21542E-14	0.00000	.61083E-13	0.00000	45890E-12	0.00000	.23637E-14	0.00000
16350E-13	0.00000	.31623E+00,	0.00000	94499E-14	0.00000	.40668E-13	0.00000	70116E-12	0.00000	73826E-13_	0.00000
.54857E-13	0.00000	•31623E+00	0.00000	10845E-13	0.00000	.39042E-13	0.00000	51848E-12	0.00000	43388E-13	0.00000
60926E-13						22106E-14				.26366E-13	
35464E-15	0.00000	.97720E-01	0.00000	~_47199E-13	0.00000		0.00000	61104E-13	0.00000	.69663E-13_	0.00000

-12726E-13 0.00000 -.25583E+00 0.00000 -.19614E-13 0.00000 -.54751E-13 0.00000 -.59940E-12 0.00000 -.42266E-14 0.00000 -.32207E-13 0.00000 -.25583E+00 0.00000 -.33745E-13 0.00000 -.78366E-13 0.00000 -.61199E-12 0.00000 -.57627E-13 0.00000

		NATURA	L Fr£QUet	iCY=11286	3E+04 _						
TX .	- TX	TY .	TY IHAG	TZ REAL	. TZ .	⊀€∀7 ∀X	R4 Imag	RYREAL	' RÝ IHAG "	REAL	RZ IHAG
==20107E-13	0.00000	.241246-11	0.00000	78627E-LZ	0.00000	29558E-11	0.00000	+27911E+00	0.00000	-29537E-13	0.00005
92558E-13	0.00000 -	~27472L-11	0.00000	/3965E-12	_0.00000	297416-11	6.00000	~27911E+00°	0.00000		0.00000
-10897E-12		·. Y3782e - 11	00000.0		000000	-10305t-11	0.00000	10661E • 00	0.00000	15729E-13	0.0000
-47405Ê-1J	[0.00500]	.i5160E-11]	0.00000	12184E-11	00000.0	.16002t-11	0.00000	.10661E÷00	~ 0.0000°	248296-13	0.00000
408722-14	0.00000 -	30478E-11	0.00000	+13092L-L1	0.00000	.43J05E-12	0.00000	344998+00	0.00000.	30083E-13	0.62200 _
39416E-13	~~ooooo ~~	. <u>3</u> 43488-11	_0.00000_	12786E-11		45726E-12	`n.500ŏġ	.34499Ē + Ūტ	_0.0 <u>0</u> 0000_	78503 <u>e</u> -14	0.00000
•44943E-13	0.00000	21045£-11,	_ <b>ó.</b> 00000	392 <u>89</u> E-11	_0.00000	•22350E-11	0.00000	10661E+00	0.00000	.41407£-13	0.00000
.17233E-1	0.00000 [	-21881E-11	0.00000	~39361E-11	^ 0.00000	.222531-11	0.00000	*10e01£+00	0.00000	58525E-14]	<u>0.0000</u>
18362E-1	0.00000	_20230E-11	0.00000	390P9E-FF		39436E-11	0.00000	.27,9116+00	_ <b>n* 00 n 0</b> 0	334798E-13	0.0000
14785E-13	0.00000	22943E-11	0.00,000	39133E-11	o.ooooo	" * •••					· · · · · · · · · · · · · · · · · · ·
-,73766E-13	_o.ooodo [	`.20316É-11	~0.00000°	395d0E=L1	_ 0.00000						
						395636-11					
						.~.22531E-11					
-,10385E-1	. o. oo òo o	. 22764F-11	0.00000	.40422E-11	i.00000		0.00000	*j0691E+00	0.00000		0.00000
.".98914E-14	0.00000	319336~11	0.00000	141058-11	0.00000	46386E-12	0.00000	344996+00	0.00000	-,433336-13	0.0000
						.47446E-12					
79557E-1	3 _0.00000	14777E-11	0.00000	12308E-11	0.00000	17061E-11	0.00000	10661E+00	0.00000	44007E-13	0.00000
						.170506-11					
						31210c-11					
746428-1	3 0.00000	27366E-11	0.0000	.786376-12	0.00000	315846-11	0.00000	27911E+00	u.00000	1,0967e-12	0.00000

NATURAL FREQUENCY= .113954E+04

		11-11-411-1							
TX REAL	TX IHAG	SEVT .	TY Imag	T.Z Real	TZ 1 MAG	₹X Real	RX I HAG	REAL	RY RZ REAL THAG
15875E+00	0.00000	75649E-13	0.00000	-41728E-14	0.00000	•12013E-12	0.00000	·15527E-12	0.00000 .376496+00 0.00000
15875E+00	0.00000	.14186E-13	0.00000	.28922E-13	0.00000	73123E-13	0.00000	.16630E-ÍŽ	0.00000 .376492.00 0.00000
-217526-00	0.00000	681 /50-14	0.00000	495281E-14	0.00000	241095-13	0.00000	359176-13	0,000003-2666-01 0.00000
.21752E+00	0.00000	.76396E-14	_0.00000	~.26739Ē-13	0.00000	42067L-14	0.00000	40307E-13	0.00000 -362666-01 0.00000
-+11797E+00	0.00000	.853311-14	0.00000	.120488-13	0.00000	366026-14	0.0000	. 302578-13	0.00300 <u>.10651F+00</u> 0.00000
117976+00	0.00000	-184082-13	0.00000	-65048E-15	0.00000	.184698-14	0.00000	.10773E-ĨŽ	0.00000 -100512+60 0.00000
-10921E+00	0.00000	. • 13347£ -13	.0.00000	67891E-14	0.00000	658826-14	0.00000_	-, 32626k-13	0.00000664794-01 0.00000
.10921E+00	0.00000	-62301L-14	0.00000	223516-13	0.00000	.25439E-13	0.00000	.13084E-12	0.00000664?9E-01 _0.00000
50006E-01	0.00000	.13517Ê-13	0.00000	-11460E-13	0,00000	.43228t~14	0.00000	33621E-13	C0000028079E-1Z 000000
50006E-01	0.00000	19710E-13	0.00000	.21321E-13	0.00000				
-50006E-01	0.00000	15597E-13		-1566ZE-13		<del></del>			
-50006E-01	0.00000	21648E-13	<u>_0</u> .00000 <u></u>			.955066-15	_0•00000 <u></u>	./1547E-13	0.000001651412 0.00000
-10921E+00	0.00000	.41639E-13	0.00000	71024E-13	0.00000	30350E-13	0.00000	.77071E-13	0.00000 -6.479E-01 0.00000
*10451E+00	0.00000	361711-13	0.00000	68814E-13	.0.00000	318108-14	0.00000_	15160E-12	0.0000066479E-01 _0.00000
:+11797E+00	0.00000	.4d596t-13	0.00000	-38601E-13	0.00006	63388E-14	0.00000	•16238E-12	0.0000010451200 _0.00000
,11797E+00	0,00000	~30380E-13	0.00000	.36898E-13	0.00000	20530E-14	0.00000	17059Ê-12	0.00000106516+00 0.000000
:21762E+03	0.00000	+13217E-13	_0.00000_	_+16447E-13	0.00000	-,109776-13	0.00000	≥61769E-13	0.00000 3.30266E-01 0.00000
,21752E+0J	0.00000	25184E-13	0.00000	.26505E-13	0.00000	.88595E-14	0.00000_	23777E-13	0.00000 .36266E-01 0.00000
15875E+00	0.00000	.20556E-14	0.00000	89626E-14	0,00000	.27222E-13	0.00000	14412Ê-12	0.00000376498+00 0.00000
.15875E+00	0.00000	394698-14	0.00000	23454E-13	0.00000	.20856E-13	0.00000	.78079E-13	0.00000376496+00 0.00000

10,00
21,230,014
*****
7

TX REAL	T.K IHAG	. TY . ieal	TY IMAG	TZ REAL	TZ Imag	K X Real	XX IMAG	RY REAL	KY IHAG	REAL_	TNAG
.15026E+00		15534E-13		.891226-14	0.0000ò	300206-14	0.00000	42218E-12	0.00000	33629E+	0.00
.15026E+00	0.00090	351568-13	0.00000	976398-13	0.00060	.11180E-13	0.00000	50985E-12	0.00000	33629E+	o. 0. 00
21765E+00	0.00000	867908-14	0.00000			24858E-13					
21765E+00	0.00000	46812E-13	0.00000	.47843E-14	0.00000	13305E-13	0.00000	14652É-12	.0.00000		o
-14247E+00		· .25714E-13	0.00000	51596E-13	0.00000	34635E-13	0.0000	19583E-12		51290E-	0.00
.+14247E+00	0.00000	.~15320ā−13	_0.00000	71653E-15	_0.00000	13578Ê-13	0.00000	72113E-13	0 • j ó ó j o o o o o o o o o o o o o o o o	51.290E-	0.00
1705dE+00	0.00000	. +13394L-14	0.00000	_19890E-13	0.00000	277296-14	0.00000	58360E-12	0.00000	149L8E-	0.00
170586+00	0.00090	.454336-14	0.00000	120996-13	`o°0000o',	.488198-13	0.00000	~43602E-12	0.00000	14918E-	01 _ 0 <u>. 00</u>
12950E+00						.11140E-13	0.00000	98168E-13	0.00000	•12950E+	00 0.00
-12950E+00		•		.94817E-14							
12950E+00	0.00000	.92194E-14	_0.00000	.21824E-13	0.00000				er versions	· i . rafafi.	⊼a <b></b> 5 <u>-</u> 5-7
12950E+00	0.00000	61691c-14	0.00000	33103E13		.14436L <u>-</u> 13	0.00000	111068_1		.129701+	AT 6 66
	0.0 <u>0</u> 000	346ZZE-13	0.00000	49690E-13		24108E-13	0.00000	40983E-14			41 - 0 - 0 4
-1705dE+00	0.00000	21069E-I3	000000	57336E-13	0.00000	.95 35 3E -15	_0.00000		ະຼຸບຸນທານດ ເຼັດຈັດຄຸດດັ	51200E	0. 0. 0. 0. 0. 0.
14247E+00	0.00000	.41622 <u>E-13</u>	. 0 • 00 00 0	_'f535jE-T1	0.00000	4u918E-13		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	ร งรับบอบบุ รักที่กักกิดกั	. =•91430E	01 0 0
==14247E+00	0.00000	•29179L-13	0.00000	.795078-14	0.00000	54778E-14	0.00000	120875-1	. 0~000ųų	" 48380E-	02 0.00
21765£+00	0.00000	.991998-14	0.00000	37389E-13	0.00000	21912E-13 12909E-13	0.00000	1285 (6.4)	. , 0.00000 2	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	ōz o o
"•21765E+00	0.00000	35069E-13	0.00000	.344085-13	0.00000	85738L-14	0.00000	.66201E-1	3 0.00000	÷.33629e+	00 0 0
1502oE+00	. 0.00000	26693E-13	0.00000	6/802E-14	0.00000	03130F-F4	3800000	,	,	33629E	

MATHDAL	EPEONS NCY=	.112800£+04

		NATURAL	. FREQUEN	CA= *115800	E+U4			
TX PEAL	IX Dami	TY REAL	TY IHAG ,	TZ REAL	TZ I MAG	KX KX	RK IHAG _	RY RY RZ RZ REAL IMAG
-48124E-13	0.00000	.13893E+00	0.00000	40324E-01	0.00000	16302E+00		27254E-11 0.0000060602E-13 0.00000
		13673L+00				163028+00	0.00000	.29337E-11 0.00000 12783E-12 0.00000
31477E-13		80033E-01				*8913E-01	0.00000	.10518E-11 0.0000056754E-13 0.00000
.95663E-13		+80033F-01		.63895E-01		.889136-01	0.00000	10671E-11 0.00000 38746E-13 0.00000
.664.1E-14		17616E+00"		.73692E-01	0.00000	.25126E-01	0.00000	.34db8E-11 0.00000 18399E-13 0.00000
36706E-13	0.00000			.73692E-01		.25126E-01	0.00000	34637E-11 0.0000025420E-13 0.00000
27058E-13	-	11467E+00				.11420E+00	0.00000	10448E-11 0.0000035704E-13 0.00000
		.11467E+00				.11820E+00	0.00000	11447E-11 0.0000019737E-13 0.00000
18257E-13				~.20873E+00		20873E+00	0.00000	28058E-11 0.00000 .17032E-13 0.00000
		11675E+00						
63367E-13		.11675E+00°						
•10910E-12		- 316750 400	ัก	-:20873È+00	0.00000	200736+00	0.00000	.28741E-11 0.0000049381E-13 0.00000
	0.0000	- 114476300	anaana anaana	*****.21302E+00	ā. ooōoo	" .11820E+00	0.00000	.10762E-11 0.0030021600E-13 0.00000
14603E-13		11467E+00					0.00000	94534E-12   0.00000 -34992E-13 0.00000
+.790908-14	-0.0000		ດ ໂດຍໄດຍສ					.15028E-11 0.00000 18980E-13 0.00000
			0.00000			.25126E-01	0.00000	35418E-11 0.0000019539E-13 0.00000
-54468E-13		.1/6162+00		70056-01	<b>0.</b> 00000		0.00000	.110826-11 0.00000 .25915E-13 0.00000
.95910E-14	0.00000		-		,		0.00000	10373E-11 0.00000 .25644E-13 0.00000
74676E-14				63895E-01				
14345E-13			•	.40324E-01				2811aE-11 0.00000 89231E-14 0.00000
~ .15236E-13	0.00000	139931+00	0.0000	.40324E-01	F 0.00300	103055400	0.0000	

NA THRA	FKEQUENCY=	.119248E+04
MATONAL	LKEGOENC!-	87717407404

TX REAL	IX Imag -	HEAL TY	TY EMAG	TZ REAL	TZ I HAG	RX Real	RX Imag	RY REAL	Y P DARI	REAL _	RZ [HAG
-36195E-13	0.00000	85934E-14	0.00000	20013L+00	0.00000	.42784E+00	0.00000	64178E-13	0.00000	16460E-13	0.00000
11658E-13	0.00000	54705L-13	0.00000	.20013E+00	0.00000	42984±+00	0.00000	10513E-12	0.00000	75684E-13	0.00000
.299288~13	0.00000	27863E-13	0.00000	.11319E+00	0.00060	.185568+00	0.00000	12612E-12	0.00000	71111E-14	0.00000
-•72628E-13	0.00000	.389596-13	0.00000	11319E+00	0.00000	10556E+00	0.00000	.84239E-13	0.00000	10880L-13	
.33423E-13	0.00000	27707E-13	0.00000	.d5664E-01	_ 0.00000	36624E-01	0.00000	57497E-13,	``o• âọeơð	.17015E-13	0.0000
39772E-14	0.00000	.96447E-13	0.00000	856648-01	0.0000	.36a24t-01	0.00000	74930E-13	_0.00000	22077E-14	0.00000
-35663E-13	0.00000		0.00000	.12242E-01	0.000000	353881-01	0.00000	99227E-13	_ စု• စုစစ္တစ္ခ်စ္	10268=-1 <u>3</u>	0.00000
519986-13	0.00000	.23315c-13	0.00000	12242E-01	0.00000	.35388E-Ö1	0.00000	13979E-12	0.00000	.325554-13	0.000007
~58792E-13	0.00000		0.00000	10971E-01	0.00000	21318E_12	0.00000	11680E-12	_ 0.00û <u>00</u>	.23610E-13	0.00000
55526E-13	ğ•000 va	44454£-13	0.00000	10971E-01	`0.000 <i>0</i> 0	, w					
_11402E-12	_0.00000		0.00000	10971E-01							
=-89306E-13	_o <u>.</u> aon áo		0.0000	10971£-01	_0.00000	21024E-12	_ 0_00000		0.00000	-46764E-13	0.00000
•			-			•				18992E-13	
76722E-13	_0.00000_	.798541-14	0.00000	12242E-01		35388E01		_=_47.32556-17	0.00000	.85042E-15	0.00000
11269E-12	0.00000	7-54297L-13	0.00000		_ 0.00000	• 36624E-01	0.00000	78769E-13	6.00000	59176E-13	0.00000
84442E-13	_0.00000	68251E-13	0.00000	65664E-01	~~ oooooo	306244-01	_ 0.00000	61248E-13	0.00000	44591E-13	0.00000
	-	31552E-13		••						44170b-13	
3803AE-13	0.00000	. 400376-13	0.0000	11319E+00	0.00000	~.10556E+00	0.00000	~~15359E-172	0 • 00'n00	20450E-13	0.00000
.359526-13	0.00000	.538528-13	0.00000	20013E+09	0.00000	424846+00	0.00000	.7315>E-13	. 0.00000	28969E-12	0.00000
-38418E-13	0.00000	47d68E-13	0.00000	-20013E+00	0•000 <u>0</u> 0	_ •42984L+00	0.00000	-17155E-12	_n• oò o o	10d56t-12	0.00000

H-40

TX REAL	. XT .	KEAL"	TY IHAG	TZ	TZ THAG	RX REAL	RX THAG	REAL	RY THAG	RÉAL	RZ IHAG
10685E-12	0.00000	83688E-14		20082E+00							
.i2322E-12	0.00000	-,54301E-13	0.00000	.20082E+00	0.00000	43013E+00	_0.00000	-18179E-12	0.00000	.57a94E-13	0.00000
<del>-</del> •9717∂E-13	0.00000	39435E-13	0.00000	. 11248E+00	0.00060	.10583E+00	0.00000	29516E-13	0.00000	19410L-13	0.00000
.86701E-13	0.00000		0.00000		0.00000	105836+00	0.00000	[ .221216-12		32627 <u>E</u> -13	0.00000
78987E-13	0.00000	47346E-Î3	Ó-0000n	. 856246-01	<u>`</u> 0.00000	34726E-01	0.00000	13395E-12		64527E-14	0.00000
				85624E-01							
				16704E-01							
				51597E-01				67936E-14	_o_ooo_oo	46545E-13	0.00000
				51597E-03							
				51597£-03							
				51597Ē <u>_</u> 63							
10886E-12	.0.00000	-,70940E-14	0.00000	16704E-01	0.00000	31_195£_01_	0.00000	56788£-13	0.00000	815426-14	0.00000
16256E-13	0.00000	-19549E-13	0.00000_	16704E-01	.0.00000	31185E_01	.,0.ó <u>0</u> 000	83968E-lij_	0.00000	₹•19313 <u>F</u> -1 <u>3</u>	0,00000
7193d5-14	0.000.00_	381281-13	0.00000	85624E-01	0.00000	34726E-01	0.00000	-15663E-12	0.0000	45893E-13	0.00000
				.85624E-01							
				112486+00							
34882E-13				11248E+00.							
				-20082E+00							
.12355E-12	0.00000	60286C-13	0.00000	20082E+00	0.00000	43013E+00	0.00000	.23854E-12	0.00000	-50670E-13	0.00000

NATURAL FALQUENCY= .119 #40E+04

TX T	IX Y 1AG KEAL	. TY TZ IMAĞ REAL	TZ	KX RK REAL IMAG	RY	IMAG KEAL IMAG
_13119L+00 0.	.000,3011672E-13	0.00000 .1532/E-	-12 0.00000	37830E-12 0.00000	19679E+00	0.0000080559F-11 _ 0.00000
7131196+00 0.	.00000 -:76447E-13	0.00000 -15193E-	12 0.00000 .	27537E-12 0.00000	19674E+00	0.00000738716-11 0.00000
.13119E+00 O.	.00000 .40946E-13	0.0000u71850E	-13 0.00000	96939E-13 0.00000	19679E+00	0.00000 .27391E-11 0.00000
-13119E+00 0.	.00000 .30796E-13	0.00000 .72826E	-13 0.00000 .	67362E-13 0.00000	19679E+00	0.0000027965E-11 0.00000
.13119E+00 0.	.0000010072E-13	0.0000028077E	-13 0.00000 .	38036E-13 0.00000	19679E+00	0.00000 .233a5E-11_0.00000
.13119E+00 J.	.00000 .71030E-13	0.00000 -109446-	-12 0.07000	22022E-13 0.00000	19679E+00	0.00000 [21890E-11 [0.00000_
.13119E+00 0.	.00000539648-13	0.0000086737E-	-13 0.00000 .	54088E-13 0.00000	19677E+00	U.00000972892-12 0.00000
,13119E+00 0.	.00000 .73519L-13	0.00000400316-	-13 0.00000 .	341388-13 0.00000	-+19679E+00	0.0000010089F-11 0.00000
.13119E+00 0.	00000648626-15	0.00000 .41016E	-13 "0"00000"	484966-13 0.00000	19679E+00	0.0000016123E-11 0.00000
.13119E+00 0.	.0000044811E-13	0.0000044551E-	-13_ 0.00000 _			
.13119E+00 0.	.00000 .38556E-15	0.00000u3263E-	-13 0.000000			
_13119E+00 0.	.0000044502E-13	0.000003,45645E-	-ï3 <u>_0</u> .00000 <u></u> .	405216-13 0.00000	19679E+00	0.00000 .14495E-11 0.00000
13119E+00 0.	.00000135536-13	0.00000 .68516E-	-1i 0.00000 ~.	490816-13 0.00000	19679E+00	0.00000 .148554-12 0.00000
	.00000412826-13		-13 0.00000 .	22442 <u>E-13                                    </u>	19679E+00	0.00000349724-14 0.00000
-13119E+00 0.	.0000014851E-13	,0*00000 -*15724E	-13 0.00000 .	241851-13 0.00000	19679E+00	0.0000035791E-12 0.00000
·13119E+00 0.	.00000		-13 0.00000 .	40447E-14 0.0000	19679E+00	0.00000 .51117E-12 0.00000
.13119E+00 0.	.0000030937£-13	. 0.000 <u>00</u> ,,32459E-	-14 _0.00000	149356-13 0.00000	19679£+00	0.00000697786-13 0.00000
.13117E+00 0.	.0000051678£-13	-15149E	-13 0.00000 ``.	51980E-13 "0.00000	~19679E+00	0.00000 -273396-12 0.00000
_13119E+00 <u>0</u>	.00 <u>0</u> 00 <u>-</u> .27179 <u>6-</u> £3	0.0000011728F	-13 J.09000 <del>-</del> .	108566-12 _0.00000	19679E+00	0.0000011003-11 0.0000
+13119E+00 0.	.0000080480E-13	. 0.00000 .25347E	-13 0.00000	852880-14 0.00000	195798+00	_0.00000 .13792t-11 0.00000

NATURAL	<b>FXLUULNCY</b> ≖	.1202788+04

		THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACTOR OF THE CONTRACT	LINEGOLII	0,- 1223210						_ ,
TX REAL	TX DAM1	TY Keal	TY IHAG	TZ REAL	TZ I HAG	RX Real	RX 1HAG	RY Real	THAG .	RZ RZ
.1361LE+00	0.00000	•52467E-13	0.00000	578438-14	0.00000	.19783E-12	0.00000	36563E+00	0.00000	.24117E+00 0.000 <u>00</u>
13611E+00	0,00000	.39601E-13	0.00000	-7865GE-15	0.00000	21392E-12	0.00000	36563E+00	0.00000	24117E+00 0.0000
.13474E+00	0.00000	23400E-13	0.00000	.72026E-13	0.00000	+43506E-13	0.00000	36984E-01	0.00000	.79296E-01 0.00000 _
13474E+00	0.00000	.13011E-13	0.00000	78411E-13	0.00000	149788-13	0.00006	36984E-01	0.00000	79296E-01 0.00000
21215E-01	0.00000	929836-13	0.00000	.42357E-13	0.00000	37d07E-13	0.00000	32993É-01	0.00000	.6170jE-01_ p.00000_
-21215E-01	0.00000	41978E-13	0.00000	-+59664E-14	0.00000	.39654E-13	0.00000	32993E-01	0.000,00	61701E-01_0.00000
.11144E-01	0.00000	707771-13	0.00000	490d1E-13	0.00000	393648-13	0.00000	.99759E-01	0.00000	.21214E-01 0.000000
111448-01	0.00000	278781-13	0.00000	145798-13	0.00000	.42230E-13	0.00000	.497591-01	U.00000	21214E-01 0.00000
64030E-01	0.00000	.64986E-13	0.00000	.35125E-13	0.00000	329586-13	0.00000	26560E-11	0.00000	64030E-01 0.00000
-64030E-01	0.00000	.42350E-13	0.00000	.431378-13	0.00060					
-64030E-01	0.00000	.63052E-13	0.00000	46172E-13	0.00000	-				
64030E-01	0.00000	.42961E-13	0.00000	25766E-13_	0.00000	33576E-13	o•oooń		0.00000	.64030E-01 0.00000
11144E-01	0.00000	327,376_13	. j. 00 0 0 j	.627538-13	0.00000	.327178-13	_0,00000		_ 0 • 0 0 0 0 <u>0</u>	.21214E-01 0.00000
11144E-01	0.00000	.17777C-13	0.00000	.55934E-13	`â.aoáoo	.22157E-13	0.00000	99759E-01	0.00000	21214E-01 0.00000
21215E-01_	0+00000	66671E-13	0.00000	50294E-13	0.00000	18902E-13			_ 0•,000,00	.61701E-01 0.00000
21215E-01	0.00300	20124£-13	0.00000	37939E-13	0.00000	60718E-14	0.00000	.32993E-01	_0.00000	61701E-01 0.00000
1-13474E+00	0.00000	je501E-13	0.00000	16280E-13	0.00000	.622106-14	. 0.00000	.36984E- <u>0</u> 1	_n• ooogo	.79296E-01 0.00000
134746+00	. 0.00100	38512L-13	0-00003	.105446-13	0.00000	-24544E-13	0.00000	-369848-01	0.00000	79296E-01 0.00000
=.1361LE+00	0.00000	•11299E-12	0.00_000	.43197E-13	9.00000	37701E-13	0.00000	_ •3656JE+00 [*]	. 0.00000	-24117E+00 0.00000
-13611E+00	3.00000	352068-14	0.00000	16170E-13	0.00000	79234E-13	0.00000	.36563E+0u	0.00000	24117E-00 0.0000

```
Tx
REAL
                                                                           REAL
                                       REAL
                                                IHAG
                                                          KEAL
                                                                 IMAG
          IHAG'
                    REAL
                             IHAG
                                                                          .32835E+00 0.00000 -.27462E+00 0.00000
                  -.67524E-13 0.00000 -.10077E-12 0.00000
                                                        .40141E-13 0.00000
-10132E+00 0.00000
.10132E+00 0.00000 -.75297E-13 0.00000 .46113E-13 0.00000 -.71775E-13 0.00000 .32835E+00 0.00300 .27462E+00 0.00000
                                                       .49436E-13 0.00000 -.26183E-01 0.00000 -.79082E-01 0.00000
                                     .52627E-13 0.00000
-.9826dE-01 0.00000
                  .17747e-13 0.03000
$98268E-01 0.00000 233436-13 0.00000 42212E-14 0.00000 -.64504E-13 0.00000 -.26183E-01 0.00000 79082E-01 0.00000
$55550E-01 0.00000 -79339E-13 0.00000 -88860E-14 0.00000 -54880E-13 0.00000 -37810E-01 0.00000 -.70197E-01 0.00000
                  .31644E-13 0.00000 -.96790E-13 0.00000 .31277E-14 0.00000 -.37810E-01 0.00000 -.76197E-01 0.00000
-.55556E-01 0.00000
                  .14050E-13 0.00000 -.61243E-14 0.00000 -.11164E-13 0.00000 -.13846E+00 0.00000 -.1686E-01 0.00000
-54992E-U1 0.00000
_.54992E-01 0.00000 -.41459E-13 0.00000 _.16286E-13 0.00000 _.23794E-13 0.00000 -.13846E+00 0.00000 -.16886E-01 0.0000
.89043E-01 0.00000 -.52016E-13 0.00000 -.87854E-14 0.00000 .36410E-13 0.00000 -.12590E+00 0.00000 .25554E-11 0.00000
-.89043E-01 0.00000 -.10881E-13 0.00000 -.14810E-13 0.00000
".890436-01" 0.00000 -.516686-13" 0.00000 ".419126-13" 0.0000
-.89043E-01 0.00000 -.13948E-13 0.00000 -.4586E-13 0.00000 -.12590E+00 0.00000 -.24052E-11 0.00000
.54992E-01 0.00000 .43836E-13 0.00000 -.67592E-13 0.00000 -.91052E-14 0.00000 -.13846E+00 0.00000 .16886E-01 0.00000
-.54992E-01 0.00000 -.19410E-13 0.00000 -.40621E-13 0.00000 -.49933E-13 0.00000 -.13846E+00 0.00000 -.16886E-01 0.00000
-.55556E-01 0.00000 -.11437E-13 0.00000 0.00000 -.27700E-13 0.00000 -.37810E-01 0.00000 -.76197E-01 0.00000
-.9826#E-01 0.00000 .46672E-13 0.00000 .44001E-13 0.00000 -.1/604E-13 0.00000 -.26183E-01 0.00000 7.79082E-01 0.00000
                  .34514E-13 0.600000 .23159E-13 0.00000 -.14875E-13 0.00000 -.26183E-01 0.00000 -.7908ZE-01 0.00000
.98268E-01 0.00000
.10132E+00 0.00000 -.93134E-13 0.00000 -.37534E-13 0.00000 .64332E-13 0.00000 .32835E+00 0.00000 .27462E+00 0.00000
.1013/E+00 0.00000 .20269E-13 0.00000 -.29246E-13 0.00000 .53152E-13 0.00000 .32835E+00 0.00000 -.27462L+00 0.00000
```

RХ

-120186E+04

ΤZ

NATURAL FREQUENCY=

7
Stantin
SW.S
Z

TX REAL	TX TY KEAL	- TY -	`TZ REAL	TZ IHAG	RX REAL _	RX	RY RY RZ RZ REAL IMAG KEAL IMAG
*23455E-14	0.09000 .589d9E-1	4 0.00000	-156696-12	0.00000	.56467E-13	0.00000	-21426E+00 0.0000032914E-13 0.00000
.89637E-14	0.0000014190E-1	3 0.00000	108456-12	0.00000	-15698L-1Z	0.00000	21426E+00 .0.00000 .11825E-13 0.00000
-27054E-14	0.00000 .80549L-I	3 9.60000	813306-14	0.00000	188681-12	0.00000	28868E+00 0.0000068635E+13 0.00000
276628-14	0.00000681406-1	3 0.00006	89283E-13	0.00000	.50004L-13	0.00000	.28868E+00 0.0000010683E-13 0.00000
•350d3&-13	0.00000 .239246-1	3 0.00000	-•10091E-12	0.00000	13791E-12	0.00000	11401E+00 U.0000086682E-14 _0.00009
222491-13	0.00000149240-1	3 0.00000	.16212E-12	0.00000	+10708c-12	0.00000	.114016+00 0.00000 .32611e-14 _0.00000
-•22265E-13	0.00000509858-1	3 0.00000	-,283088-12	_0.00000	. •30766t-13	_0.00000	. 32827E+00 _0.00000770576-14 _0.00000
61006E-14	0.00000 .48381E-1	3 0.00000	.1577eE-12	0.00000	-43421E-13	0.00000	32827E+00 0.0000047218E-13 0.00000
-124856-13	0.00000 -895716-1	4 0.00000	11030E-12	0.00000	.76236E-13	0.00000	-19398E-12 0.00000 39563E-13 0.00000
-18651E-13	0.00000 .27415E-1	3 0.00000	18802E-12	0.00000	•		
-+297556-13	0.0000073609E-1	4 0.00000	72107E-14	0.00000			
•31773E-13	0.00000 -31180E-1	3 0.00000	82240E-13	0.00000	159821-12	0.00000	108346-15 0.00000 .365996-14 0.00000
87302E-14	0.00000118716-1	3 . 0.00000	·13472E-12	0.00000	.56911E-13	0.00000	32827E+00 0.0000023099E-13 0.00000
-275826-13	0-00000 -34717E-1	4 0.00,000	~.92106E-13	0.00000	~.311196-13	0.00000	.32827E+00 0.0000039235E-13 0.00000
22653E-13	0.00000 .359508-1	3 0.00000	±,11956E+12	0.00000	-13078L-13	_ 0.00000	-11401E+00 0.0000087864E-14 0.00000
.39254E-13	0.00000396655-1	3 0.00000	16958E-12	0.00000	36199E-13	0.00000	11401E+00 0.00000 12912E-13 0.00000
897146-15	0.0000053759E-1	30.00000	_ • 22259E-12	_0.000¢ĝ	21303E-13	0.00000	-28868E+00 0.0000030605E-13 0.00000
. +26898E-14	0.0000044597L-1	á ¯ 0.6∪00ŏ¯	13662E-12	0.00000	3u664c-13	0.00000	28866E+00 0.0000024091E-13 0.00000
31048E-13	0.00000	3 0.00000	. 1247 /E-12	0.00000	.544 i 3L-13	0.00000	21426E+00 0.0000011700E-13 0.00006
.13235E-13	0.00000 .200706-1	3 0.00000	14474E-12	0.00000	_+1v343L-12	0.00000	.21426E+00 U.0UUUU68453E-14 _0.00000

NATHNAL	Fire CHI NCY=	1181645 406

	TX	T4 LHAG	TY KEAL	TY IMAu	TZ Real	TZ.	K KE A L	RK IMAG	RY	HAĞ.	REAL	ŘZ THAG —
	-61737E-01	0.00000	204548-13	0.60000	* -134265-12	0.00060		- "				
	61737E-01	000000 €C	~.16225E-13	0.00000	11164E-1Z	0.00000	.29097E-12					
	53717E-01	, o • o o o o ·	.152708-13	ō•0000ú	97864E-13	0.00000	58699E-13	0-00000	1027QL+00	0.00000	35376E-	-01 0.00000
	=.53717E-01.	0.00000	270796-13	0.00000		_0.00000	-94229E-13	0.0000	10270E+00	_ o. oco o o	•35376E-	-01 0.00000
	13798E+00	0.00000	. 28715E-13	0*00000	Z91g2E-L3_	~ v.0000ō		0.00000	79794E-01		-20936E-	-01-0-00000
	13798E+00	0.0000	-210841-13	0.00000_		0.00000	26179E-13	`0.0000 <i>o</i> `	79994E-01		20936E-	-0 <u>1 0.0000</u>
	-82324E-02	0.0000ò	.11850L-13	0.00000	•23946E-13	0.00000	.45214E-13	0.00000	31940E+00	0 . 0 0 0 0 0 0	54814c-	0.0000
	82324E-02	0.00000	-33988E-13	_0.cooou		0.00000	225401-13	0.00000	31946L+C0	0.00000	.548146-	01 0.60000
Ħ	-25744E+00	0.00000	47021E-13	0.00000	37889E-Ï3	0.000000	.18445E-13	0.00000	67834E-13	ij. 000 d <u>0</u>	25744E	000000
1-4	25744£+00	0.00000_	-22320E-13	0.00000	-,31900L-13	0.00000						
O)	25744E+00	0.00000	48964t-13		100182-13	0.00000						
	25744E+00	0.00000	20653E-13	o.60000g		0.00000	, 231 32C-13	0.00000	235986-12	0.00000	25744E	00 0.00000
	-182324E-02 .	0.00000_	224536-13	ó.000g0 <u> </u>	·232836-13	`o`ooōoo`	12356E-13	0.00,000		_0.00000 <u>.</u>	54814E-	-01 0.60000
	.82324E-02	0.00000	113348-14	0.00000	10912E-13	0.00000	.107936-13	0.00000	319465+00		54814E-	01 0.00000
	.13798E+00	0.00000	-43135E- <u>13</u>	0.00000	64829E-14	0.00000	27923E-13	0.00000	799 <u>9</u> 4E-01	0.00000	.20936Ê-	0.00000
	.13798E+00	0.00000	76544E-14	0.00000	.68564E-14	0.00000	355116-13	0.0000	.79994E-01	0.00000	20936E-	01 0.00000
	-+53717E-01	0.00000	.93228£-14	0.00000	.25629E-14	0.00000	30443E-13	0.00000	` .10270E+GQ	0. 000 00	353768-	-01 0.60000
	.53717E-01	0.00000	22880E-13	0.00000	-31080E-15	0.00000	42140£-13.	0.00000	.102 70L+00	6.00000	35376E-	01 0.00000
	61737E-01	0.00000	156728-13	0.00000	638996-14	0.00000	+13036E-13	0.00000	.96818F-0Î	0.00000	-60496E-	-01 0.00000
	.61737E-01	1.00000	55979É-14	0.00000	08367E-14	0.00000	.45354E-14	0.00000	.96818E-0ĺ	0.00000	-+609961-	01 0.00000
	•			•		•			•			

" NATUPAL FREQUENCY= .1231476+04 TZ ' - TX .. TY 17 RX REAL .13936E-13 0.00000 -.37908E-13 0.00000 -.46685E-13 0.00000 .10027E-01 0.00000 -.28216E+00 0.00000 .89492E-01 0.00000 -89492E-01 0.00000 -.54418E-13 0.00000 .41469E-13 0.00000 -.25330E-13 0.00000 .10027E-01 0.00000 .28216E+00 0.00000 .46351E-01 0.00000 .28497E-13 0.00000 -,18318E-13 0.00000 .39009E-13 0.00000 -,27720E+00 0.00000 .12517E-01 0.00000 -.46351E-01 0.00000 .60125E-14 0.00000 .4956JE-13 0.00000 -.52397E-13 0.00000 -.27720E+00 0.00000 -.12517E-01 0.00000 .64333E-01 0.00000 .11660E-13 0.00000 .85904E-14 0.00000 .39538E-14 0.00000 .80737E-01 0.00000 .59509E-01 0.00000 -.64333E-01 0.00000 .27887E-13 0.00000 -.48824E-14 0.00000 -.36705E-13 0.00000 -.80737E-01 0.00000 -.59509E-01 0.00000 -.63007E-01 0.00000 -.12666E-13 0.00000 -.67391E-14 0.00000 .31038E-14 0.00000 .10621E+00 0.00000 .1088E-00 9.00000 .63007E-01 0.00000 .54505E-14 0.00000 -.21903E-13 0.00000 .18773E-13 0.00000 .10621E+00 0.00000 -.1088dE+00 0.00000 -.13717E+00 0.00000 -.30824E-13 0.00000 -.48034E-13 0.00000 -.36607E-13 0.00000 .24170E+00 0.00000 .54863E-12 0.00000 _-13717E+00 0.00000 --85468E-14 0.00000 --56466E-14 0.00000 -- 13717E+03 0.00000 -- 30653E-13 0.00000 -- 29444E-13 0.00000 -13717E+00 0.00000 --12659E-13 0.00000 --12659E-13 0.00000 --77424E-14 0.00000 -24170E+00 0.00000 --48251E-12 0.00000 -.63007E-01 0.00000 -.44274E-15 0.00000 -.28528E-13 0.00000 .24825E-13 0.00000 .10621E+00 0.00000 -.10888E+00 0.00000 -630076-01 0.00000 -176796-13 0.00000 -399016-13 0.00000 -13198-13 0.00000 10000 0.00000 .100000 0.000000 .11602E-13 0.00000 -.34661E-13 0.00000 -.80737E-01 0.00000 -.59509E-01 0.00000 -6433JE-01 0.00000 .34570L-13 0.00000 -.64333E-01 0.00000 -.39432E-14 0.00000 -.16673E-13 0.00000 -.19804E-13 0.00000 -.80737E-01 0.00000 -.59509E-01 0.00000 -46351E-01 0.00000 -57039E-13 0.00000 -63425E-14 0.00000 -.12678E-13 0.00000 -.27720E+00 0.00000 -.12517E-01 0.00000 .95339E-14 0.00000 -.47d80E-13 0:00000 -.27720E+00 0.00000 1.12517E-01 0.00000 --46351E-01 0.00000 .15616E-13 0.00000 .22104E-13 0.0000 -10732E-14 0.00000 .10027E-01 0.00000 -22216E+09 0.00000 .89492E-01 0.00000 -.14171E-13 0.00000 -.89472E-01 0.00000 -.206214-13 0.00000 -.22270E-13 0.00000 .32138E-13 0.00000 .10027E-01 0.00000 -.28216E-00 0.00000

### NATURAL FREQUENCY= .1219161+04

TX REAL	XT DAMI	TY .	TY THAG _	TZ KEAL	TZ IHAG ,	RX . KEAL	KX IMAG	RY REAL	ŘŶ	REAL	RZ THAS
10034E+00	0.00000	.51093E-13	0.00000	.977758-13	0.00000	233116-12	0.00000 '	. 20654£-02	0.00000		
10034E+00	0.00000	29017É-13	0.00'000	84424E-13	0.00000	.15969E-12	0.00000	20654E-02	_0.00000	28552E+00	0.0000
76487£-01	0.00000	378756-13	0.00000	57911E-13	0.00000	.13631a-13	0.00000	.29451E+00	0.00000	.41771Ê-02	
.76487E-01	0.00000	.25233E-13	0.00000	.19214E-13	0.00000	.66409E-13	`o.0000ó ``	.294516+00"		4177E-02	0.00000
10597E+00	a•0090 <u>0</u>	19138E-13	0.00000	-+39967E-15	0.00000	.35185£-14	`ö.ooooo * `	[18416E+00]	_0.00voo;		0.0000
10597E+00	0.00000	32621E=13	[0000co.d	93713E-13	0.00000	19491E-13	`0.0000 <u>ò</u>	.18410E+00		799406-02	0.0000
61947E-01	0.00000	345336-13	0.00000	37344E-13	0.00000	.51728E-13	0.00000	608206-02_	0.00000	10203E+00	0.00000
.61947E-01	0.00000	.25713E-13	0.00000.	91055E-14	0.00000	60867L-14	0.00000	60820E-02	_0400000 <u>_</u>		0.0000
-91187E-01	ó.00000 ⁻	10270E-13	0.00000	i2525E-13_	0.00000	`-+82310E-14	0.00000	411656-12	0.00000	.9118 <u>7E-01</u>	0.00000
91187E-01	0.00300	18372E-13	0.00000	10009E-13	0.00000	<b>-</b>					
91187E-01	0.00000	.983336-14	0.00000	288258-14							
-91167E-01	ຼີດ ເດ່ວດດ່ວ ຸ້	26235E-13	0.00000	319346-113	0.0000	10637E-13	_ o.ooooo	45364E-12	0.0000	91[87 <u>E-01</u>	0.00000
-61947E-01	3.00000	.13524E-13	0.00000	-93051E-L4	0,00000	10779E-13	0.00000	_60820E-02	0.00000		0.0.000
61947E-01	0.00000_	47386E-14	0.00000	.36175E-13	0.00000	39751 <u>6</u> -14	0.00000	60820£-02	_0•003 <u>00</u>	.1 <u>0</u> 203E+00	0.00000
•10597E+00	0.00000	713419E-13	0.000007	76401E-15	0.00000	23321 <u>E</u> -14	_0.00000;	18410E+00	0.00000	79940E-92	0.00000_
10597E+00	~00J00~	-18944Ê-Î3	0.00000	12054E-13	<b>0.</b> 00000	648381-14	0.00000	18410E+00	0.00n_00	79940E-02	0.0000
.76407E-01	0.00000	.47638E-14	0.00000	38220E-14	0.00000	11181 <u></u>	0.00000	-1294516+00	0.000000	_41771E-02	
76487E-01	0.00000	-144975-13	0.00000	.18602E-14	0.00000	.21>176-13	0.00000	29451E+00	0.00000	41771E-02	0.0000
10034E+00	0.00000	56930E-14	0.00000.	42733E-1,4]	0.00000	.16747E-Ì3	0.00000	20654E-02	` <b>0.</b> 00000	.28,552E+00	0.000000
==10034E+00	0.00000	186431-13	0.00000	.67008E-15	0.00000	.249871-13	0.00000 _	206542-02	.G. 00000	285525+00	

MATHD AL	CALDIII NC V	- 1274441 + 114	

				Y= .127844							
TXREAL	THAG	TY ŘEAL	TY THAG	- TZ	TZ	RX . Real	RX IHAG -	RY REAL	RY	RZ REAL	RZ IHAG
20150E-13	0.00000	.503346-12	0.00000	.35519E-12	0.00000	46221E-12	0.00000	•19629E+00°	0.00000	13071E_13	<u>.0.00000</u>
		50490L-12									
44272E-14	0.00000	=56507E-12	0.00000	_11'015E-11	0.00000	.97105E-14	0.00000			74526t-13	
		.55489E-12								d32386-14	
.462066-14	0.00000	60848E-12		12155E-12	0.00060						
		.694835-12								35169E-13	
·35569E-13	0.00000	.39220E-12	0.00000	-:48810E-12		65353L-12	0.00000	-31760E+00	0.00000	39737t-14	0.00000
.337576-14	0.00000	36571E-12	0.00000	-12537E-11	6.00000	2286E-12	0.00000	-,31760E+00	0.00000	27660E-13	0.00000
		.733261-12			,		0.00000	19629E+00	0.00000	42032E- <u>1</u> 3	0.00000
		71085£-127									
		.70667E-12					**	1 <del>** =</del> , 2, <del>**</del> , ** = 2 2 2		·	
		330726-12									
		35649E~12									
		69152E-12									
		50962E-12									
			•							195816-13	
		.513415-12									
		46525E-12									
**********	, 4455450	**********	740000	,						•	

NATURAL FREQUENCY= .129134E+04 TZ REAL . TX REAL TΧ TY ΙY 12 RХ Rx RY ۲Y INAG REAL INAG IHAG REAL INAG REAL DAMI REAL _ IHAG -.679365-14 0.00000 -.12769L+00 0.00000 .4819ZE-12 0.00000 .5d405E-14 0.00000 .11960E-13 0.00000 0.00000 -.8//352-01 0.00000 -.149516-13 0.00000 -28283E-14 0.00000 -.30542L-13 0.00000 .127690+00 0.00000 .87735E-01 0.00000 -.52011E-12 -.14283E+00 0.00000 -.66238E-12 0.00900 -.10014t-13 0.00000 -.26797E-13 0.00000 -10531L+00 0.00000 .12643E-13 0.0000U --17830E-13 U.00000 .11803£-13 0.00000 .142436+00 0.00000 -.10531E+00 0.00000 .70873E-12 0.00000 -.17641E-13 0.00000 -.6363/E-13 0.00000 -.19991e-14 0.00000 -.11603E-13 0.00000 -.29481E-13 0.00000 .9987dE-01 0.00000 .20670±+00 0.00000 -.99878E-01 0.000ug .937266-13 0.00000 -.328476-14 0.00000 .45804E-13 0.00000 -.20b70t+00 0.00000 0.00000 .759148-12 0.00000 .886456-15 0.00000 -.12627E-13 0.00000 -.15012E-13 0.00000 .3045dE+00 0.00000 -41/25[-01 .17172L-13 0.00000 -.30458E+00 0.00000 -.41725E-01 0.00000 -.72148E-12 0.00000 .13839E-13 0.00000 -.76487E-15 0.00000 --92314E-14 0.00000 -.15837E-15 0.00000 .19031E+00 0.00000 -.13031E+00 0.00000 -.42918E-12 0.00000 -.84287E-15 -17554E-13 0.00000 -.16653E-13 0.00000 -.19031E+00 0.00000 .88398E-14 0.0000 -. TB121E-13 0.00000 -. 190111+00 0.00000 --38485E-13 0.00000 --35743E-13 0.00000 19031E+00 0.00000 0.19031E+00 0.00000 38225E-12 0.00000 17242E-13 0.00000 -.24051E-13 0.00000 .547256-14 0.00000 -.30458E+ÔU 0.00000 -.417256-01 0.0000Ô -.55325E-12 0.0000Ô 537176E-13 0.0000Ô -42571E-13 0.00000 -.15348t-14 0.00000 .3045dE+00 0.00000 -.41725t-01 0.00000 -.49105E-12 0.00000 -.41713c-13 0.09900 -.45428E-13 0.00000 .37622E-14 0.00000 F.99878E-01 0.00000 .20b70E+00 0.00000 .15410E-12 0.00000 .32168E-14 0.00000 -.Z0040E-13 0.00000 -.Z0570L-13 0.00000 1.14283£+00 0.00000 .10531t+00 0.00000 -.53339E-12 0.00000 -.26d82t-13 0.00000 .37634E-13 0.00000 -13893t-13 0.00000 --14283t+00 0.00000 --13531t+00 0.00000 -53559t-12 0.00000 -51383t-13 0.00000 .11014E-13 0.000JO .34/34E-14 0.000GJ .12769£+00 0.00000 --87735£-01 0.00000 .28895£-12 0.00000 .48901E-13 0.00000 -60250E-15 0.00000 -.77106E-14 0.00000 -.12769E+00 0.00000 .87735E-01 0.00000 -.29712E-12 0.00000 -.88790E-13 0.00000

Ž.	
35	
ŧ	
¥	

τx	1,4	ΤΥ	ΤΥ	TZ	T Z	R.K	8 X	RY Real	KT 1HAG	44 u£ai	THÂĞ"
REAL	IMAG	KEAL	IMAG	RLAL	IMAG	KE AL	IMAG	••	-	-	
.29161E-13	0.00000	.754528-13	0.00000	•20326E•00	0.00000	.350386-01	0.00000	52083E-12'	0.00000	35900F-13_	_0.00000_
.527648-13	0.00000	30717E-13	0.00000	203266+00	0.00000	35038c-01	0.00000	.444758-12	0.00000		,
.76536E-14	0.00000	11675L-12	0.00000	.2080 dE+00	0.00006	75291E-01		•63252E-12		.65885E-13	
.22175E-13	g-00000	.802216-13	0.00000	20888E+00	0.00000	.752916-01	0.00000	72690E-12	0.00000		
.301758-13	0.00000	42018E-13	0.00000	.42646E-01	0.00060	18396L+00	0.00000	.134148-12			
.21350E-13	0.00000	·103826-13	0.00000	42046E-01	0.00000	-14396£+00	0.00000			281d9c-13	
•47995€-L3	0.00000	.64399t-13	0.00000	184806+00	0.00000	14612E+00	0.00000	64403E-12	0.00000	-, 585776-13	0.00000
.583356-13	u.00000			.18460L+00					0.00000	.263775-13	0.00000
-15251E-L3	0.00000					449426-12	0.00000	.402608-12	0.00000	332636-13	0.00000
.49466E-13	v.00000	565556-13	6.00000	-26999E+00	0.00000						
.74992E-14	0.0000		0.00000	Z6999È+00_	_ 0°00000	•					
.63500E-13	J.00J00	328296-13	`0.00000	269976+00	0.00000	.64615E-12	0.00000	38697£-12	0.00000	52242E-I3	0.00000
•32463E-13	0.00000	22985E~13	อ. ยบโกอย	~+ L8480E+00		.14012E+00	0.30000	53081E=12	_n:00n0ò	591756-13	0.00000
		31636E-13	_0.02000	L8480E+.00	0.00000	14612E+00	_0.00000	-42710E-12	0.00000	-41038E-13	0.00000
-41604E-13	_	733826-13	0.00000	.42646E-01	0.00000	.18376E+00	0.00000	18947E-12	0.00000	-313534-14	0.03000
.258278-14	000000	.49240E-13	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	- 426468-01	0.00000	-118396E+00	0.00000	.35750E-13	Ď. 00000	7600eL-L3	0 <u>*</u> _03003_
-601385-14	o.0000a	303102-13	ô <b>∙</b> ỗ? 000	20888E+00	0.00000	.75291£-01	0.00000				
16771E-13	0.00000	.520236-13	ō• 0aique	20888E+00	0.00000	75291E-01	0.00000	47740E-12	0.00000	92849E-13	0.00000
535348-13	~ a.aoooo	.34953E-13	~o.`ooooa	.20326E+00	0.00000	35039E-01	0.00000	21723E-12	0.00000	520291-13	0.00000
.25278E-13	, 0.00000	354798-13	0.00000	20326E+00	_0.00000	.350386-01	0.0000	28719E-12	. ö• očaoč		~ 0.50000

### NATURAL FREQUENCY= .131763E+04

TX REAL	TX	- "KEVT"	TY INAG	T.L REAL	TZ IMAG	RX Real	RX IMAG _	RY KY KZ RZ RZ REAL IMAG
-10666E+00	0.00000	800458-13	0.00000	,92997E-13	0.00000	.46898E-13	0.00000	-11406E+00 0.00000 -21429E 00 0.00000
-106634	0.00000	20042E-13	0.00000	•11620E-12	0.00000	e256856-13	0.00000	.114066+00 3.00000 21429= 00 0.00000
.34183E-01	0.00000	•444966-13	0.00000	79406E-13	0.00000	94622E-13	0.00000	.88106E-01 0.0000015274E+00 0.00000
34183E-01	0.00000	46855E-13	0.00000	-98024E-13	0.00000	68459E-13	0.00000	.88106E-01 0.00000 .15274E+00 0.00000
-100456+00	0.00000	•33947E-13	0.00000	13042E-12	0.00000	42421b-13	0.00000	30280E+00 0.0000025308E-01 0.00000
·•10045E+00	0.00000	-44866E-13	0.00000	-12891E-12	0.00000	•62o31E-13	0.00000	30280E+00 0.00000 .25308E-01 0.00000
.68169E-01	0.00000	504866-14	0.00000	10910E-12	0.00000	.73559E-13	,0.00000	84213E-01 [0.0000014597±+00 [0.00000]
68169E-01	0.00000	.24082L-13	0.00000	•64574E-13	0.00000	10190E-13	0.00000	84213E-01 0.09000]14547E+00_ 0.00000
96136E-01	0.00000	•90043E-14	0*00000	81857E-13_	_0.00000	19445E-13	0.00000	.18485E+000.0000011867E-110.00000
•96136E-01	0.00000	568621-13	0.00000	•58302E-13	0.00000			
9613bE-01	.0.00000	•77822L-14	0.00000,	- <u>-</u> 12157€-12	0.00000			
•96136E-01	0.00000	56006E-13	0.00000	.:17033E-12_	0.00000	.548146-13]	_0.00000	-18485E+00 0.00000 -81511E-12 0.00000
.68169E-01	0.00000	+454346-13	0.00000	17314E-12	0.00000	52016E-13	0.00000	84213E-01 0.0000014597E+00 0.00000
68169E-01	0.00000	. 154518-13_	0.00000	.18460E-12	0.00000	.37804E-13	0.00000	84213E-01_0.0000014597E+000.00000
-10045E+00	0.00000°	276276-13	0.60000_	~18937E-12	0.00000	.442386-13	0.00000	30280E+00 _0.0000025308E-01 _0.00000
10045E+00	0.00000	.78875É-13	0.00000		_0.00000°	-68648E-13	0.0000	30280E+00 _0.0000025308E-01 _ 0.0000
-34183E-QI	0.00000	23453E-13	0.000,00	17785E-12	_0.00000	25888E-13	_0.00000	.88106E-01 0.00000 .15274E+00 0.00000
34183E-01	0.00000	.605596-14			_0.00000_	-31306E-13		.68106E-01 0.00000152746+00 0.00060
- <u>-</u> 10666E+00	ō•00000_	-30160€-13	. ó • ōa o o o	13884E-12	_0.00000.	45739E-13	0.00000	.114066+00 _0.00000214296+00 _0.00000
•10665E+00°	0.00000	47850E-13	0.00000	-15887E-12	0.00000	30843E-14	0.00000	.11406E+00 0.00000 .21429E+00 0.0000

### MATURAL Frequency: .13111221+04

TK REAL	1.4 1.446	T Y	TY IHAG	VEWF LT	T Z L HAG	· KŁAL	KK KK	RY REAL	Y Y I MAG	KEAL KEAL	RZ Inau
.20643{-13	0.00000	54604c-13	0.00000	-,28017c+00	0.00000	226238-02	0.00000	18249E-12	0.00000	262088-13	0-00000
-9507 pt-14	J.00J90	.204986-13	0.00000	.286178+00	0.00000	.22623E-02	0.00000	.169508-12	0.00000	21620E-13	0.00000
1996of-Ls	0.00000	.91490£ -13	0.00003	28046£+00	0.00000	.23102E-01	0.00000	.28697E-12	0.00000	237844-13	0.00003
46166E-14	0.00000	61868E-13	0.00000	.20045E+00	0.00000	231026-01	0.00000	29570E-12	0.00000	109786-13	0.00000
104016-13	J.00000	.103116-13	0.00000	-,23336E+00	0.00000	-66293E-01	0.00000	.945741-13	0.00000	-245898-13	9.60000
+299006-13	0.00000	13808E-13	0.00000	.23336E+00	0.00000	66293L=01	0.00000	57588E-13	0.00000	151556-13	0.0000
47220E-13	0.00000	518456-13	0.00000	14545E+00	0.00000	.81508E-01	0.00000	28283E-12	0.00000	91969E-14	0.00003
-187036-13	0.00000	.37140E-13	0.00000	.14545E+00	0.00000	81508E-01	0.00000	-35720E-12	0.00000	.51463E-14	0.00000
.188346-13	0.00000	-,21910E-13	0.00000	-,67405E-01	0.00000	.67405E-01	0.00000	.14011E-12	0.00000	. •17142E-13	0.000 <u>0</u>
-195516-13	0.03000	.64434E-14	0.60000	.674056-01	0.00000						
589596-13	0.00000	15391E-13	0.00000	.67405E-01	0.00000						
•53187E-14	0,00000	.183728-13	0.00000	67405E-01	0.00000	67405E-01	~0.00000°	68741E-13	0.00000	.254496-14	ō-0000ō
.64241c-13	0.00000	.13476£-13	0.00000	.14545E+00	0.00000	.815086-01	0.00000	84909E-13	0.00000	57631E-13	0.00000
252916-13	0.00000	121736-13	0.00000	145458+00	0.00000	81508E-01	0.00000	.5549bE-14	0.00000	.243836-13	0•0 <u>ď</u> 000
.446511-13	0.00000	· L4520E-13	0.00006	.23336E+00	0.00000	.66293t-01	0.00000	140768-12	0.00000	.35975E-14	0.00000
50727E-13	0.00000	29741E-13	0.00000	23336E+00	0.00000	66293E-01	0.00000	14513E-12	0.00000	71783E-13	0.00000
163676-11	0.90000	•14500L~13	0.00000	.28046E+00	0.00000	-23102t-01	0.00000	.99340E-13	U.00000	.108126-12	0.00000
201836-13	0.00000	24876E-13	0.00000	2804uE+00	0.00000	23102E-01	0.00000	.30237E-13	0.00000	70198L-13	3.00 <u>0</u> 00
191146-13	0+00010	252316-13	0.00000	. 28017E+30	0.00000	22623E-02	0.00000	.27172E-13	0.00000	10598E-12	0.00000
.757931-13	1.00000	.201316-13	0.00000	260176+00	J.00000	.22a23ë-02	0.00000	.78653E-13	0.00000	.74926E-13	0.00000

The light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the light of the l

# NATURAL FREQUENCY= .136237E+04

T×	TK	TY	TY	7.7	TZ	RX	RX	RY	, ky	RZ	RZ
REAL	IHAG	. REAL	IHAG	REAL	I MAG	. KEAL	IHAG	REAL	DAKI	REAL	THAG
27748E-14	0.00000	19527E-01	0.00000	.35496E-01	0.00000	•30667E+00	0.00000	.62218E-13	u.00000	17837E-13	0.00000
~37514E-13	0.00000	175276-01	-0.00000	35476E-01	0.00000	-30667E+00	0.00000	72065E-13	_0.00000 <u>_</u>	61450E-13	0.00000
11380£-13	0.00000	*ST188C+00	0.00000	91344E-01	0.00000	20451E+00	0.00000	33523É-1,2	¯ o•ōɔɒoō˙	-18429E-12	0.00000
23891E-13	0.00000	21188E+00	0.00000	913448-01	0.00000	20451E+00	0.00000	.29630Ē-1Z	0.00000_	[-1535]4-12	_0*000000
179518-13	0.00000	35416E-02	ò.00000	.105156+00	0.00000	.40730E-01	0.00000	.49238E-12	0.00000	-13272c-12	0.00000
-46893E-L3	0.00000	.35416E-0Z	0.00000	•10515E+0Ó	0.00000	-40730E-01	0.00000	37104E-12	` 0.00000 <u>.</u>	83274E-13	0.000000
~.37639E-13	0.00000	18683E+00	0.00000	27984E-01	0.00000	.144201+00	0.00000	19011E-12	0.00000	12482E-12	
-215906-13	0.00000	.18n83E+00	_0.00000°	27984E-01	0.00000	.14420E+00	0.00000	.34199E-12	0.00000	.14379E-12	0.00000
.617958-13	0.00000	18197E-12	0.00000	21320E-01	0.00000	13042E-12_	0.00000	.64494E-14	_ 0 <u>00</u> 00 <u>0</u>	• 23 <u>544</u> 6 <u>-13</u>	0.00000
_ •20362E-13	0.00000	.17285L-12	0.00000	21320E-01	0.00000	•					
±.24576E-13	u.00000	<u>15583E12</u>	_0.00000	21320E-01"	0.00000	•					
47280E-13	0.00000	.17095E-12	_0.00000	213205-01	<u>0</u> • 00 0 0 0	26960E-12	0.00000_	- <u>3</u> 2893E-14	0.00000	17780E-13	0.00000
20819E-13	0.00000	-14603E+00	0.00000	27984E-01	0.00000	14420E+00	0.00000	.73436E-13	0.00000	•15e38E-13	0.00000
E-24077E-13	9.00009	18083E+00	_0*00000	<u>279</u> 84E-01"	0.00000	144208+00	0.00000	-,46406E-13	0.00000	-17871E-13	<u>0.0000</u> 0
319675-13	0.00000	"-35416E-02	0.00000	-1051>E+00	0.00000	40730L-01	0.00000	86103E-13	0.0000	-34587E-13	0.00000
<u></u> 36232E-13	0.00000	35416E-02	0.0000	.105156+00	0.00000	40730£-01	_0.00000_	362236-13	_0.00000_	42971t- <u>[</u> 4	.0.00000
12455E-13	0.00000	211882+00	0.00000	91344E-01	0.00000	-20451E+00	0.00000		0.00000	.75978±-13	0.00000
622388-14	0.00000	.21188E+00	_0.00000_	91344E-01	. 0. 00 u u o	.204516+00_	_0.00000_	266228-13	0.00000	72573E-14	<u>_0.05005_</u>
7-40661E-13	0.00000	-14527E-01		35496E-01	` îa.ooooo "	30667L+00	0.00000	.73733£-13	0.00000	"37257±-14	0.00000
.493645-13	0.00000	19527L-01	0.00000	.35496E-01	0.00000	30667E+00	0.00000	.68113E-13	0.03600	.419446-13	0.60000
	4 *	- I						ė			

-	NATURAL	FREGUENCY=	-131957E+04

TX REAL	TX	KEAL,	TY .	TZ	TZ 1 HAG	RX REAL	. RX IMAG	RY REAL	IHAS	ZZ"REAL_	RZ THAG
.20846E-12	0.00000	.71112E-14	0.00000	223b1E+0J	0.00000	.85118E-13	0.00000	15841E-12	0.00000	39487t-12	0.00000
17350E-12	0.00000	.471898-14	0.00000	.,223a1E+00 ⁻	0.00000	16510E-13	0.00000	24021E-12	0.00000	.34742E-12	_ 0*0000n_
54261E-13	0.00000	.22861E~14	0.00000	223a1E+00	0.00000	.60814E-13	0.00000	19307E-12	0.0000	.23906E-1Z	0.00000
-659298-13	0.00000	18070L-13	0.00000	. 00+419ESS•	0.00000	11469b-12	0.00000	11980E-12	0.00000	27653E-12	_0.00000
.17633E-12	0.00000	40693E-13	á.00000	223616+00	0.00000	20574E-13	0.00000	.55575E-12_	0.00000	.695146-13	0.00000
-19607E-12	0.00000	.57306E-14	0.00000	•22361E+0V	0.00000	.70976E-13	0.00000	•52132E-12		-,45648L-13	0.00000
-144156-12	0.00000	-1592706-14	0.00000	22361L+00	0.00000	18520±-12	0.00000	.187168-12.	[0.00000]		_0.00000_
-13456E-12	0.00000	.11847t-13	0.00000	22361E+00	0.00000	.17876t-12	0.00000	15218F-15	0.00000	.20150c-12	0.00000
.19630E-12	0.00000	.205168-13		22361E+00	_0.000000		0 00000	29147E-12	. 0. 00000	.405026-13	0.00000
-15248E-12	0.00000	3836ht-13	0.00000	-22361E+00	0.00000						
-116195-12	0.00000					• • .					
-154585-12	0.00000	.11893E-14	_o•o:oo:i_	• 5530 iĘ.• 00 _	_ `n•oooo'o"	14883E-13	_0.00000	29247E-12	0.000000	31190E-13	0.03000
.55358E-13	0.00000			22361E+00							
				.22361E.00							
-12638E-12				22361E+00							
¥12935E-12				. 22361E+00							
-•68634E-13	0.00000	•		223618+00_							
244588-13	0.00000			.22361E+30						· ·	
-16697E-12				00+319F22*-							
-13900E-12	0.00000	29751L-13	0.00000	.22361E+00	0.00000	22079E-12	0.00000	14400E-12	0.00000	29057E-12	` a.ôoooộ

"NATURAL FREQUENCY= " .134445E+04

TX FX TY TY YZ TZ RX RX RY KY RZ RZ  REAL IMAG REAL IMAG REAL IMAG REAL IMAG	
\$91686-01 J.0000058622E-13 0.0000096111E-12 0.0000010570E-11 0.00000 .50326E-12 0.0000016347E-01 0.00000	
.59168E-01 0.00J0049069E-13 0.00000 .93413E-12 0.00000 .17039E-11 0.00000 .48591E-12 0.0000016347E-01 0.00000	
20781E-01 0.00000 -57004E-13 0.00000 -64668E-12 0.00000 -17242E-11 0.00000 -52018E-12 0.00000 -31639E+00 0.00000	
.20781E-01 0.00000 .32993E-13 0.00000 .66676E-12 0.0000017849E-11 0.00000 -41841E-12 0.0000031699E+00 0.00000	•
33738E-02 0.00000 30117E-13 0.00000 -22764E-11 0.00000 .74398E-12 0.00000 -13816E-11 0.00000 -16789E+00 0.00000	
.33738E-02 0.00000 .48013E-13 0.0000022284E-11 0.0000076441E-12 0.0000013236E-11 0.0000016789E+00 0.00000	-
-13621E-01 0.0000038407E-13 0.00000 .83788E-12 0.0000020440E-11 0.0000046314E-12 0.0000033860E+00 0.00000	-
13621E-UI 0.0000021516E-13 0.0000002800E-12 0.00000 .20465E-11 0.0000043395E-12 0.0000033860E+00 0.00000	-
56464E-G1 0.0000035323E-13 0.0000015427E-11 0.00000 .25352E-13 0.00000 .60292E-12 0.0000056464E-01 0.00000	-
56464E01 0.00000 .19158E-13 0.00000 .14545E-11 0.00000	
.56464E-01 0.0000041426E-13 0.0000014931E-11 0.00000	
.56464E-01 0.00000 .20124E-13 0.00000 .15415E-11 0.00000 .41394E-13 0.00000 .57286E-12 0.00000 -56464E-01 0.00000	-
13621E-DI 0.00000 .30498E-13 0.00000 .87682E-12 0.00000 .19670E-11 0.0000024713E-12 0.0000033860E+00 0.00000 _	
13621E-01 0.0000031173E-130.0000087590E-12 0.0000019960E-11 0.0000016937E-120.0000033860E-00 0.00000	•
33738E-02 0.00000 .21569E-13 0.00000 .21803E-11 0.0000084759E-12 0.0000092854E-12 0.0000016789E+00 0.00000	-
33738E-02 0.0000016878E-13 0.0000021826E-11 0.00000 -81236E-12 0.0000081455E-12 0.0000016789E+00 0.00000	
=-20781E-01 0.0000017778E-13 _0.0000062725E-12 0.0000016857E-11 0.0000020644E-12 0.0000031699E+00 0.00000	•
20751E-01 0.0000051649E-13 0.00000 .65224E-12 0.00000 .16208E-11 0.00000 .20759E-12 0.0000031699E+00 0.00000	•
59168E-01 0.0000025268E-13 0.0000091746E-12 0.00000 .16851E-11 0.00000 .39644E-12 0.0000016347E-01 0.00000	
59168E-01 0.00000 -30301E-13 0.00000 .87955E-12 0.0000015941E-11 0.00000 .29842E-12 0.0000016347E-01 0.00000	•

NATURAL FREQUENCY= .134626E+04 TZ ŔХ IMAG. KEAL -.64676E-01 0.00000 .689146-14 0.00000 .14359E-12 0.00000 .22854L-12 0.00000 -.49887E-12 0.00000 .22759E-01 0.00000 -64676E-01 0.00000 .54009E-14 0.00000 -.17481E-12 0.00000 -.46886E-12 0.00000 -.50742E-12 0.00000 .22759E-01 0.00000 -.11927E-01 0.00000 -.36675E-13 0.00000 .96688E-13 0.00000 -.23955E-12 0.00000 -.33305E-12 0.00000 333191E+00 0.00000 --11927E-01 0.00000 -33494L-13 0.00000 --.50361E-13 0.00000 .34732E-12 0.00000 -.41567E-12 0.00000 .33191E+00 0.00000 -.27648E-U2 0.00000 -37099E-13 0.00000 -.42843E-12 0.00000 -.1908ZE-12 0.00000 .10563E-11 0.00000 .14144E+00 0.00000 -- 27646E-02 0.00000 -- 44622C-13 0.00000 -37440E-12 0.00000 -47348E-13 0-00000 .10735E-11 U.00000 .14148E+00 0.00000 .19663E-01 0.00000 -22255c-13 0.00000 -.17211E-12 0.00000 -24762E-12 __0.00000 __.33606c+00 __0.00000 ___ .30755E-12 0.00000 -19663E-01 0.00000 --30443C-13 0.00000 -14373C-12 0.00000 --33805E-12 0.00000 -31703E-12 0.00000 -33608E+00 0.00000 259705E-01 0.00300 -.85675E-14 0.00000 .29767E-12 0.00000 -.25017E-13 0.00000 -.45743E-12 0.00000 -.36718E-11 0.00000 -59705E-01 0.00000 -.86157E-15 0.00000 -.22675E-12 0.00000 .59705E-01 0.00000 -.98212L-14 0.00000 .24490E-12 0.00000 -59705E-01 0.00000 -35425E-14 0.00000 -310199E-12 0.00000 -41121E-13 0.00000 -50521E-12 0.00000 -3988E-11 0.00000 .19663E-01 0.00000 -34108-13 0.00000 -11643E-12 0.00000 -34458E-12 0.00000 -82122E-13 0.00000 -336062.00 0.00000 -19663E-01 0.00000 .70533E-13 0.00000 .15661E-12 0.00000 .41018E-12 0.00000 -85006E-13 0.00000 -33606E-00 0.00000 -276486-02 0.00000 --333586-13 0.00000 --454176-12 0.00000 -105626-12 0.00000 -313706-12 0.00000 -1141486-00 0.00000 -27648E-02 0.00000 -.89965E-14 0.00000 -43726E-12 0.00000 -.82516E-13 0.00000 .38454E-12 0.00000 -.14148E+00 0.00000 -.11927E-01 0.00000 -.87980L-13 0.00000 .90401E-13 0.00000 .38537E-12 0.00000 .8862ZE-13 0.00000 -.33191z-60 0.00000 -11927E-01 0.00000 -.41364L-13 0.00000 -.130b0E-12 0.00000 -.36792L-12 0.00000 -97279E-13 0.00000 -.33191c+00 0.00000 .64676E-01 0.00000 .24710L-13 0.00000 .21120C-12 0.00000 -.43031m-12 0.00000 -.27884E-12 0.00000 -.22759m-01 0.00000 -64676E-01 0.00000 1.51984E-13 0.00000 -16778E-12 0.00000 .27465E-12 0.00000 -.22961E-12 0.00000 -.22759E-01 0.00000

TX

ŦΧ

	NATURA	L FKEOJEN	CY= .130729	E+04			
	- TY	TY IHAG	" YZ	TZ I mag	KX Real	RX I hag	
000	232746-13	0.00000	.29947E-12	0.00000	52966E-13	0.00000	• 9
000	.38232E-13	0.00000	28382E-12	0.00000	1d100E-14	Ô.00000	
					56793E-13		
000	35671L-14	0.00000	- <u>.</u> 28316E-12	0.00000	223048-13	0.00000	• 3
					.65203E-13		
					.46282E-13		

REAL IMAG .91390E-01 0.00000 _ .21998E+00 0.00000 -.10203E+00 0.000 91390E-01 0.00000 -.2199dE+00 0.00000 -10203E+00 0.00U .12827E+00 0.00000 -.131472+00 0.00000 .28667E-01 0.000 .12827E+00 0.00000 _ .13147E+00 [0.00000] --28667E-01 0.000 .29157E+00 0.00000 -.74670E-01 0.00000 .84533E-01 0.00U .29157E+00 0.00000 .74670E-01 0.00000 --84533E-01 0.00000 .19964E-12 0.00000 -.22354E-13 0.00000 -.11612E+00 0.00000 .12515E+00 0.00000 -18754E-13 0.00000 _13365E+00 0-0000C .43560E-13 0.00000 -.11612E+00 0.00000 -.12515E+00 0.00000 .11690E-13 0.00000 -.25490E-12 0.00000 -.13355E+00 0.00000 --93315E-01 0.00000 .69812E-14 0.00000 .16439E-12 0.00000 --89667E-13 0.00000 .18511E-11 0.00000 --93315E-01 0.00000 -93315E-01 0.00000 _-.39837E-13 0.00000 -.15084E-12 0.00000 -93315E-01 0.00000 -98526E-14 0.00000 -.15769E-13 0.00000 -.93315E-01 0.00000 --39674E-13 0.00000 -.30448E-13 0.00000 .63569E-13 0.00000 .16898E-11 0.00000 .93315E-01 0.00000 --13385E+00 0.00000 --40310E-13 0.00000 .32164E-14 0.00000 --54966E-13 0.00000 .11612E+00 0.00000 .12515E-00 0.00000 -13365E+00 0.00000 3.32245L-13 0.00000 .67390E-13 0.00000 .1287ZE-12 0.00000 .1161ZE+00 0.00000 -.12515E+00 0.00000 -34533E-01 0.00000 -.22236E-13 0.00000 -.16035E-12 0.00000 -.14402E-12 0.00000 .29157E+00 0.00000 -.74670E-01 0.00000 -84533E-01 0.00000 34769E-13 0.00000 19422E-12 0.00000 10421E-12 0.00000 29157E700 0.00000 74670E-01 0.000000 -28667E-01 0-00000 --54870E-13 0.00000 --28661E-12, 0.00000 --31960E-13 0.00000 --12827E+00 0.00000 --13147E+00 0.00000 -28667E-01 0.00000 .51730E-13 0.00000 .10354E-12 0.00000 .77610E-13 0.00000 -12827E+00 0.00000 -13147E+00 0.00000 -.10203E+00 0.00000 -.23518E-13 0.00000 -.23495E-12 0.00000 -.31531E-13 0.00000 -.91390E-01 0.00000 -.21934E+00 0.00000

# NATURAL FREQUENCY= .137419E+04

TX REAL	TX TY TY TZ TZ TAGE THAG REAL THAG	RX RX RY RY RZ RZ REAL IMAG REAL IMAG REAL IMAG
11549C-13	0.0000012058L-13 0.0000011069E+00 0.00000	20222E+00 0.00000 .21155E-12 0.00000 .28139E-13 0.00000
177656-13	0.00000227185-13 0.00000 .11069E+00 0.00000	.20222E+00 0.0000019054E-12 0.0000011619E-13 0.00000
<b></b> 20109E-13	0.0000023037E-12 0.0000041866E-01 0.00000	.21444E+00 0.0000051315E-12 0.0000043171E-14 0.00000
362772-13	3 _0.00000236386-12 0.00000	21444£+00 "0.00000 [.47170Ê-12 0.00000 .35026£-13 0.00000]
105786-13	0.00000 .29733E-13 0.00000 .24688E+00 0.00000	37057E-02 0.00000 .54418E-12 0.00000 .12070E-12 0.00000
-186569E-14	0.00000 [423986-14 0.00000 [246886+00 ]0.00000	.37057E-02 0.0000052527E-12 0.0000011373E-13 0.00000
14473E-13	0.00000 .22536E-12 0.0000047708E-01 0.00000	24271E+00 0.0000032276E-12 0.00000 :82107E-13 0.00000
•21941E-13	0.0000020527E-12 0.00000 .47768E-01 0.00000	.24271E+00 0.00000 .40968E-12 0.00000 .49763E-13 0.00000
-15209E~13	0.00000 T.23464E-13 0.00000 = 15714E+00 0.00000	.15714E+00 ]0.00000 88453E-14 0.00000 .40897E-13 0.00000
42153E-14	0.00000123866-13 0.00000:157146+00 0.00000	
23396L-13	0.0000021864E-14 0.00000 .15714E+00 0.00000	•
261778-13	1 0.00000	15714E+00 0.0000020380E-14 0.00000 1.16024E-13 0.00000
_12278E-13	3 0.0000024905E-12 0.00000 .47768E-01 0.00000	24271E+00 0.00000 [.27347E-12 0.00000 1.14792E-12 0.00000]
189326-13	3 0.00000 .20730E-12 0.0000047764E-01 0.00000	.24271E+00 0.0000031447E-12 0.00000 .17577E-12 0.00000
- <u>-1</u> 8544E-13	3 0.00000 [92923E-16 0.0000024608E+00 00000	37057E-02 0.000004878dE-12 0.00000 .50765E-13 0.00000
J11235E-13	3 0.0000085037E-14 0.00000 .2468dE+00 0.00000	.37057L-02 0.00000 .49569E-12 0.00000 .19434E-13 0.00000
226798-13	3 0.00000 .278678-12 0.00000418668-01 0.00000	.21444E+00 0.00000 .45948E-12 0.00000 .50215E-13 0.00000
.27515E-13	3 0.00000262308-12 0.00000418668-01 0.00000	21444L+00 0.0000037956E-12 0.0000012978E-12 0.00000
•16292E-13	0.0000018974L-11 0.00000 .11069E+00 0.00000	20222E+00 0.0000020577E-12 0.00000 -21259E-13 0.00000
642631-14	• 0.00000 -18115E-14 0.000001106/E+00 0.00000	.20222L+00 0.00000 .16045E-12 0.0000020056L-13 0.00993

NATHDÁÍ	てっへいけ MCY虫	. 1387866+04

TY TY TY TY TY TY TY TY TY TY TY TY TY T	-	RX RY RY RZ RZ IMAG REAL IMAG REAL IMAG
154276-13 0.00000 57698E-13 0.00000 77477E-14 0.	00000 -7>709E-13	0.0000099105E-01 0.0000014953E-13 0.00000
-61354F-13 0-0000021139E-13 0.00000 -47316E-13 0.	00000 17198E-12	0.00000 .99105E-01 0.00000 .67633E-13 0.00000
7352406-13 0.00000 7 .83486E-13 0.0000080509E-13 0.	.000009J271E-13 _	0.00000 -25946E+00, 0.00000 -14382E-12 0.00000
.47276E-13 0.0000085041E-13 0.0000039881E-14 0.	00000114661-12	0.0000025946E+00 0.00000 .65679E-13 0.00000
-32196E-15 0.0000015822E-13 0.0000 .90931E-13 0.	. 00000 . 27804E-13	0.00000 32071E+00 0.00000 20835E-12 0.00000
.65054E-13 0.00000 -19770F-13 0.00000 .82381E-13 0.	.00000 414620-14	0.00000 .32071E+00 0.0000021065E-12 0.00000
65454E-13 0.0000072091E-13 7.0000078866E-13 0.	.00000 30064E-13	0.00000 -25946E+00 0.0000074504E-13 0.00900
35093E-13 0.00000 .76834E-13 0.0000011261E-13 0.	.00000 .94807E-13	0.0000025946E+00 0.0000028228E-13 0.00000
24502L-13 0.00000 17909L-14 0.0000047035E-13 0.	.0000081023E-14	0.0000049105E-01 0.0000018242E-14 0.00000
86911E-14 0.0000039229E-13 0.00000 88497E-13 0.	• ឬី០ចំ០០ ្ព័	
20094E-13 0.00000 .56958E-14 0.0000052492E-13 0.	• 00000 ;	
14 N		
-14663E-13 0.00000 -122543E-15 0.00000 [	.0000050977E-13	0.00000 -99105E-01 0.0000027304E-14 0.00000
.43307E-15 0.00000 .45567E-14 0.00000 .99211E-13 0.	.00060 .41006E-13	0.00000 .25946E+00 0.00000 .16151E-13 0.00000
	.00000 .41006E-13 .0000076276E-13	0.0000025946E+00 0.0000022896E-13 0.00000
.43307E-15 0.00000 .45567E-14 0.00000 .99211E-13 0.	.00000 .41006E-13 .0000076276E-13	0.0000025946£+00 0.0000016151£-13 0.00000 0.0000025946£+00 0.0000022896Ē-13 0.00000 0.0000032071£+00 0.0000055259£-13 0.00005
43307E-15 0.00000 .45567E-14 0.00000 .99211E-13 0. [.20830E-13 0.0000015752L-13 0.0000023843E-13 0. 34519E-13 0.0000011384E-13 0.0000060654E-13 0. [.12892E-13 0.0000062547E-15 0.0000097436E-13 0.	.00000 .41006E-13 .0000076276E-13 .0000025048E-13 .00000 .60085E-13	0.0000025946£+00 0.0000016151£-13 0.00000 0.0000025946£+00 0.0000022896£-13 0.00000 0.0000032071£+00 0.0000055259£-13 0.00000 0.00000 .32071£+00 0.0000068019£-13 0.00000
.43307E-L> 0.00000 .45567E-14 0.00000 .99211E-L3 0.20830E-L3 0.0000015752E-13 0.0000023843E-L3 0.34519E-L3 0.0000011384E-L3 0.000006054E-L3 0.12892E-13 0.0000062547E-L5 0.0000097436E-L3 0.22934E-L3 0.0000060395E-14 0.0000057176E-13 0	.00000 .41006E-13 .0000076276E-13 .0000025049E-13 .00000 .60085E-13	0.0000025946£+00 0.0000016151£-13 0.00000  0.0000025946£+00 0.0000022896£-13 0.00000  0.0000032071£+00 0.0000055259£-13 0.00000  0.00000 .32071£+00 0.0000068019£-13 0.000000  0.00000 .25946£+00 0.0000063256£-13 0.00000
43307E-15 0.00000 .45567E-14 0.00000 .99211E-13 0. [.20830E-13 0.0000015752L-13 0.0000023843E-13 0. 34519E-13 0.0000011384E-13 0.0000060654E-13 0. [.12892E-13 0.0000062547E-15 0.0000097436E-13 0.	.00000 .41006E-13 .0000076276E-13 .0000025049E-13 .00000 .60085E-13 .0000036749E-13	0.0000025946£+00 0.0000016151£-13 0.00000  0.0000025946£+00 0.0000022896£-13 0.00000  0.0000032071£+00 0.0000055259£-13 0.00000  0.00000 .32071£+00 0.0000068019£-13 0.00000  0.00000 .25946£+00 0.00000 .63256£-13 0.00000  0.0000025946£+00 0.00000 .1381£-12 0.00000
.43307E-L> 0.00000 .45567E-14 0.00000 .99211E-L3 0.20830E-L3 0.0000015752E-13 0.0000023843E-L3 0.34519E-L3 0.0000011384E-L3 0.000006054E-L3 0.12892E-13 0.0000062547E-L5 0.0000097436E-L3 0.22934E-L3 0.0000060395E-14 0.0000057176E-13 0	.00000 .41006E-13 .0000076276E-13 .0000025048E-13 .00000 .60085E-13 .0000036749E-13 .00000 .32673E-13	0.0000025946£+00 0.0000016151£-13 0.00000  0.0000025946£+00 0.0000022896Ē-13 0.00000  0.0000032071Ē+00 0.0000055259Ē-13 0.00000  0.00000 .32071Ē+00 0.0000068019Ē-13 0.00000  0.00000 .25946Ē+00 0.00000 .63256Ē-13 0.00000  0.0000025946Ē+00 0.00000 .11381Ē-12 0.00000  0.0000049105Ē-01 0.00000 .10261Ē-13 0.00000

--11450£+0J 0.00060

-54229E-01 0.00000

.54223E-01 0.00300 -.23792E-13 0.00000

11424=+00 0.00000

" NATURAL FREQUENCY= - TX REAL TZ КΧ 7.2 RΚ REAL REAL IHAG REAL IMAG REAL -.54223E-01 0.00000 .413586-13 0.00G00 .49305E-13 0.00000 -.92407L-13 0.00000 .25746E-12 0.00000 .66226E-01 0.00000 -,54228E-01 0.00000 .29814L-13 0.00000 -.11494E-14 0.00000 .24054E-13 0.00000 .23639E-12 0.00000 .66226E-01 0.00000 .11450E+00 0.00000 -.21983E-13 0.00000 .32542E-13 0.00000 .10027E-12 0.00000 -.27579E-12 0.00000 .13424E+00 0.00000 .11450£+00 0.00000 ~.83051E-14 0.00000 -.68557E-14 0.00000 -.50429E-13 0.00000 -.3038E-12 0.00000 <u>.13424E</u>+00 0.00000 12503k-01 0.00000 285906-13 0.00000 7851kE-13 0.00000 -.62387k-13 0.00000 -.79326E-13 0.00000 -.44262E-00 0.00000 .12503E-01 0.00000 -.61158E-13 0.00000 -.12238E-12 0.00000 -.23005E-13 0.00000 -.20693E-12 0.00000 -.44262E+00 0.00000 -11450E+00 0.00000 .17756E-13 0.00000 .67424E-14 0.00000 -17963E-13 0.00000 .40353E-12 0.00000 .7419E-01 0.00000 -.11450E+00 0.00000 .23250E-13 0.00000 .77337E-14 0.00000 .81358E-13 0.00000 .41983E-12 0.00000 .74119E-01 0.00000 [.47721E-01 0.00000 -.31035E-13 0.00000 ".46817E-13 0.00000 -.400526-13 0.00000 -.53477E-13 0.00000 .47721E-01 0.00000 -47721E-01 0.00000 .35300E-13 0.00000 -.23261E-13 0.00000 --47721E-01 0.00000 -.33557E-13 0.00000 -.24577E-13 0.00000 -47721E-01 0.00000 .32902E-13 0.00000 .13792E-13 0.00000 .21213E-13 0.00000 .10130E-13 0.00000 .47721E-01 0.00000 -.11450E+00 0.00000 -.61567E~14 0.00000 .1997[6-13 0.00000 -.32212E-13 0.00000 -.39753E-12 0.00000 _.74119E-01 0.00000 -11450E+00 0.00000 -.46352E-13 0.00000 -.38496E-13 0.00000 -.58982E-13 0.00000 -.30586E-12 0.00000 .74119E-01 0.00000 -.12503E-01 0.00000 -.1107ZE-13 0.00000 1.1085ZE-13 0.00000 -.63664E-13 0.00000 2.2780E-12 0.00000 -.4426ZE+00 0.00000 -.12503E-01 0.00000 -.65148E-14 0.00000 .30618E-13 0.00000 .73156E-13 0.00000 .17152E-12 0.00000 -.44262E+00 0.00000

-.11450E+00 0.00000 -.14828E-13 0.00000 -.27713E-13 0.00000 .54655E-13 0.00000 .24870E-12 0.00000 .13424E+00 0.00000

.25055E-13 0.00000 ~.40276E-14 0.00000 -.107d3E-13 0.00000

.23850E-12 0.00000

.341601-13 0.00000 -./>3436-13 0.00000 -.30344E-12 0.00000 -.66220E-01 0.00900

.37466c-13 0.60000 -.24940E-13 0.00000 -.33049c-14 0.00000 -.34400E-12 0.00000 .6022ac-01 0.00000

.139958E+04

### NATURAL FREQUENCY= .141/62E+04

.11948E-13 0.0000071365E-01 0.0000022500E-01 0.0000030058E+00 0.00000353363E-14 0.0000027004E-13 0.0000027004E-13 0.0000027004E-13 0.00000
.81535E-14 0.00000 .71365L-01 0.0000022500E-01 0.0000030058E+00 0.0000020562E-13 0.0000027004E-13 0.00000
.28111E-14 0.0000015195E.00 0.00000 .3215EE-01 0.00000 .19759E.00 0.00000 .72647E-13 0.0000040179E-13 0.00000
.29379E-13 0.00000 1.15195E-00 0.0000019759E+00 0.0000057013E-13 0.0000028200E-13 0.0000
.236456-13 0.00000 .14746E+00 0.0000055678E-04 0.0000021796E+00 0.0000019761E-L2 0.00000782796-13 0.00000
-35649E-14 0.0000014946E+00 0.0000055878E-01 0.0000021796E+00 0.00000 1.14400E-12 0.0000015120E-13 0.00000
.31088E-13 0.00000 .59539E-01 0.00000 .36042E-01 0.0000013972E-01 0.00000 .15751E-12 0.000076075E-13 0.00000
\$214876-13 0.00000595396-01 0.00000 .360426-01 0.00000139726-01 0.00000282826-12 0.00000913346-13 0.00000
,46782E-13 0.0000013812E+00 0.0000046691E-01 0.0000046691E-01 0.0000018646E-13 0.0000010389E-13 0.00000
.67303E-14 0.00000 .13612E+00 0.00000 .46691E-01 0.00000
54662E-13 0.0000013812E+00 0.0000046691E-01 0.00000
.73950E-13 0.00000 .13812E+00 0.0000046691E-01 0.0000046691E-01 0.0000015590E-12 0.0000040927E-13 0.00000
.12055E-12 0.00000 .59539E-01 0.0000036042E-01 0.0000013472E-01 0.0000061631E-13 0.0000011077E-12 0.00000
.77203E-13 0.0000059539E-01 0.0000036042Ê-01 0.0000013972E-01 0.0000046142E-12 0.00000 .22864E-13 0.00000
38055E-13 0.00000 .14946E+00 0.0000055878E-01 0.0000021796E+00 0.0000015273E-12 0.00000 .17897E-12 0.00000
,30990E-13 0.00000 [14946E+00] 0.00000 [.55878E-01] 0.00000 [21796E+00 0.00000 ] .2500ZE-12 0.00000 [26274E-12 0.00000
.78884E-13 G.0000015195E+00 0.0000032158E-01 0.00000 .19759E+00 0.0000037584E-12 _0.0000072977E-13 0.00000
.84040E-13 0.00000 .15195E+00 0.0000032158E-01 0.00000 .19759E+00 0.0000094313E-13 0.00000 .12407E-12 0.00000
.77366E-L3 0.0000071365E-01 0.00000 .22500E-01 _0.0000030058E+00 0.0000022380E-L2 _0.0000090001E-13 _0.00000
.44770E-13 0.00000 .71365E-01 0.00000 .22509E-01 0.0000030053E+00 0.0000047448E-13 0.0000011042E-12 0.00000

NATURAL FREGUENCY=	.141040É+U4			

TX REAL	TX	. IY KEAL	TY INAG	TZ REAL	11 24 D	KX KEAL	RX I HAG	RY Real	IHAG	REAL	RZ ÎHAĞ
-60583E-01	0.00000	32878E-13	0.00000	.35018E-13	0.00000	12970E-12	0.00000	57,790E-11	0.000000	19797E=	01 0.00003
60583E-01	0.00000	-44348E-13	0.00000	[=.19590E=i3]	`` <b>0.</b> 00000`	~.55043E-13	0.00000	58140E-11	_000000_	- <u>.19</u> 7978-	01 0.00000
-6101GE-02	0.00000	64048E-13	0.00000	.15601E-13	0.00000	.73043E-13	0.00000	-63812E-11	0.00000_	344602+	00 0.00000
.61010E-02	0.00000	+55861E-14	0.00003	278d2E-14	0.00000	.799396-14	0.00000	.64237E-11	_ 0.00000	34460E+	00 0.00000
143296+00	0.00000	.25623t-13	0.00000	1285 /E-13	0.00000	39663E-13	0*00000	.33226E-11	_0.000000	_ •35 <u>6</u> 2ífé <del>_</del>	or <u>o</u> •00007.
143298+00	0.00000	678026-13	0.00000	42303E-13_	0.00000	7.11745E-12	0.00000	33301E-11	_0.00700]	32931E-	010.05000
-25451E-01	0.00000	.34327E-13	0.00000	134218-13	0.00000	.41669m-13,	0.00000	93782E-11	_0.00000 <u>_</u>	.32800E+	00 <u>0.0700</u> 0
-25451E-01	0.00000	.36967E-13	0.00000	.56709E-13	0.00000	.23252E-13	0.00000	93319E-11	ด•ู oʻbon oʻʻ	_35g00 <u>E</u> +	000.0000
51157E-01	,0.00000	82846E-14	,0.00000	.25,762E-13	0.00000	.19685E-15	0.00000	36852E-12	_0.00000	57888E-	11 0.00000
.51157E-ul	0.00000	•37930E-13	0.00000	15200E-13	0.00000						
-51157E-01	0.00000	82466E-14	0.00000	.19926E-13	0.00000				,		
51157E-01	0.90000	-40536É-13	0.00000	51125E-L3_	0.00000	19126E-13	0.00000	33[63E15		11086E-	11 0.00000
-25451E-01	0.00000	47507L-13_	ó.0000a	51354E-13	0.00000	.20313E-13	0.00000	.84172E-11	_0.00000_	32800£÷	00 <u>00</u> 0 <u>0</u> 0000
.25451E-01	0.00000	46365E-13	0.00000	-14765E-13	0.00000	.51400E-14	0.00000	.836161-11	0.00000	32800E+	00 0.00000
14329E+00	0.00000	.697738-13	0.00000	.20492E-13	0.00000	91182E-13	0.00000	31992E-11	0.00000	32931E-	0.00000
14329E+00	0.00000	623276-13	0.0000	.19567E-13	0.00000	15332E-12	0.00000	32478È-11	0.00000	32931E-	01 0.00000
-610108-02				51182E-14				568128-11		-	
-61010E-02	0.00000	•13264E-12"	0.00000	11666E-13	_0.00000	`•12445E-12	0.00000	56484E-11	0.00000	-34460E+	00 0.00000
-60583E-01	0.00000	8745dE-13	0.00000	.106675-13	0.00000	94788b-13	0.00000	.525298-11	0.00000	.197976-	01 0.00000
.60583E-01	0.00600	18411E-13	0.00000	. 1906ZE-13	ò.00000	12524E-12	0.00000	.53464E-11	0.00000	•19797E-	01 0.00000

5		MUNICIPAL SALL MARKET SHAPPING	
		5	
	-	=	
~ × .			•

-		NA TURA	L FREQUEN	ICY= .142730	Ŀ+04						
TX REAL	XX IMAG	TY REAL	TY THAG	T Z Real	TZ I HAG	RX Real	RX THAG	RY REAL ,	RY	RZ XEAL	RŽ IMAG
.83457E-01	J.00000	77332E-12	0.00000	.76063E-13	0.00000	.16731E-12	0.00000	.1373d£+00	0.00000	.12548Ê+000	0.00000
-83457E-01	0.00000	82 ou 8E -12	0.00000		0.00000	]206848-13	0.00000	13738E+00	0.00000	12548E+00	0.00000
.859016-01	0.00000	-11277E-11	0.00000	44672E-14	0.00000	14529L-12					
85701E-01				65250L-13						. 14557£+00	
.14424E-01	J.00000 j	.35994E-12	0.60000	12496E-13_	0.00000	.14760E-12	0.00000	50298E-01	0.50000	26700E+00_	0.00000
14424E-01	0.00000	42987E-12	0.00000		•	73546E-13					
89379E-01	0.00000	123421-11	0.00000	.62886£-13	0.00000	45268E-13					
				127416-12							
~72511E-01	0.00000	.49835E-13	0.00000	~~.57496E-13	0.00000		.0.0000.0	~.14623E+00~	0.00000	10736E-12	0.00000
72511E-01	0.00000	360808-13	0.00000	• 48154E-13	0.00000						
				47983E-13		-					
				99814E-13							
~_89377E-01	0.00090	.11892E-11	0.00000	.50919E-13	0.00000	.786965-13	_ 0.00000_	22771E+00_		85935E-01	0.00000
				1,0735E-12							
				30413E-13							
14424E-01	0.00000	42214E-12	~0.00000	18828E=13	0.00000						
.85901E-01	0.00000			23393E-13						·145576+00_	
85901E-01	0.00000			36006E-13							
83457E-01	0.00000	.81704E-12	0.00000	.56739E-13	.0.00000	68708E-13	0.0000			-,12548±+00	
.83457[-01	0.00000	.800 POE -12	0.00000	29756E-13	0.00000	.77289E-13	0.00000	•1373dE+00	0.00000	.125488+00	0.09009

HATURAL	FREQUENCY=	.137880E+U4
---------	------------	-------------

TX TX TY TY TY TY	TY TZ	TZ IMAG	RX TE	RX"	REAL	RÝ. IHAG	KZ RZ KEAL IMAG
-11154E-13 0.0000025984E-13	3_ 0.04000 <u>8</u> 7209E-1	<u>i</u> 0.00000	11035E12	0.00000	11401E+00	0.00000	-12648E-13 0-00000
81970E-14 0.0000035636E-13							
11058E-13 0.00000 .18478E-12	2 0.00000 12898E-1	ž g.00000, i	250391-13	0.00000"	. 28868E+00	0.00000	.28156E-13 0.00000
61943E-14 0.0000024050E-12	2-0.00000883118-1	4 0.00000	38482E-12	0.00000	28868E+00		22048E-13 0.00000
20905E-13 0.00000 15-15987E-13	3 _0.0000030974E-1	2 0.00000 "	37935E-13	0.00000	32827E+00	0.00000	15235E-13 0.00000
53800E-13 0.0000042822E-13	3 [0.00000]123346-1	2 0,000007	36952E-13	0.00000	.32827E+00	0.00000	56199E-13 0.00000
42878E-13 0.0000016299E-12	2 0.0J000 .42474E-1	4 0.00000	54327c-13	0.00000	+21426E+0U	0.03000	75961c-13 0.03000
19936E-13 0.0000023476E-12	20.0000034113E_1	30.00000_	.37278E-12	0.00000	21426E+00	0.00000	65088E-13 0.00000
70526E-13 0.0000052282E-1	3 0.0000016169E-1	Z0.00000	.19001E-15	0.00000	32718E-12	0.00000	37760E-15 0.00000
.68765E-14 0.00000 .17160L-13	3 0.00000 .666896-1	3 0.00000					
43850E-13 0.0000026918E-13	3 0.00000 .185346-1	2 0.00000					
	3 0.0000018353E-1	2 0.00000	±.14375€=12	0.00000	21634E-12	0.00000	.36943E-14 0.00000
21746E-13 0.00000 .22243F-13	2 0.60000313598-1	3 0.00000	480958-12	0.00000	21426E+00	0,00000	
-44577E-13 0.0000030995E-1	2 0.0000011646E-1	2 3.00000	.55608E-13	0.00000	.21426E+00	0.00000	877636-13 0.00000
20274E-14 0.00000 .62386 <u>E</u> 1;	3 . 0.00000 73042E-1	3 0.00000	10295E-12	0.00000	328276+00	_0.00000g	79843E-13 _ 0.00000 _
86539E-140.0000035953E-1	3 0.00000 .43977E-1	2 0.00000	11772E-12	0.00000	32827E+00	0.00000	79425E-13 0.00000
=-29074E-13 0.0000027583E-1	2 0.0000095876E-1	3_ 0.00000	•56255E-12	0.00000	,28868E+u0	_ 0.00000	.12032E-13 0.00000
	2 0.00000217596-1	2 0.00000	-11u56E-12	0.00000	.288686+00	0.00000	17942E-13_0.00000
126252-13 0.00000174348-1	3 _ 0.0000016245E-1	2, 0.00000	721444-12	0.00000	1,140,16+0,0	_ <b>0.</b> 0000 <u>0</u>	22589E-13 0.00000
.184545-13 0.00000359496-1	3 0.GU00056794E-1	3 0.00000	293906-12	0.00000	11401L+00	<b>0.00000</b>	.52092E-13 [0.30000]

## HATURAL FREQUENCY= .139491E+04

				-						- RZ	" RZ """
TX Real	TX IAAG	TY REAL	TY Imag	TZ` REAL	TZ IHAG	KFAL KX	RX IHAG	RY REAL	RY IHAG	KLAL KLAL	IHAG
43380E-01	0.00000	67321 <del>-13</del>	0.00000	217416-13	0.00000			22638E-12			
43380E-01	0.00000	.170876-13	_0.00000	.19080E-13	3.00000	.10021E-13	0.00000	-		65684E-01	
12138E+Du	0.00000	.464446-13	0.00000	.52860L-13	0.00000	.375696-13	0.00000			62940E-01	
12138E+00	0.00000	.65006E-13	0.00000	10764E-12		23574E-13					
	0.00000	230266-13	0.00000	.229316-13	0.00000	107786-13					
.15829E-01	0.00000	31232E-13	0.00000	645748-13	0.0000	.11634E-13				45321E+00	
-99713E-01	0.00000	65902¢-13	0.00000	33924E-13	0.00000	.50527E-13				- <u>.11667</u> ē+00	
.99713E-ul	0.00000	73507E-13		.230682-13						11607E+00	
3754dE-01	6.00000	.785396-13	0.00000	.40830E-13		41488E-13	0.00000	~11437E-12	0.00000	~59656E-12	0.50000
37548E-01	၀. ၀၇ပဝဝ	,131586-13	0.00000	39471E-13	0.00000			•			
37548E-01	3.00000	.75176E-13	_o.00000		0.00000	•					
±.3754dE-01	0.00000	106708-13	0.00000	.27860E-13	0.00000	.34697E-13	_0.00,000	89384E-13	0.00000	37237E-12	0.00000
.99713E-01	0.00000	2d342E-13	0.00000	:22738E-13	0.00000	.161658-13	∕>0•00000	_ •36130E-12	0.00000	*11001E+00	0.00000
99713E-01	0.00000	671746-13	0.00000	26967E-13	0.00000	39965E-13	" o.oooda		0.00000	11667E+00	0.00000
15829E-01	0.00000		0.00000	92561E-14	_0.00000	28187E-13	0.00000	82972E-13	0.00000	45321E+00	0.00000
.15829E-01	0.0000	123536-13	0.00600	83880E-14	0.00000	.843761-13				45321E+00	
12138E+00	0.00000	.95994E,-13	0.00000	37409E-13	.0.00000	62656E-14	0.00000	25070E-12	0.00000	62940E-01	0.00000
12138E+JJ	0.00000	.708622-14				72990L-13					
433808-01	_0.00000	<u>23563E-13</u>	0.00000	33053E-13		.33 <u>9786-13</u>	_ `0•000 <u>0</u> 0	.10891E-12			. 0.00000
.43350E-01	0.00030	-,47335L-13	0.0000	22280E-13	3.00000	.10426E-12	0.00000	.16505E-12	0.00000	.65684z-01	. 0•0າດວລ

						•					
TX REAL	TX THAĞ	KEAL	TY .	. TZ PEAL	TZ . DANI	RX Real	RX	REAL .	RY	RZ	RZ IHAG
-55416E-01	0.00000	<u>.</u> 68272E-14	0.00000	56825E-14	0.00000	.14698E-12	0.00000	21441E-ÍĪ	0.00000	10970E-01	0.00020
-55416E-01	0.00000	14043E-13	_0.0000n_	22253E-13		.84469c-13_	0.00000	20133 <u>6</u> -1 <u>1</u>	0.00000	10970E-01	0.00000
24061E-01	0.00000	-32404E-13	0.00000	_ :d1769E-14	0.00000	104776-12	0.00000		0.00000	33 +65 <u>E</u> +00	<u> </u>
-24061E-01	0.00000	65344E-13	0.00000	15558E-14	0.00000	3d277b-13	0.00000	.23128E-11		33985E+00	0.00000
<u>=</u> .14223E+00	0.00000	46283E-13	0.00000	l51396-13_	0.00000		0.000000	.11458E-11	0.00000	41965E-01	0.00000
Ę•14223€+00	0.00000	-47271E-14	0.00000		.0.00000	.78448E-13	`0.00000`	11502E-11			0.00000
3490eE-03	0.00000	.55668E-13	0.00000	206708-13	0.00000	52118Ê-13	0.00000	32473E-11	0.00000		
-,347066-03	0.00000	.85721E-14	_0.000ú0	47758E-13	0.00000	.253098-14	0.00000	32924E-11	0.00000	332882+00	
50989E-01	``o•oooo``		0.00000	2950 <u>4</u> E_i}]	0.00000	12/052-13	.0.0000	.25621 <u>E-12</u>		.50989E-01	0.0000
*2099AE-01	0.00000	40765b-13	0.00000	50778E-14	0.00000						•
509898-01	0.00000	. 274691-13	0-00000	47043E-13_		-					
50989E-01	0.00000	37798e-13	ำอ.ไอเวืออว โ	.47603E-13				~21969E-12	0.00000	.50989t-01	0.0000
_34900E-03	0.00000	83040£=14	.0.00000	89884E-13_		12139 <u>E</u> _13_			0.00000	_33283E+00	0.00000
-3470cE-03	0.00000	64190E-13	0.00000	885186-14	0.0000	41d43E~13		Z5747E-11	0.00000	.33288E+00	0.00000
-14223E+QU	0.00000	11533L-12	0.00000	45813E_13	_0.00000	.70039E-13	0.00000_	11934E-11	0.00000	41965E-01	0.00000
-14223E+00				•		. 17324L-12					
240clE-01	3.00300	.3883tE-13	0.00000	19860E-13	0.00000	489191-13	0.00000	18929E-11	0.00000	33985E+00	် ဝိုင်္ကဲ့ဝေပ်
240616-01	0.00000	10468E-12	0.0000	.90915E-15	0.00000	13697E-12	0.00000	18505E-11	0.00000	33785E+00	0.00000
55416E-01		•53900E-13				.12709b-12					
55416E-01	0.00000	2s310E-13	0.00000	"75939E-14"						-	

NATURAL FREQUENCY+

-140861E+U4

-	"NATHDAL"	FREQUENCY=	.14856/E+04
	NATUKAL	PKE QUENCI -	* F40 70 4 F 4 A 4

TX -	IX IHAG	TY	TY	TZ REAL	TZ _IHAG	KX KEAL	RK IHAG	RY	KY	RZ	RZ IHĀG
44913E-13	0.00000	37672L-12	0.00000	12644E+00_	0.00000	198228+00	0.00000	13866E-13	0.00000	.54616c-13	0.00000_
43400E-13	0.00000	~.16968E=Ī3	` oʻ• oʻo o oʻ <u> </u>	.12644E+00	_0.00000	.19822E+00	0.00000	.12746E-13	0.00000	-, 42511E-13	_0.00000
-56862E-13	0.00000	.30215E-12	0.00000	.87486E-01	0.00000	.2,u738E+00	0.00000	91025E-13			<u></u>
						20738±+00					
.30073E-13	ő.00000	24867b-12	0.00000	68664E-01	0.00000	28729E+00					
,206391-13				68664E-01		•28929E+00					
43438E-13	0.00000	57206E-12	(0.00000)	18133E+0a	0.00000	.87407E-01	0.00000	-14284E-12	_a.60000	1313	0*0 <u>0000</u> _
.2808>E-13	0.00000	82554E-13_	_ 0.00,000	18133E+00	_0.00000	87407E-01					
-401116-13	0.00000	.21551E-12	0.00000	.1516JE+00	0.00000	.22278E-12	0.00000	81130E-1		-,21549b-13	_0.00000
-11901E-13	0.00000	19267E-12	_0.00000_	-,15163E+00_	0.00000						
-51432E-13						•					
,49207E-13						18462E-12_					
841518-13						87407E-01					
						-87407E-01					
+13225E-13	0.00000					~28929±+00					
.205446-13						28929E+00					
50979E-13						20738E+00					
254568-13	00,000	.34099E-12	0.00000	87486E-01	0.00000	.20738£+00	0.00000				
952945-13	0.00000	309506-13		12644E+00						-,70816E-13	
283584-13	0.00000	39047E-12	0.00000	.12644E+00	0.00000	1 18226+00	0.00000	.52137L-1	3 _0.00000	.446756-14	0 • 9 ô 9 0 <u>5</u>

1004
E
:
ì
•
٨

		NA TURAL	FREOULHC	Y= .1413748	+04						
. TX Real	TX	TY	TY	. T.L. REAL .	T Z [ HAG	KKAL -	RX I HAG	-		REAL	
•	_	19826-13		.16790E-13	0.00000			•		.13396E+00	
.87931E-01	0.00000 .1	30036-13	0.00000	32495E-14	0.00000			.14421E+00			
.80915E-01		9726E-13	0.00000	10704E-12	0.00000			15646E+00			
.80915E-01				51127E-13				15696E+00			
				65003E-13	0,00000			86590E-01			
-30891E-01				.60681E-13	0.00000	.11529č-12					
-11747E+00	0.00000 .2	1459Ė-13	0.00000	62608E-13		12348E-14					
.11747E+00		ιοβ14 <u>Ε</u> ÷ <u>Ι</u> 4 "		.13075E-13	0.000.00	28859 <u>k</u> -13_	0.00000	,22942E+00	0.000 vo	17544E-01	0.00000
.61450E-01	0.00000 ".	75384E-13	0.00000	.11141E-1J	0.00000	.24205E-13_	0.00000	37343E-12	0.00000	61456E-01_	0.00000
				31956[-13]							
61450E-01	p.00000 .1	3144 <u>3</u> E-13	_0.00000[	_54778E-13	_0.00000						
-61450E-01	ij . 0000in	565 <u>7</u> 6E-13	_0*00ōŏñ_	.5486 JE-11	0.00000	44132E- <u>13</u>	_0 <u>•000</u> 000_	<u>.</u> 39035E-12	0.00000	61456E-01	0.00000
.11747E+00	0.00000	135585-12	0.00000	98672E-14	_0.00000	.12810L-12	0.00000	+ 22942E+00	_0.0050 <u>0</u> _	37544E-01	0.00000
11747E+00		126625-13	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	97093E-I4	0.00000	13843E-12		22942E+00	0.00100	.37544E-01	0.00000
30891E-01	0.00000	50509E-14"	0.00000			.Ž3462E-13	0.00000	.86590E-01	0.00000	.200476+00	0.00000
.30891E-01				30931E-13		.94918L-14		.86590E-01	0.00000	20647E+00	0.00000
80915E-01		12290E-12	0.00000	80715E-14	_0.00000	66747E-13	0.00000	.15696E+0Ö	,ó•0000ō	15625E+Q0	``o* <u>oō</u> ooo
-80915E-01	0.00000 .	20465E-13	~a.ooooo			~.35730E-13	~0.00000	.15696E+00	0.00000	-15625E+00	0.00000
.879316-01		140725-13		.86667E-14				14421E+00		.13390c+00	0.00000
879315-01		55125L-13		-114852-14	0.00000	.41001e-13	0.00000	14421E+00	0.00000	~.13396L+00	0.00000
	-										

NATURAL	FREQUENCY =	.149273E+04
NATURAL	FKŁOUENCY≠	*149273E+0

TX REAL	T.K IMAG	TY REAL	TY IHAu	TZ KEAL	T	KX KEAL	KX Ihag	RY .	KY IHAĞ	- RZ -	RZ
.21367E-13	0.00000	.10584E+00	0.00000	:10204E-01	0.00000	•17563E+00	0.00000	325826-13	0.00000	338041-13	0.00000
1439 <u>15-13</u>	0.00000	106846+00	0.00000	.10204E-01	0.00000	.17563E+00	0.00000	73990E-13			
31258E-13	J.30000	.20090L-01	0.00000	.2185>E-01	0.00000	84948E-01	0.00000			78223 <u>+</u> _1_1	
•15778E-13	0.00000	200901-01	.0.00000	21855E-01	0.00000	84948E-01	0.00000			65782E-j3	
32040E-13	0.00000	16074E+00	.0.00000	261868-01	0.00000	-28520E+00	0.00000			787076-13	
-120916-13	0.00000	.16094E+00	0.00000	26186E-01	0.00000			.3717dE-13			
762231-15	0.00000	.15205,6+00	_0.00000	>335LE-U1_				78099E-13			
4309sE-13	0.00300	15205E+00	_0.00000	53351E-01	•	20088£+00					
93925E-14	•					.61297E-13	0.00000	3984LE-14	o• จัดภัลิจั	• 19069E-1	0.00000
_ •22732E-13	a . 000 oo	210146-12									
264206-13		-517565-13		474788-01							
17531E-13	0.00000	-1223736-12	0_0000_0	474/8E-01	0.00000	~~.41899E~13	_0.00000	20999E-13	0.00000	.1295 (E-1.	. 0.00000
28703E-13	_0.00000	15205E+00	_0.00000	53351E-01	<u>0</u> •0000 <u>0</u>	-3698gF+00	0.00000	640,00EL4	0.00000	.72173E-1	3 0 • 10 000
218935-13						-25688E+00					
747415-13	.0.00000	160946+00	0.00000	261868-01	0.00000	28520E+00	0.00000	79783E-13	0.00000	133405-1	50*00003
58419E-14	0.00000	<del>-</del> .160945+00°	. 0.00000	261866-01	0.00000	~ = .285206+00					
43386E-13	0.00000	20090E-01	.0.00000	.21855E-01	0.00060	.84948E-01				274436-1	
43006E-13	0.00000			.21855E-01		.849486-01				52884E-I	
1638LE-13	0.00000	106341+00	_ 0.00000	10204E-01				11101E-13		-	4 0.000000
-17621E-13	0.00000	.10684E +00	0.00000	-10204E-01	0.00000	17563E+00	0.00000	37681E-14	0.00000	, -40020c-1	2 0 2 0 2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

SER TILL AT	FREQUENCY=	.150+756+04
NAIUKAL	PKEUULNLTE	

TX REAL	IAAG	REAL TY	TY -	TZ	TZ IMAG	K K K K K K K K K K K K K K K K K K K	RX	RY REAL	LHAG	RZ REAL	RZ IHAG
£23127E-14	0.00000	.18587L+00	6.00000	.124368-11	0.00000	.16884E-11	0.00000	10658E-13	0.00000	.19581É-16	0.00000
-10985E-13	0.00000		_0.00000;	12'977E-11_	0,00000	20049E-11	0.00000	16884E-13	0.00000	•5 <u>1</u> 473 <u>E</u> —14	0.00000
67445E-14	0.00000	300756+00	_0:00000_	11977E-11	0.00000	17250E-11 "	0.00000	68697E-13	~0.00000 [=		_0,00000_
52666E-13	0.00000	300756+00	0.00000	11731E-11	0.00000	•17652L-11	0.00000	697988-13	0.00000	·•43649 <u>E</u> =14	0.00000
377518-10	0.00000	.31621E-13	0.00000	-24351E-13	0*00000	.2d370b-11	0.00000	. •36292E-13	_0.002.00	.15315L-12	
10363E-13	0.00000	263215-12	0.00000	-21800E-14	0.00000	7-33635E-11	0.00000	37370E-13	u. 00000	746651-13	[0] 000000
-252058-13	0.00000	.30075t+00	0.00000.	<u>.</u> 10499E-11_	_0.00000	,173036-11	0.00000	.±13320E-13	0.00000	. <u>1</u> 7119 <u>E</u> -12	0.00000
.17160E-13	0.00000	. + 30075[+00	0.00000	93658E-12	0.00000	.23382E-11	0.00000	398298-13	0.00000	.395316-13	
-70134E-14	0.00000	105878+00	0.00000_	1535ÌE-11	0.00000	17142E-11	Ó.00000	~81135E_14	0.00000.	24955£- <u>-13</u>	0.00000
27341E-13	0.00000	185878+00	0.00000	.14226b-11	0.00000	•					
34365E-13	0.00000	18587E+00	0*00000 <u>.</u>	19516E-11	0.00000	•					
.12572E-13	ໍ່ພໍ•ຸວ່ວນວວ໊	I8587E+00	0.00000	19654E-11	(0.00000	171466-11	0-00000	~22629E-13	0.00000	.151516-13	0.00000
+342d9E-13	0.00000	.30075±+00	0.00000	15401E-11	_0.00000	244492-11	0•00000	~ 35636E-1 <u>3</u>	<u>0.00000</u>	- <u>.5</u> 9220 <u>-</u> 13	0.00000
-60311E-14	0.00000	.300756+00	0.00000	16255E-11	0.00000	-21690E-11	0.00066	26156E-13	0.00000	-62950E-13	0.00000
-•42245E-13	0.00000	46078E-13	_0.000000	23631E-12	_0.00000.	~42934F-11	0.00000	197888-13		-46639E-13	0.0000 <u>0</u>
26183E-14	0.00000	.185878-12_	0.00000,	21893E-IZ	0.00000	39295E-11	0.00000	•39605E-13	0.00000	. 15223E-12	0. 05 0 0 <u>0</u> <u>0</u>
565312-13	0.00000	30075å+00	0.00000	•14682E-11	0.00000	26103E-11	0.00000	.98707E-14	0.00000	74689E-13	0.00000
11948E-13	0.00000	30075E+00	0.00000	15039E-11	0.00000	-23787c-11	0.00000	.32133E-13	0.00000	•15774c-12	0.00000
-827138-13	0.00000	.1¢587E+00	0.00000	16669E-11	0.00000	•25769E-11	0.00000	28752E-13	0.00000	.11607E-12	. 0.00009
40820E-13	0.00000	18587L+00	0.00000	, -16820E-11	0-00000	243376-11	0.00000	823088-14	0.00000	44121;-13	

NATURAL FREGUENCY= .151565E+04

		(12,101.2	e inceden		,					Marco
YX Real	TX Imag	ly - Keal	IMAG IY	TZ Real	TZ I HAG	RX REAL	RK Imag	RY Real	KY IMAG] [	RZ RZ RZ RZ THAG
.19464E-13	0.00000	.22990E-11	0.00000	12235£+00	0.00000	181436+00	0.00000	23910E-13	0.00000	34605E-13 0.03000
219216-13	0.0000	.232768-11	0.00000	.12235E+00	0.00000	.18143E+00	0.00000	28480E-13	o∵ooōoō	
-15034E-13	0.00000	372476-11	0.00000	.11138E+J0	0.00000	.17875E+00	0.00000	26488E-13	0.00000	27240=-13 0.00000
-89351E-14	0.00000	373396-11	0.00000	-+11138E+00	0.00000	17875L+00	0.00000	-•97525E-14	0.00000	18986E-13 0.0000
-34661E-13	0.00000_		0.00000	•309ATE-05	0.00000	3022 <u>3</u> E+00	0.00000	.46857E-13	0.00000	31132e-13 0.00000
*23936E-13	0.00300	27605E-13	0.000000	908915-02	_0.00000	.302Z3£*+0Ö	_o.ooooo	. 46672E-13	o • jo ò o <u>ö</u>	.59309E-13 0.00000
.34602E-13	0.00000	.37502L-11	0.00000	10689E+00	0.00000	.10262±+00	0.00000	.421416-13	_o. joonob	4800813-0.00000
12709E-13	0.00000	.373416-11	0.00000	.10689E+00	0.00000	1d262t+00	0.00000	30463E-13 T	0.00000	141276-12 0.00000
43792E-15	0.00000	237526-11	0.00000	.142756+00	0.00000	142951+00	0.00000	.515098-14	<u>0•</u> 00 <u>700</u>	16841E-13 0.00000
-38046E-13	0.00000	229888-11	0.00000	14295£+00	0.00000					
-54973E-13	0.00000	2J246L-11	<b>6.</b> 00000	-1142,456,400	0.00000					
-11380E-13	0.00000	231655-11	_0.00000	•14295É+00			0.00000	49603E-13		.265176-13 0.00000
59941E-13	0.00000	-3/43TE-TT	0.00000	10083£+00	.0.00000	-18565E+00	0.00000	.77915E-13	_0 <u>.</u> 00 <u>0</u> 000]	92439E-13 0.00000
-842736-14	0.00000	.38226E-11	0.00000	~. 10689E+00	0,000,0	1826ŽE+00		710276-13	0 • 000 <u>00</u>	10873E-12 0.00009
32823E-13	0.00000	305178-13	0.00000	90891E-02	0.00000	30223E+00	0.00000	28614E-13	0.00000	.85545E-13 '0.00000
-54899E-13	0.00000	215256-14	0.00000	908Ä1 <u>E</u> ÷05_		-30223E+00		43185E_13	<u>0.0000</u>	.230596-12 0.00000
.62209E-13	0.00000	374760-11	0.00000	11136E+00	0.00000	.17875E+00	0.00000	242458-14	0.00000	.85313e-13 0.00000
7-59348E-13	0.00000	377926-11	0.00000	.11138E+00	0.00000	17875E+00	0.00000	:36897E-13	0.00000	17983E-13 0.00000
146646-13	0.00000	.227658-11	0.00000	.122351+00	0.00000	181436+00	0.00000	26556E-13	0.00000	
32777E-13	0.00000	.24054E-11	0.00000	12235E+00	0.00000	.18143E+00	~~o.oooo~~	.15711E-13	0.00000	77763E-14 0.00000

		ASUTAŘ	L FREGUEN	CY= 156512	E+04						
TX REAL	IX	TY .	TY 1HAG	. IZ REAL	TZ I HAG	KX Real	RX Imag	KY Real	YY IMAG	KEAL	RZ IHAG
.143d3E-12	0.00000	73165E-01	0.00000	93298E-02	0.00000	823566-01	0.00000	171996-12	0.00000	139616-12	0.00000
16805E-12	0.00000	.73165L-01	0.00000	932988-02	0.00000	82356E-01	0.00000	21072E-12	0.00000	.16694E-12	0.000000
13428E-12	3.00000	.29904E-01	0.00000	1828ot-01	0.00000	60357E-02	0.00000	-20860E-12	0.00000	156356-12	0.00000
	0.00000	299046-01	0.00000	1828oE-01	0.00000	60357E-02	0.00000	.22453Ē-12	0.00000	.185716-12	cōoōō•
-28769E-13	0.00000	•64611£-01	0.00000	.50528E-0Ì	0.00000	10028E+00	0.00000	13611E-12	0.00000	26807£-12	0.00000
284945-13		646112-01		.505281-01		160281+00		14457E-12	ù.00000	.19430E-12	
19012E-12	0.00000	14570E+00	0.00000	.53175E-01	0.00000	.35800±+00	0.00000	.20052E-12	0.00000	15362E-12	
-17038E-12	0.00000	.1457ÖE+00	0.00000	.53175E-01	_0.00000	.35800L+00	0.00000	-258,16E-12	_0.00000	10990E-12	_0.00000_
.10337E-12	0.00000			118328+00		.11832E+00		`14762E-12			
10442E-12	, 0.0000ò	194246+00		11632E+00'	_0.00000	<u>.</u> 					
-		19424Ê+00									
		19424E+00				11832E+00	- 0.00000	16659Ê-12	0`00000	460275-13	0.00000
		14570E+00									
		14570E+00									
		-64611E-01									
		64611E-01									
		29904E-01									
		73165E-01				82356::-01					
109ssE-12						82356r-01					
***	•	•	•	•	•						

MATURAL FREQUENCY= - .154656E+04

TX	TX IMAG .	TY .	TY IMAG	TZ REAL	TZ THAG	K X	RX IHAG	RY .	LAY IMAG	REAL _	RZ IMAG
195862-01	0.00000	884228-15	0.00000	865111-14	0.00000	55>816-13	0.00000	75551E-02	0.00000	25799E-01	0.00000
-195865-01	0.00000	.93836 <u>F</u> -13	0.00000	248676-13	0.00000	90086t- <u>1</u> 3	0.00000	75551E-02	ຸ່ນ.00ບບວຼີ	.25799E-01	
73963E-01	0.00000	.329386-13	0.00000	683441-14	0.00000	.17442E-13	0.00000	.899B0E-01	0.00000	.Z1894E+00	0.00007
73963E-01"	0.00000	44037£-15	0.00000	-52146E-13	0.00000	40180L-13	0.00000	.89980E-01		21894E+00	
-19023E-01	0.00000	.82745E-14	0.00000	851Î0E-14	0.00000	.199156-13	0.00000	65155E-01	0.0000	<u>i</u> 13836+ <u>0</u> 00	0.00000
19023E-01	0.00000	36930E-13	0.00000	10164E-14	0.00000	.92951c-13	0.00000	7.65156E-01	_`0.00000	11383E+000	0.0000 <u>0</u>
48991E-01	0.00000	-92284E-13	0.00000	35342E-13	0.00000	11856E-12	0.00000	64845E-01	0.00000	.37015E+00	0.00000
48991E-01	0.00000	.40737£-13	0.00000	·121746-13	0.00000	.18472E-12	0.00000	.64845E-01	_0.0000 <u>0</u>	39012±+00	_0.00000
.882178-01	0.00000	130076-13	0.00000		0.00000	,20378E- <u>1</u> 3	0.00000	J9986E-12			0.00000
88217E-01	0.00000	476476-13	0.00000	79669E-13"	0.00000						
				199206-14		•					
	0.00000	437726-13	0.00000	93930E-14	~0.000ç0	-35736E-13	0.00000	39585E-12		88217E-01	0.00000
						45598E-13					
48791E-U1	00000.0	10971E-13	ີ້ດ.ບວ່ວດວັ	31828E-13	0.00000	*16611E-13	0.00000	64845E-01		39015£ <u>+</u> 00	0.00000
						•419956-13					
-19023E-01	0.00000	.18367E-13	0.00000	23636E-13	0.00000	91492E-E3	0.0000	-65 I 56E-01	0.00000	11383F+00	0.00000
-73963E-01	0.00000	25d50c-13	0.00004	24482E-13	.0.00000	565616-13	0.00000	89980E-01	0.00000		_0.00000_
73963L-01	<b>~0.</b> 00000 ~	87385E-13	0.00000	-5229oc-13	000000	638396-13	0.00000	899808-01	000000	218946+00	0.00000
19586E-01	0.00000 [	•116dZE-13	0.00000	344948-14	0.00000	32097E-13	0.00000	75551E-02	ñ•0ōr <u>đ</u> o	25794E-01	0•nòooo
1958cE-01	0.00000	.206898-13	0.00000	.13844E-ĪJ	0.00000	13299E-13	0.00000	75551C-02	_ 0 • 0 0 3 3 0 0 <u>.</u>	25799L~01	0.00000

HUCK	
, witte	
farms.	
Ř	

ويو د درو د د ويو د د درو د د د ويو د د د ويو د د د ويو د د د د		
TX TX TY TY TZ TZ TZ REAL THAG REAL THAG	REAL IMAG REAL IMAG REAL	IÑAG
-49578E-01 6.0000011123E-13 0.0000037388E-13 0.00000	61343E-13 0.0000022209E-01 0.00000 .14991E-02	0.0000
.49578E-01 0.0000031807E-13 0.0000049093E-13 0.00000	18997E-14 0.0000022209E-01 0.0000014991E-02	0.00003
-50537E-01 0.0000042127L-13 0.0000064679E-15 0.00000	.220076-13 _0.00000507506-01 _0.00000275046 +00	0.60000
.50537E-01 0.00000 39937E-13 0.00000 1.16338E-13 0.00000 -	18604E-12 "0.0000050750E-01 0.00000	0.00000
-14002E-01 0.00000 35424E-13 0.00000 46893E-13 0.00000	.17450E-13 0.00000 41153E-01 0.0000015457E+00	0.00000
.14062E-01 0.00000 .248996-13 0.0000058183E-14 [0.00000	.14033E-13 0.00000 41153E-01 0.00000 15457E+00	_0.00000
.10031E-01 0.0000042517E-13 0.00000 10096E-13 0.00000	.3522dE-13 0.0000044251E-01 0.0000035612E+000	
_10031E-U1 0.0000082163E-13 0.0000026224E-14 0.00000	44075E-13 0.0000044251E-01 0.00000 .35612E+00	0.00000
.96084E-01 0.00000 .15918E-13 0.0000078884E-14 0.00000	.27705E-13 0.00000 .76057t-01 0.00000 .1107ZE-11	0.00000
.96084E-01 0.00000 1.36035E-13 0.00000 87736E-14 0.00000		
-96084E-01 0.00000 .18317E-13 0.00000 .54457E-13 0.00000		
_96084E-01 0.0000035371E-13 Q.000050262E-13 D.00000	30012E-13 0.00000 -76057E-01 0.0000011205E-11	0.00000
-10031E-G1 0.000003d176r-13 0.0000047940E-13 0.00000	.70161E-13 0.0000044251E-01 0.00000 .35612E+00	0.00000
:.10031E-01 0.0000040890E-13 0.00000 .44408E-13 0.00000	8488ZE-13] 0.0000044251E-01 0.0000035612E+00	0.00000
-14062E-01 0.0000024424E-15 0.00000 .93417E-14 0.00000	76763E-14 0.00000 .41193E-01 0.00000 .15457E+00	0.00000
.140625-01 U.00000 .50580L-13 0.0000U138525-13 0.000UU	207976-13 0.0000041153E-01 0.0000015457E+00	0.00000
50537E-01 0.0000020511E-13 0.0000060217E-13 _0.00000	1/359E-13_ 0.0000050750E-01 _ 0.00000 ~ .27504E ±00	0.00000
-50537E-01 0.00000 .16015E-13 0.00000 .32355E-13 0.00000	.27371E-13 0.0000050750E-01 0.0000027504E+00	0.00000
.49578E-01 0.0000024055E-13 0.00000 .35225E-13 0.00000	59413E-14 0.0000022209E-01 0.0000014}91E-0Ž	0.0000
49578E-01 0.00000 .19416E-13 0.00000 ~.33740L-13 0.00000	.62465e-13 0.0000022209E-01 0.00000 -14991E-02	0.00000

NATURAL FREQUENCY=	.156238E+04	
--------------------	-------------	--

TX TX	TY TY	TZ REAL	YZ [HAG	RX KEAL	RX IMAG	RY REAL	RY [HAG	RZ REAL	RZ THAG
	34830E-13 0.00000	)16252E14(	0.00000	109834-13	0.00000	12320E+00	0.00000	97208E-01	0.00000
-12993E+00 0.00000									
95945E-01 0.00000	14063E-15 0.0000	90100E-14	0.00000	12199E-12	0.00000	*15940E+00	0.00000	27375E+00	0.00000
959458-01 0+00000	64003E-13 T0.0000	105236-13	0.00000						
-48150E-01 0.00000				.82912E-13					
-48150E-01 0.00000		34469E-13	å•oó000 <u>.</u>	93712E_13					
14554E+0J 0.00000	38806E-14 0.0000			.12820E-12		•186546+00			
.14554E+00 0.00000									
_54700E-01 _0.00000		48143E-13	Qo ô o o . <u>.</u>		o•oōo <u>ōo</u>	335 <u>20E~11</u>	0.00060	.54700E-01	0.00000
54700E-v1 J.00000	378903-13 0.0000	15450E-13	0.0000						
	.31235L-13 0.00000								
	38179E-130.0000							,	
	29213L-13 0.0000								
	. *81643E-13 0.0000								
	20060c-13_0.0000								
	28600E-13 0.0000								
95945E-01 U.00009	1686#£-13 0.0000	058703E~13 _\	0.00000	849126-13	0.0000				
95945E-01 U.00000	•					15940E+00			
12993E+00 0.00U00	47412L-13 0.0000	0 -63677E-13	0.00000	57585E-13	0.0000			97208E-01	
.129932+00 0.00600	.91821E-14 9.0000	0590936-13	0.00000	•35060E-13	0.00000	.123202+00	0.00000	.97203E-01	0.00000

	THÀ TURAL FREQUENC	Y=,_, -,1564716	÷04						
TX TX TX TAG	TY THAG	TZ REAL	TZ 1HAG	RX REAL	RX IMAG	ŘÝ ŘEAL	IHAG	RZ REAL	RZ IMAG
11990É+00 0.000002	1817Ē-13 0.00000 _	31009E-13	0.00000 -	. 137838-13	0.00000	11840E+00	0.00000	• 39330E-01	0.00000
]-11990E+03 0.000002	1451E-1 <u>3</u> 0.00,000		<u>0</u> .00000 _ '	.39181 <u>E-</u> 13	0.00000	118406+00	0.0000	96990E-01	0.00000
.10630E+00 0.00000 13	94336-13 0.00000	.87811E-14	0.00000 -	-12385E-12	0.00000 -	17021E+00	0.00000	-22051E+00	0.00000
F-10630E+00 0.000001	.0822È-14 0.0000Ö	399148-15	0.00000	.32237E-13	`	.170216+00	0.00000	220515+00	0.00000
50967E-01 0.000002	59158-13 0.00000	93112E-14	0.00000	-25d14E-13	0.00000	.15154E+00¯	0.00000	1289\$£+00_	0.0000
.50967E-01 0.00000 .2	0936E-13 . 0.00000 ]		0.0000 -	.74401E-13	0.00000	-15154E+00	0.00000	12392E+00	0.00000
.14645E+00 0.000003	35387E-13_`0.00000	29201E-13	`à.00000 -	.38118E-13	0.00000	.19933E+00 <u>.</u>	ີ່ວັດດີດີດູ໌. ຜ	-10549E+00	_o.ooooo <u></u>
14645E+00 0.000003	81730L-13 0.00000	187446-14	0.00000 -	94372E-13	0.00000	.1993JE+00	n;ŏono <u>ŏ</u>	.10549E+00	0.000000
81882E-01 0.00000 .4	7612E-14 0.00000	.68200E-14_		.11756E-13"	0.00000	.49e01E-0[	_o-ooooo	.18572E-11	0.00000
.818826-01 0.00000 .1	17224E-13 "0.00000"	.26754E-13	0.00000						
F.81882E-01 0.00000	322246-14 0.00000	56044E-14							
081882E-010.00000	ţġ719̃Ĺ-13 _ 0.00000.	11296E-14	<u></u>	.10346E-13	0.00000	.99601E-01	0.00000	18309E-11	0.00000
	141246-13 0.00000	41252E-13	0,00000	.1871 <u>3E-13</u>	0.00000 -	.19933E+00	0.00000	.10549E+00	0.00000
14645E+00 0.00000	22419E-13 0.00000	.16116E-13	0.00000	.30938 <u>E-</u> 13	0.00000	.19933E+00	0.00000	10549E+00	0.00000
50967E-01 0.00000	205076-13 0.00000	-,11490E-13	0.00000	.27055E-13	0.00000	.15154E+00	0.00000	12892E+00	0.00000
50967E-01 0.00000	57551E-14 0.00000	-21704E-13	o. <u>ō</u> oაგი	15070E-12_	0.00000	15154E 00	0.00000	.12892E +00	0.0000
	151946-[4][0.000000]	5]813E-[14]		~32700t-13	0.00000	.17021E+00		22051E+00	0.02000
1063GE+00 0.00000	25130E-13 0.00000	85990E-14	_0.00000_	.10404E-12	0.00000	.17021E+00	0.00000	. 22051E+00	
11990E±0J 0.00000 .	337386-13 0.00000	.11641E-14	0.00000	.59771E-13	0.00000	.1184uE+00			ั้ง • งุกจึงกั
	28656E-13 ~0.00000	29990E-L3	^ó.oouoo ^~	.44191E-13	0.00000	-11840E+00	<u> </u>	.96970E-01	0.00000

NATURAL FREQUENCY - 1501408+04

TX	TX TY	TY ÎHAG	TZ . REAL	TZ ZHAG	RX	RX THAG	RY REAL	RY THAG	ŘZ KZ REÁL IHÁG
",1073E13	o obuon ==19592E+00	0.00000 -	84425E-01	0.00000	27528E+00	0.00000	34958E-13	_0 × 000 00 ===	0924E-17
	G 0000 1 195925 00	0.00000	84425E-01	0.00000	27528E+00	0.00000	52631E-13	0.00000 - 3	Troaf-ra o pooni
~ = a = 3 = 0 · 1 · 1	0.00000 49743501	0.00000	-58925E-01	0.00000	333881+00	0.00000	64269E-13	<u></u> 0.000007	8301F-13 0.000ñ
.90060E-13	0.00000697428-01	0.00000	.58925E-01,	o • 0 0 0 0 0	33388E+00	0.00000	.64883E-13	0.00000.0	7,373E130.00000
:•3978JE-13	0.00000445976-01	ò <u>.</u> 00000	31688E-01	0.00000	.79350E-01	0.00000	11133E-13	0.00000 -14	2707E-13 0.00000
.24128E-13	D.00000 .44597E-01	0.00000	.31688E-01	0.00000	.79350E-01	0.00000	170325-13	0.00000	2551E-12 0.0000C
361586-13	0.00000460528-02	0.00000	20740E-01	0.00000	76626E-01	ักักกกกัก		_ 0.00000	1574E-12 0.0300
•10395E-12	0.0000047360L-02	0.00000	20740E-01	0.00000	76628E=0 <u>L</u>	_0.000000_	49314E-13	0.000001	35316-15 0.00000
						••••	4		_
	0.0000047360E-02 0.0000047360E-02								
-2/437t~13	0.00000 -47360E-02	0.00000	16173E-0Ĺ_	0.00000	16173E-01	0.00000		0.00000	54386E-13 0.0000
71591F-13	0.0000046052E-02	0.00000	.20740E-01	0.00000	76626E-01_	0.00000	99904 <u>E</u> -13	0.00000	\$55316-13 0.0000
-75052F-13	0.00000 .46052E-02	0.00000	.20740E-01	0.00000	76626E-01	0.00000	.92220E-13	0.00000 .	60423E-13 0.0000
ำวัลก็พระการ์	0-00000 -44597k-01	0.03000	31688E-01	ā : 0 ó o o o	~79350E-01	0.00000	59897E-13	0.00000 .	15513F-15 0.0000
_ 512776=13	a.aanun .44597E~01	0.00000	31688E-01	0.00000	.79350E-01	0.00000	41795E-13	0.00000	520°11€-13-0-0000
=.355,37E-13	0.00000 .69742E-01	0,00000	58925£-01	_0,00000	333886+00	0.00000		0.00000	10017E-12 0.0000
.758791-13	0.00000697426-01	0.00000	58925E-01	_0_00000	~.33388E+00	0.00000	.43446E-13	0.00000	364305-14 0-0000
-512346-13	U.9000019592E+00	0.00000	.84425E-01	0.0000	2/528c+00	0.00000	1/329E-13		348496-13 0.0000
49352E-13	0.00400135926+00	0.00 <u>0</u> 00_	84425E-OL	~0.00000	275288+00	0.00000	*541ADFT.		5.40% CF 4577 420005

_		ŅATURA		CY= .160117							· · · · · · · · · · · · · · · · ·
TX REAL	TX IMAG_,	TY	TY . IHAG	T/ REAL	TZ 1HAG	RX	RX IMAG	RY REAL	KY IMAG	RZ	RZ THAĞ
		198261.00	0.00000	.04884E-01	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	.27817E+00	0.00000	.7893BE-13	`ō.ooooō´	.84991E-13	
.12576E-12	0.00000	19826E+00	0.00000	.84834E-01	~0.00000						
.11017L-12	0.00000	70664E-01	0.00000	-,58911E-01	0.00000			735538-13			
116266-12	0.00000	.70664Ė-01	0.00000	58911E-01	0.00000			87722E-13			
.21173E-13	0.00000			32511E-01				19022E-13			
26417E-13.	0.00000	42822E-01	0.00000	, 325116-01	.0.0000	76582E-01					
.61449E-13	0.00000	.789775-02	0.00000	-:17350E-01	0.00000	.6dl836-01	0.00000	58614E-13		28849E-12	2 0.00000
11449E-12	0.00000	78979L-02	0.00000	.173508-01	0.00000	.68183:-01	0,00000	1062 5E-12	0.00000	.238791-1	2 0.00000
86872E-13	0.00000	41633E-12	_0.00000_	10812E-01	0.00000	12680L- <u>1</u> 1	_0.00000	179158-13	0.00000	24878£-1	0.00000
		.44630E-12									
	0.00000	45345E-12	_0.00000	10812E-01	0•00000	_					
-47678E-13	`0.00000	-42416E-12	0.0000	10812E-0Î	0.000000	~~.13281E-Î1	` 0.00000		0.00000	.62993E-1	3 0.00000
~48444E-13	-0.00000	789796-02		17350E-01				89997E-13	<u>~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~</u>	15 <u>784E-1</u>	3 0.00000
49365L-13	0.00000	78979E-02		L735@E <u></u> 01	o_ooooo	68183E-01	· 0.00000	74656E-13	0.00000	.13698E-1	3 0.00003
-,44687E-13	~0.00000	420226-01		32511E-01		765828-01	~ ~6.555655	.78456E-13		91347E-1	3 0.00000
-57666E-13	0.00000	-42822E-01		325116-01	0.00000	. 76582L-01	o•onō <u>ó</u> <u></u>	87619E-1	<u>0</u> *000 <u>00</u>	1113466-1	2 0.0000
.72785E-13	0.00000	.706648-01	.00000u	589116-01		3 34 42E +00	ั้วังจึงจังอั	10973E-12	0.00000	34073E-1	3 0.00000
-1208928-13	<b>3.0000</b> 0	70654E-01	00000.0	58911E-01	. 10.00000	33442=+00	0.00000	98311E-i.	, 0•00000		i 0.50,000.
75750E-13	J.00000	19826E+00	0,90000	.84884E-01	. 0.00000	278178+00	~0.0000	.47088E-13	3 ~ jo. obuvo	62298E=1	3 _0.00000
•79597E-I3						27817E+00					

NATURAL FREQUENCY= +165625E+04

TX REAL	TX IHAG	TY KEAL	TY IMAĞ	TZ REAL	TZ I MAG	RX REAL	RX -	REAL .	RZ RZ IHAG ŘEAL INĀG
47273E-13	0.00000	49682E-13	0.00000	.10640E+00	0.00000	.260166-01	.0.00000	.51340E-13	0.00000 .56496E-13 0.0000
833426-13	0.00000	.80711E-13	0.00000	10640E+00	~o.ooooo	20016E-01	0.00000		0.0000042286E-13 0.0000
.64727E-13	0.00000	.84175E-14	0.00000	.43328E-01	0.00000	.28142E+00	0.00000		0.00000614366-13 0.00000
107276-12	0.00000	714360-13	0,00000	43328E-01	0.00000	281426+00	0.00000		0.00000 30985 -13 0.00000
121926-12	0.00000	.40753E-13	0.00000	.13857E-01	0.00000	.21049E+00	0.00000		0.00000 .535038-13 0.00000
•11340c-12	0.00000	.45087t-13	0.00000	138578-01		210496+00	0.00000		0.0000014776E-13 0.00000
.242208-13	0.00300	452346-13	0.00000	295446-01	0.00000	.31574E+00	0.00000	=	0.0000055620E-13 0.00000
277>06-13	0.00000	206396-13	0.00000	-295448-01	0.00000	31574E+00			0.0000093544E-13 0.09000
223218-13	0.00000	182446-13	0.00000	902786-01	2.00000	.90278E-01	0.00000	.12865E-13	0.00000101176-13  0.00000
-14437E-13	0.00000	139648-13	0.00000	.40278E-01	0.00060				
.43300E-14	0.00000	.64480£-14		.90278E-01					
471832-13	0.00000	111286-13	0.01000	90278E-01	0.00000	902781-01	0.00000	15038E-13	0.00000 .21772E-13 0.00000
54031E-13	0.00000	.14325E-13	0.00000	.295448-01	0.00000				0.00000620405-13 0.00000
.584756-13	0.00000	.67095E-13	0.00000	29544E-01	0.00000				0.00000 718008-13 0.00000
61673E-1J	0.00000	67455E-13	0.00000	138578-01	_ 0.00000				0.00000 201776-13 0.00000
B4565E-14		1/3085-13	ਹื⊌ถถ <i>ด</i> ์₀๋	.138578-01	0.00000				0.0000013112E-13 9.00000
86665E-13	0.00000	.97777E-14	0.00000	43328E-01	0.00000	-			0.0000018581E-12 0.00000
59806E-13	0,00000	731736-13			0.00000	281426+00	0.00000		0.00000 42559E-13 0.00000
11720E-12	0.00000	.379446-13	0.00000	10640E+00	0.00000	.20016E-01	0.00000		0.0000063550E-13 0.00000
-10263E-12	6.00030	33305E-13	0.00000	.10640E+00	0.00000	26016L-01	0.00000	.76697E-13	U.00000 .36333E-13 0.00000

į
•

· ·		NATURAL	. FREQUEN	CY= .162483E	:+04						
TX REAL	TX IHAG	TY	TY IHAU	TZ PEAL	TZ IMAG	RX PEAL	RX Imag	RY REAL	YAY QAhl.	RZ —	R.L.
84794E-01	0.00000	85263E- <u>13</u>	0.00000	_ • 17461E-12	0.00000	-22880E-12	0.00000	.74136E-01	0.00000	.85204E-01	0.00000
.84794E-01	0.00000	62183E-13	0.00000	14554E-12	0.00000	98156E-13_	0.00000	74136E-01	_ 0.00,000	85204 <u>E-01</u>	0.00000
-15130£+00	`0.00000	-,40272E-13	0.00000	189646-12	0.00000	.8>805E-13	0.00000	12654E+ÒO	~ 0 <b>~</b> 000 00 0	00 +356 AF 1 •	0.0000j
151302+00	0.00000	49257E-14	0.00000.	.153608-12	0.00000	16583E-12	0.00000	126548+00	0.00500	13892E+00	0.00000
•16589E-01	0.00000	939401-13	0.00000	.93247E-13]	0.00000	12458=-12	0.00000	40942E-02	_0.001 <u>0</u> 0_	37663E+00	_ <u>0</u> _00000
-116589E-01	0.00000	•33799E-13	0.00000	13106E-12	0.00000	19566E-12	0.00000	40942E-02	0.00000	.37663E+QQ	_ <u>o_o</u> ooo <u>oo</u>
126085+03	0.00000	.297J18E-13	0.00000	167498-12	0.00000	76725E-13	0.00000	.94212E-Q1	0.00000_		0.00000
.125888+90	0.00000	.52178E-13	0.00000	.20095E-12	0.00000	834881-13	0.00000	.94212E-01	ົ ນ. 00 ນ 0 0 ຼີ	368346-01	0.60000
-42733E-01	0.00000	46075E-14	0.00000	. 959938-13	0.00000	52974E-13	0.0000	30146E-11	_0.00000	.42733E-01	0.00000
42733E-01	0.00000	223531-13 _.	0.00000	95377E-13	0.00000						
42733E-01	0.00000	43910E-14	ŏ.03005	16017E-13	0.0000						
.42733E-01	_0.00990	209776-13	0.00000	20679E-14	_0_00000	478556-13	_0.00000	30162E-11		42733E-01	0.00000
.128885+00	0.00000	.402096-13	0.00003	41797E-13	_0,_00000	34850t-14	0.00000	94212E-01	0.00000	- 34834 <u>E-01</u>	<u></u>
12888E+GU	0.00000	.34988E-13	0.00000	.13102E-15		26917L-13	0.00000	94212E-01	0.00000	38834E-01	9.00000
16539E-01	0.00000	91804E-13	, <b>0</b> •00000	_=-39629E-13	0.00000	17364E-12	0.00000	-40942E-02	, n. 00000	37,663 <u>E</u> +00	0.00000.
.165d9E-01	~00000°	.69556E-15	0.00000	.32115E-13	0.00000	111836-i3	0.00000	409428-02	0.00000	• 37663E • 00	0.00000
15130E+00	0.00000	.22793L-13	0.000,00	_ +34930E=13	0.00000	141981-12	0.00000	+12654E+00	0.00000	. 13392E+00	¯ o•′ōoooo′
.15130E+00	0.00000	.372115-13	0.00000	.12719E-13	.0.00000	.80867E-13	0.00000	.12654E+00	0.00000	13945FF 00	0.00000
.84774E-01	0.00000	27157E-14	0.00000	•53109E-13	0.00000	711705-15	0.00000	74130E-01	0.00100	85204E-Q1	0.00001
84794E-01	0.00000	20000E-13	0.00000	27269E-13	0.00000	-27131E-13	0.00000	- 74130E-01	ò. 00000	85204E-01	0.00000

NATURAL	FREQUENCY=	.1636V3E+04
---------	------------	-------------

		. 1410									
TX .	TX IHAG	TY REAL	YI Dahi	TZ Real	TZ IHAG	KX . KEAL	R.K I M A G	RY REAL		REAL	
- -24201E-01	-		0.00000	.73167E-13	0.00000			• 56525E-0}			
• •		18734E-13	0.00000	20304E-13	0.00000	.859621-13	0.00000	.56525E-02			
- -80987E-01	0.00000	.33401£-13	0.00000	24686E-13	0.00000	.18948E-12	0.00000	10108E+00			
86987E-01	0.00000	~~.25338E-13	0.00000	.20313E-13	0.00000	13279L-13	0.00000			_ • 265638+00 _	
19709E+00	0.00000	.213368-13	0.00000	640758-13	0.00000	297820-13	0.00000			33622c-01	
.19709E+00	0.00000	.568045-14	0.00006	.587856-13	0.00000	.13843c-12				33622E <u>-</u> 01	
.53147E-01	0.00000	184778-13	0.00000	_ +103646-13	0.00000			78565E-01			
		35309L-13						78565E-01			
.3875cE-01	0.00000	.45762E-15	0.00000	.401528-13	0.00000	20644t-13	0.00000	69214E-02	0.00000	.5a0a8E-12	`` <b>0</b> +ō0000
38758E-01	0.00000	.144961-13	0.00000	42523E-13.	ó.00000	•					
-387582-01	0.00000	.83763E-16	0.00000	15098E-1J	0.00000						: ``o="ooo5.
387588-01	0.00000	-14884E-13	0.00000	.62347E-14	0:00000	.24d16E-13	0.00000	69214E-02	_0•'00000	-,59629E-12	
531478-01	0.00000	19910E-13	0.00000	58895E-13	0.00000			78565E- <u>0</u> 1			
53147E-01	0.00000	3759ZE-13	0.00000	641540-13	0.00000	798446-13	0.00000	78565E-01		28360E_00 <u></u>	
1970 /6+00				665456-13						.33 ₀ 22 <u>t</u> -01	
.19767E+00	0.00000	45062L-13	0.00000	.62992E-13	0.00000	10d07E-13	0.00000			_1,0-3,522,620,1_ 	
80987E-U1	0.00000	49209 <u>E</u> -13	6.00000	12200E-12	, 0.00000	43063E-13	_ o•oōooō	10103E+00	.0.0000	24542-400	0.0000
807a7F-01	0.00000			10904E-12						26563c+00 20798c-01	
-242016-01	9.00-00	.2421313	0.00000	116436-12							
242018-01	0.0000	67160E-16	0.0000	.10917E-12	0.00000	75165E-13	0.00000	•56525E-02	_0.00000	*501.40E_AT	-
•											

		"NA TURA	L FREQUEN	CY= _ +163408	3E+04						
TX REAL	TX THAG	≺EAL	TY IHAG	TZ * RĘAL	TZ I mag	R X n E A L	RX IMAG	RY REAL	I HAG	RZ	RZ IHAG
.23957E-01	0.00000	102046-12	0.00000	143526-12	0.00000	185176-12	_0.00000	66426E-02	_0.00000		1 0.00000
.239578-01	0.00000	.66883E-13	0.00000	.99738E-13	0.00000	.67090£-14	0.00000	~66426E-02	0.00000	-22435E-0	1 0.00000
.850156-01	0.00000	.897996-13	0.00000	.169658-12	0.00000	280386-12	0.00000	-10538E+00	0.00000	1 .27121E∓0	0.09900
-95015E-01	0.00000	L.10425E-13	0.00000		_0.00000	238226-13	0.00000	. 10538E+00	0.00000	27121 <u>E</u> +0	0.00000
.19804E+U0	0.00000	10450L-12	0.00000	10622E-12	0.00000	107816-12	0.00000	183836+00	0.00000	416816-0	0.00000
-19804E+00	0.00000	13932E-13	0.00000	.12249E-12	0.00000	.57716E-13	0.00000	18383E+00	0.00000	41681E_C	1 0.00000
.50922E-01	0.00000	.37706E-13	0.00000	14929E-12	_0.00000	14421E-12	_ 0.00000	.79750E-01	_ 0.00000	27101E±0	0.00000
•50922E-01	0.00000			143791-12		.50361E-13	0.00000	.79750E-01	0.0000	27101E+0	ງດ ຶ ດ. ໂດ ງ ດວດ
.23470E÷01	0.0000	87432Ē-Ī4				19731E-13	0.00000	36446E-12	0.00000	234706-0	0.00000
		18966E-14							-		
		871926-14									
		-46264E-15					_ <u>0-</u> 000 <u>0</u> 0	∃.36940E-13	<u></u>		01_0.000 <u>00</u>
		.i9965 <u>E</u> -13									
		40509£-13									
		.66847E-13									
19804E+00		16632E-13									
		15790E-13				' <del>-</del>		105381+0			00 0.00000
		210508-15									000.00000_
.23957E-U1						.544678-13				224356-	01 0.00000
		.59526E-14									
-•\S 3A216-0T	0.00000	. • 777200-14	0.00000	~ #4444 FC_T	. 0.00,000	_ ,••••••		•	-	•	

ţ	
£	
Ž	
3	•
3	
Ž	
,,	•

<del></del> .		NA TURA	L	CY= .1623548	E + 0 4						
TX REAL	TK . Imag	TY KEAL	TY IMAG	TZ REAL	T Z I MAG	REAL	RX Imag	RY REAL	IMAG	KEAL TIHAG	
.86194E-01	0.00000	-211748-13	0.00000	132388-12	0.00000	-,73945E-13				871726-010.00	
86194E-01	0.00000	.51764E-13	0.00,000	.597788-13	0.00000	398208-14	0.00000			.87172E-01 0.00	
15447E+U0	0.00000	429196-13	0.00000	.7883d£-13 [~]	0.00000	228101-12	0.00000			13766E+00 '_0.00	
15447E+00	0.00000	7-1432946-13	_0.00ōōòò	25668E-13	_0.00000_	.16477E-12	0.00000	13027E+00	0.000000	.13766E+00 0.00	0000
127368-01				92685E-14	0.00000	65777E-13	0.00000	.18366E-02	0.00000	.37633E+00, 0.00	נטטט
-12936E-01	0.00000	. 46781E-13	0.00000	. 183531-13	0.00000					37633E+00 0.00	
.12184E+00	9.00000	.863276-14	0.00000	.92764E-13	0.00000					419346-01 0.00	
12184E+0J	0.00000	203788-13	0.00000	87031E-13	0.00000			99490E-01		•	
406Z6E-01	0.00000	.93308E-14	0.00000		0.00000	19193E-13	0.00000	43274E-01	" n• önnőő .	.33905E-11 0.00	722-
-40626E-01	0.00000			.50958E-14							
40626E-01									_00000 <u>v_</u> _	33577E-11 0.0	0000
`-40026E-01					0.00000					41934E-010.0	
		239781-13					. v v v v v v	12.09490E-01	0.000000	41934E-01 0.0	0000
12184E+0J				85278E-13						-,376336+00 0-0	
<u></u> 12930E-01		•	0.00000	.219224-14	_ v		0100000 0100000			-37633£±00 0.0	
10-306-01										.13766E+00 0.0	
15447E+00										13766E+00 0.0	2002
-15447E+00				73329E-13 11901L-12	•					.87172E-01 0.0	
-86194E-01				-						87172t-01 0.0	
<b></b> 86194E-01	J.0000	0116361-13	0.00000	4 700 7E L - LJ	2,0000	•					

•		NATURA	L FKEQUEN	CY= .166716	E+04						
TX REAL	TX IHAG	IY Real	TY THAG	TZ REAL	TZ EHAG	KX Real	RX Ihag	RY .REAL	. KY	RZ	RZ ÎMAĞ
-40043E-13	0.00000	46612E-13	0.00000	.20073E+00	0.00000	.13638£+09	0.00000	19115E-13	0.00000	99012E-13_	0.00000_
307466-13	0.00000	.13526E-15	0.00000	20073E400	0.00000	13538E+00	0.00000	34604E-13	0.00000	•10205E-12	0.00000
16520E-12	0.00000	.565366-13	0.00000	132886+00	0.00000	-25896L+00	0.00000	.16209E-12	0.00000	.38186E-13	<u>0.00000</u>
•16953E-12	0.00000	.23129c-13	0.00000	.132886+00	0.00000	25d96E+00	0.00000	· .11487E-12	0.00000	623498-13	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~
.57273E-13	J.00000	676926-14	0.00000	.88700E-01	0.00000	.20901C+00	0.00000	56923E-13_	0.00000	40198E-12	0.00000
76991E-13	0.00000	547018-13	0.00000	88700L-01	0.00000	20901E+00	0.00000	39830E-13	0.00000	32243t-12	0.00000
.11763E-12	0.00000	.349786-13	0.00000	22353E+00	0.00000	.47261E-01	0.00000	83454E-13	0.00000	24364£-12	0.00000
12112E-12	0.00000	37691E-14	0.00000	•22353E+00	0.00000	472611-01	0.00000	72155E-13	0.00000	530886-13_	ั้ว ๑๐๐๐๐ัง
41123E-13	0.00000	-307918-14	0.00000	.66986F-01	0.00000	.475916-12	0.00000	.17460F-13	0.00000	41358E-13	
•19912E-13	0.00000	288531-14	0.00000	66986E-01	0.00000						
-55294E-L3	0.00000	.33310E-13	0.00000	.669dbE-01	0.00000						
85956E-13	0.00000	12625E-13	0.00000	66986E-01	0.00000	44338E-12	0.00000	36868E-14	0.00000		0.00005
.133726-13	0.00000	14256E-12	0.00000	223534+00	0.00000	47261E-01	0.00000	48807E-13_	ō.00500 <u>,</u>	31448E-12_	_0 <u>_0</u> 00000 <u>0</u> 0_
122728-13	0.00000	.46285Ê- <u>1</u> 3			,0.00000	472618-01	0.00000		0.00000	.47169E-12	0.00000
- 217616-12	0.00000	534636-13	0.00000	-88700E-01	0.00000	209016+00	0.00000	.1966JE-12	0.00000	-69948E-14	0.00000
.28916E-12	0.00000	•12797L-12	0.00000	88700E-01	0.00000	.20901E+00	0.00000	-18881E-12	0.00000	56205E-14	0.00000
15755E-12	o.00000	10870E-12	0.00000	13288E+00	0.00000	25896E+00	0.00000	117358-12	_ o. ooooo_	24319E-12_	0.00000
13477E-12	0.00000	23317E-13	0.00000	-13288E+00	0.00000	.25896£÷00	0.00000	11779E-12	0.00000	45845E-12	
25133E-13	0.00000	.27596E-13	0.00000	.260738+00	0.00000	13a3dE+00	0.00000	62823E-14	0.00000	950141-13	0.00000
194288-13	0.00000	33157c-13	0.00000	200736+00	0.00000	-13638E+00	0.00000	153721-13	0.00000	-110635-12	_0.00000_

		NATURAL	- EKFORENC.		-		•				
TX REAL	TX IHAG	TY «EAL	TY IHAG	TZ REAL	TZ 1MAG	R X Real	RX Imag	RY REAL		RZ T	
.99159E-14	0.00000	.148136-12	0.00000	18569E+00	0.00000	15685E+00		25872E-13			
21773E-13	0.00000	21102L-13	0.00000	.185698+00	0.00000	.15685E+00		_ •29503E-15			
.43116E-13	0.00000	27003E-12	0.00000	.22405E+00	0.00000	156186+00		81386E-13			
12596E-14	0.00000	11075E-12	0.00000	22405E+00	0.00000	.156181+00		21376E-13			
31168E-13	0.00000	.703816-13	0.00000	91327É-01	0.00000	90778E-02		32593E-13		•	
.5823aE-13	0.00000	.323700-12	0.00000	.71327E-01	0.00000	. •98778E-02	0.00000	26146E-13			
.905478-13	0.00000	22737b-12	0.0000	.230206+00		.125256+00				.22086c-12	
16003E-13	0.00000	47878E-13				125251+00					
.29014E-13	0.00000	.64455E-13	0.00000	16721E+0Ó	0.00000	. *10721E+00	0.00000	15752E-13		.25970E-13	<u> </u>
•3551>E-14	0.00000	65027E-13	0.06000	.16721E+00	0.00000						
=.14869E-13	0.00000	.65232E-13	0.00000	.16721E+00	0.00000						
1.38357E-14		67545t-13	~~	1672 IE+00	0.00000	16721E+00	0.00000	20745E-13	0.000.00	-67 4 3 6 E - 1 4 "	0 <u></u> 0,00,000,000
.32175E-13	0.00100	.23404E-13	0.00000 _	23ó20€ €00 _	0.00000	125256+00	. 0.00000	55 <u>0</u> 39E-13		158066-12	0.00000
42257E-13		.297941-12	0.00000	. <u>5</u> 3020E+00	0.00000	12525E+00	0.00000	43432E-13	0.00000	.63459E-13	0.00000
=.84393E-13	0.00000	41583E-12	0.00000	.91327E-01	0.00000	98778E-02		.87420E-13			
~75623E-13	0.00000	40987£-13	0.00000	913276-01"							
10912E-12	U.00000	.12354E-12	0.00000	22405E+00	0.00000						
~6575QE-13	0.00000	.334706-12	0.000000		0.00000	•15a1dE •00	0.00000	.68923E-13	0.00000	200408-12	_0*0000 <u>3</u>
.8631/E-13	0.00000	-24437E-13	0.00000	.18569E+00	0.00000	156851+00					
965555-13	0.00006	146561-12	0.00000	18569E+00	0.00000	.15685c+00	0.00000	61503E-13	0.00000	10562E-12	. 9.00000

		, NATURA	L FKLGULN	CY= .171962	L+U4	·					
TX Real	TX 1mag	. TY REAL	TY Imaj	TZ Real	TZ 1mag	RX Real	RK IHAG	RY REAL	KY THAG	RZ REAL	RZ IHAG
64782E-13	0.00000	576636-01	0.00000	. 1885dE-U2	0.00000	57a33E-01	0.00000	•31520E-13	0.00000	150098-13	0.00000
.52722E-13	0.00000	.59669E-01	0.00000	.38858E-02	0.00000	57833E-01	0.00000	16873E-13	0.00000	57341E-13]	0.00000
-29849E-13	0.00000	.65336c-01	0.00000	47754E-01	0.00000	-14164c+00	0.00000	113766-13	0.00000	.15319E-12	0.00000
18122E-13	0.00000	653361-01	0.00000	.477548-01	0.00000	.14164E+00	0.00000	.196sl£-14	0.00000	10661 <u>-</u> -12	0.000000
-63694E-13	0.00000	.10522£+00	0.00000	.13756E-01	0.00000	.355126+00	0.00000	69798E-13	0.00000	22015E-14	0.00000 _
580116-13	0.00000	105226+00	0.00009	13756E-01	0.0000	•35512E+00	0.00000	46421E-13	0.00000	-42465E-13	0.00000
·•67613E-13	0.00000	.91973E-01	0.00000	41698E-01	0.00000	.20157E+00	0.00000	. 44205E-13	0.00000	13467E-12	0.00000
-29400E-13	0.00000	91973L-01	0.00000	41698E-01	0.00000	.20157E+00	0.00000	14060E-13	0.00009	_ •1406 <u>2</u> É-12	0.00000
42573E-13	0.00000	-30660E-12	0.00000	23698E-01	0.00000	.52615E-13	0.00000	•13254E-1J	_0.000000	13807 <u>E</u> -13	0.00000
-11906E-14	0,00000	281016-12	0.60000	2369BE-01	0.00000						
.+32437E-13	0.00000	,298476-12	0.00000	23698E-01	0.00000						
21121E-13	9-00000	28112E-12	0.40000	23698E-01_	0.0000	44212E-13	0.00000.	14571E-13	0.00000	20054E-14	
-47963E-13	0.00000	91973E-01	0.00000	416988-01	0.00000	20157E+00	0.00000	621056-13	0.00000	40815E-13	0.00000
69389E-13	0.00000	•91973E-01	0.00000	416988-01	0.00000	26157E+00	0.00000	670476-13	0.00000	218276-13	_0.00000
-42131E-16	0.00000	105228+00	0.00000	1/3756É-01		~+35512 <u>+</u> +00	0.00000	99189E-14	u. ბიინი	46995E-13	0.0000
13397E-13	0.00000	105226+00	0.00000	.13756E-01	0.00000	-+35512E+00	~`0.00000	8090dE-14	`0.00000	752586-13	
81698É-14	0.00000	65336E-01	0.00000	47754E-01	0.00000	14164E+00	0.00000	65321E-14	0.00000	12983E-13	0.00000
.24583E-13	0.00000	.65336L-01	0.00000	.47754E-01	0.00000	141646+00	0.00000	15401E-13	0.00000	.36498E-13	0.00000
5.55465E=14	0.00000	•596676-01	0.0000	.3885 * 05	0.00000	.57833E-01	0.00000	19208E-14	0.00000	11111dz13_	_0.00000
_32354É-13	_0*00000	59669E-01	0.00000	.38858E-02	0.00000	57833E-01	0.00000	45615E-14	` 0+0 <u>0</u> 0000	19541E-13	.0.0000

"NATURAL FREQUENCY= .165778E+04"

TX REAL	TX IHAG	TY REAL	TY [HAG	T <i>I</i> Real	TZ IHAG	RK KEAL	RX I mag	RY REAL	RZ RZ RZ IMAG IMAG
•38537E-13	0.00000	.586576-14	0.00000	.892276-02	0.00000	55711E-01	0.00000	28313E-1J	0.00000 -144428E-13 0.00000
45087E-13	3.00000	767826-14	0.00000	89227E-02	ă.00000	.55711E-01	0.00000	~.42280E-13	0.00000 -77638E-13 0.00000
41879E-13	0.00000	15967E-13	0.00000	.13752E+00	0.00000	.21554E+00	0.00000	-31311E-13	0.00000 .84650E-14 0.00000
.35o91E-13	0.00000	.15909E-14	0.00000	13752E+00	0.00000	21554E+00	0.00000	.44248E-13	0.00000 .44680 <u>e-13 0.00</u> 000
-197256-13	3.00000	.29252:-13	0.03900	63270E-01	0.00000	.96220E-01	0.00000	46766E-14	0.000001d427E-13  0.00000
10344E-14	0.00000	.14847⊨-14	0.00000	632708-01	0.00000	962206-01	0.00000	24896E-13	0.00000 36467E-14 0.00000
473908-14	0.00000	26806E-13	0.00000	-10046L+00	0.00000	.35862L+00	0.00000	•4055d£-13	0.0000010119=-15_0.01000
.581216-13	0.00000	154196-13	0.00000	10046E+00	0.00000	35862E+00	0.00000	.48162E-13_	0.00000 61001F-13 0.00000
68310E-14	0.00000	26216E13	_0.00000	18364E+00	_0.00000	45213b-11_	0,00000		0.00000 .95410E-14 0.00000
210508-13	6.09600	.25357L-13	0.60000	.183648+00	0.00000				•
-3795dt-14	0.00000	7575de-14	0.00000	183646+00	0.00000				
67262E-14	0-00000	-92741E-14	0.00000		<u></u>	45018E-11_	0.00000		0.0000 -92630E-14 0.00000
-53124E-13	0.00000	.405841-13	0.00000	.10046E+00	0.00000	3>8628+00	0.00000	678448-13	0.00000284782-130.00000
98647E-14	u.00000	+37091C-13	0.00000	10046E+00	0.00000	*35862£+00	0.00000	70749E-13	0.00000 .498418-130.00000
684076-13	0.00000	51147L-13	0.00000	63270E-01	0.00000	9u220E-01	0.00000	•10255E-12	0.00000 .41670t13 0.6000 <u>3</u>
.85030E-13	0.00000	26653E-13	0.00000	.63270E-01	0.00000	.96220E-01	0.00000	.99709E-13	0.0000031362E-13 0.00000
8742dE-13	0.00000	•31750E-13	0.00000	•13752E+00	0.00000	21>548+00	0.00000	78602E-13	0.00000 .52821E-13 0.00000
691716-13	0.00000	13616E-13	0.00000	13752E+00	0.00000	.21554E+00	0.00000	67950E-13	0.0000017652E-12 0.00000
282956-13	0.00000	44400E-14	0.00000	.892276-02	0.00000	.5>711E-01	0.00000	-272784-13	0.00000169486-13 _0.09909
-*23766-13	4.00000	205961-13	0.60000	892276-02	0.00000	557111-01	0.00000	.35668E-13	0.00000 .22772E-13 9.00009

## NATURAL FREQUENCY= .172450E+04

•		NATUKA	AL PREGUEN	4CY= 4172450	E+04							
TX REAL	X X Qan 1	KEAL Ty	TY THAG	T/ KEAL	ST DAH1	REAL	RX EHAG	RY Real	AY .	RZ REAL	•	RZ
.35762E-13	0.00000	.63788E-01	0.00000	55062E-02	0.00000	+60589E-01	0.00000	252388-13	0.00000	29061E-	-13	0.00000
923468-14	0.00000	637886-01	0.00000	550628-02	0.00000	.00589E-01	0.00000	_ •91181E-14	.0.00000	-36514E-	13	<u></u>
616750-13	0.00000	718946-01	0.00000	51147E-01	0.00000	163156+00	0.00000	.70166E-13	0.00000	5058ŽE-	.13	0.00000-
-61489E-13	0.00000	.71894E-01	0.00000	51147E-01	0.00000	16315E+00	0.00000	.29028L-13	0.00000		13	0.00000
45755E-13	0.00000	117348+00	0.00000	40370E-02	0.00000	375346+00	0.00000	3331dE-13	0-00000	71233E-	i3 [	0.00000_
•13004E-13	0.00000	•11734E+00	0.00000	40370E-02	0.00000	37534E+00	0.00000	49363E-13	0.00000	12Ž40E-	.12_	0.00003
_=18243E=13	0.00000	875986-01	0.00000	.45239E-01	.0.00000	20271E+00	0.00000	613776-14	0.00000	510616-	13	0.00000_
51303E-14	0.00000	.87593E-01	0.00000	45239E-01	0.00000	20271E+00	0.00000	117716-13	0.00000	18757e-	13	0.00000
-17764E-13	0.00000	.49494E-Q1	0.00000	.112348-02	0.00000	11234E-02	0.00000	558858-14	0•00000_	109336-	13	0.00007_
.60560E-14	3.00000	494348-01	0.00000	·11234E-02	0.00000							
15478E-13	_0.00000	-44494E-01		11234E_02	0.00000							
31631E-13	0.00000	49494E-01	0.00000	11234E-02	0.00000	11234E-02	0.00000	21784E-13	0.00000	16396E-	·13	0.00000
21048E~15	0.00000	87598E-01	0.00000	45239E-01	0.00000	20271E+00	0.00000	-14708E-13	0.00000	=-70270E-	.13	0.00000
•33765E-13	0.00000	.875988-01	0.00000	45239E-01	0.00000	202716+00	0.00000	.17227E-13	0.00000	. 8383 <u>9</u> E-	13	0.00000
=-38021E-13	0.00000	-+11734E+00	0.00000	.40370E-02	0.00000	~375 34E+00	0.00000		0.00000	1654ZE-	12	0.0000
-56476E-13	0.00000	-11/34E+00	0.00000	403/0E-02`	0.00000	~37534E+00	_0.00000	;46628E-13	_ 0.000 <u>0</u> 0_	22 <u>145</u> E-	-12	0.0000
79325E-13	0.00000	71894E-01	0.00000	.51147E-01	0-00000	·16315E+00	0.00000	24239E-13	0.00000		-13	0.0000
40167E-13	0.00000	.71994E-01	0.00000	.51147E-01	0.00000	16315E+00	0.00000	13389E-13	00000.0	71237E-	·13 -	0.00000
911a3E-14	0.00000	-63788E-01	0.00000	.55062E-02	0.00000	.60589E-01	0.00000	156308-13	.000000	32298E-	-14	0.00000
19759E-13	0.00000_	63789E-01	0.00000	55002E-02	0.00000	.605891-01	0.00000	51663E-14	. 0. 00000	- 64890E-	·13"	0.00000

-.49212E-13 0.00000 .16167E-12 0.00000 .12010E+00 0.00000 -.26002E+00 0.00000 -.44498E-13 0.00000 -.79439E-13 0.00000 .31888E-13 0.00000 -.32449E-13 0.00000

-.11922E-13 0.00000 -.35798E-12 0.00000 -.12010E+00 0.00000 -.26002E+00 0.00000 -.35084E-13 0.00000 -.29461E-13 0.00000

RK IMAG

.12236E-12 0.00000 .29782E-01 0.00000 -.29396E-01 0.00000 -.94157E-15 0.00000 -.10427E-13 0.00000

RY REAL THAG REAL THAG

.29396E-01 0.00000 -.10144E-13 0.00000 .16366E-13 0.00003

.29396E-01 0.00000 .21771E-13 0.00000 -.16930E-13 0.00000

NATURAL FREQUENCY= -175973E+04

.15071E-12 0.00000 -.29782E-01 0.00000

TΧ

IMAG

--28824E-13 0.00000

-11034E-13 0.00000

KEÂL

- TX - REAL

NATURAL	FRL JULNCY=	-176161E+04

TX REAL	TX EMAG	TY ≺EAL	TY Imag	TZ " Real	IZ IMAG	KEVF KX	RX IHAG	RY REAL	THAG SA	RZ REAL	RZ
.275585-13	0.00000	.38794E-12	0.00000	106768+00	0.00000	93938E-01	0.00000	.743328-13	0.00000	•39106Ē-13	0.00000
437366-13	0.00000	-34887E-12	0.0000	•10676E+00	0.00000	.93938E-01	0.00000	*50146E~13	0.00000	.73025E-14	0.000000
.506428-13	0+00000	95026E-12	0.00000	.19150±+00	0.00000	113186+00	0.00000	63305E-13	0.00000	559146-13	0.00000
919276-13	0.00000	908626-12	0.00000	19150E+03	0.00000	.11318E+00	0.00000	19503E-13	0.00000	.90118E-13	0.00000
78735E-13	0.00000	.11474E-11	0.00000	.21885E-01	0.00000	.34474£+00	0.00000	.66824E-13	0.00000	39964E-13	0.0000
•85691E-13	0.00000	.11847E-11	0.00000	218850-01	0.00000	34474E+00	0.00000	.71964E-13	0.00000	40988E-14	0*00000
.38332E-13	å*00900	964538-12	0.00000	20542E+00	0.00000	672598-01	0.00000	44504L-13	0.00000	?6387E-13	_0:0000 <u>5</u> _
1881aE-1j	U.00000	942326-12	0.00000	.20542E+00	0.00000	.67259E-01	0.00000	7704dE-13	0.00000	33121E-13_	<u> </u>
64522E-13	0.00000	•39249£-12	0.00000	.97480E-01	0.00000	97480E-01	0.00000	13435E-13	0.00000	106234_13_	0.0000
-506298-13	0.00000	386966-12	0.00000	97480E-01	00'000.0						
-29910E-14	0.00000	.30272E-12,	0.00000	97480L-01	0.00000						
108d4E-13	0.000,00	38651E-12	0:00000	97480E-01	, 0 • 000 0 0	.97480E-01	0.00000	62331E-14		.19747E-13	0.00000
76588E-14	0.00000	10562E-11	0.00000	.20542E+00	<b>⊺ა</b> ∙00∪00	~.67259E-01	0.00000	.23513E-14	0.0000	[31173 <u>E</u> =13]	0.00000
38120E-14	0.00000	- <u>.</u> 10673E- <u>!</u> 1_	0.00000	20542E+00	. 0.coooo	6/259E-01	ŏ•oòoóō	73090E-14	. 0.00000		0.00000
19065E-13	0.00000	[ .13360E-11]	0.00000	21885E-01	0.00000	•34474E+00	0.0000	.16610E-13	0.00000	.45052E-13	0.00000
-10377E-13	0,00000	.130168-11	0.00000	218858-01	0.00000	34474£+00	0.00000	•13429E-13	0.00000	.23979E-14	_0•00000
•13751E-13	0.00000	103344-11	9.09000	19150E+00	0.00000	11318£+00	0.00000	.39917E-13	0.00000	.22d17t-13	0.09000
15667E-13	0.00000	168998-11	0.00000	-19150E+00	0.00000	.113186+00	0.00000	.34241E-13	0.00000	76d61E-13	0.00000
19155E-14	0.90000	.407726-12	0.00000	.10676E+00	0.00000	93938&-01	0.00000	22316E-LJ	0.00000	42d77t-13	0.00000
39777E-14	_0.00000	-44457L-12	₫•ºº0₫0₫	10676E+00	0.00000	.939368-01	0.00000	17621E-13	0.00000	29199E-14	0.00000

_		NATURAL	FREQUER	CY= .1774d2E	· 04						
TX REAL	XT Daki	TY REAL	TY IMAU	T.Z Real	TZ IMAG	RX , KEAL	KA IHAG	REAL	NY IHAG	RZ REAL	RZ [HAG ]
11361E#15	0.00000	.97120L-01	0.00000	.35034E-12	0.00000					11_133613	
14696E-13	J.00000°	.97720r-01	0.00000	33634E-12	0.00000	23400E-12`.	0.00000		0.00000_	.23435E-13	_0 * 99 dó 0
- 74320F-15	0.00000	25583£+00	0.00000	51410E-12	0.00000	.54268E-12	0.00000	48110E-14	0.00000	.37176E-13	ขึ•่ดอดักดี _
1646LE-13	0.00000	25583L+00	0.00000	.49434E-12	0.00000	64467E-12	0.00000	59188E-14	0.00000	[79344E-13]	. 0 • 00 0 0 û
75713E-14	0.00000	.31623E+00	0.00000	33466E-12	0.00000	11768E-11	_0.00000	57276E-13_	0.00000	13799E-13	ด์•อิดภักิกั
77253E-13	0.00000	.31623E+00	0.00000	.34521E-12	0.00000	.10427E-11	0.00000	45677E-13_	ō 0000a	2322dt-13	0.00000
87278E-13	0.00000	25583E+00	0.00000	84783E-12	0.00000	14533E-14	0.00000	25266E-13_	0.00000	87978E-15_	_0.000000
.11632E-13	0.00000	-125583E+00	0.00000	d3673E-12	ó.00000	41269E-14.	0.00000	.10390E-13	0.00000	14694E-13	
-92663E-14	0.00000	.97720E-01	0.00000	35100E-12	0.00000	.52653E-12	0.00000	47603E-14	_o•ooooo	.657 <u>27E-14</u>	0.00000
-29957E-14	0.00000	.97720E-0I	0.00000	.33875E-12	0.00000						
250940-13	0.00000	.9/7206-01	0.00000	.71015£-12	0.00000						
.10186E-13	0.00000	.97720E-01	0.00000	F. /1404E-12	0.00000	52596E-12	0.00000	63652E-14	0,00000	11412E-13	.σ_σφοσσ. .σ.σφοσσ.
43543E-13	0.00000	255832+00	0.00000	12677E-i1	_0.00000	91010E-12_	0.00000	10723E13_		.22769E-13	0.00000
239028-13	0.000000	25583E+00	0.0000	.12704E-11	0.00000	9 JO17E-12	0.00000	16112E-13	0.00000	26459E-13	0.00003
18730E-13	3.00000	.31623E+00	0.00000	35036E-12	_0.00000	26024E-11		99263L-14	000000	54375E-13	_ 0*00000
406608-13	0.00000		0.00009	.358978-12	0.0000				0.00000	.69668E-13	
25461E-13	J.00000	25583£+00	0.00000	.162826-11	0.00000	.34440E-12				- <u>82193</u> 5-1 <u>4</u>	
87574E-14	0.00000	25583£+00	0.00000	16123E-11	0.00000	350468-12	0.0000	.14295E-13	0.00000	79196E-14	0.00000
+22606E-13	0.00000	.977201-01	0.00000	72953E+12	0.00000	.74872L-12	0.00000	43087E-13	0.00000	315746-15	_ 0.000000 _ 0.00000
_37076E-1J	0.00000	.97720L-ul	0.00000	.12987E-12	0.00000	74194E-1Z	0.00000	342756-13	<b>0.0</b> 0000	183326-13	ก*ากกัดกั

```
Maked becomes, so was no st
```

<b></b>		SI THE		CV 131 L	P . 4. 4						
			L FRLCULN								
TX REAL	THÁG THÁG	- TY - KEAL	TY [HAG	TZ REAL	TZ Imag	RX KEAL	RX 1mag	RY REAL	THAG :	REAL	THAS
163278-13	0.00000	.61643E-12	0.00000	•42023E-01	0.00000	21887E-01	0.00000	•21167E-13	0.00000	66223t-14	0.00000
-116868E-13	0.00000	•52476C-12	.0.0000	[42023E-01]	`p.00000	.21887L-01	0.00000	.298368-13	0.00000	31667 <u>E</u> -13	_ 0.00000
-44513E-13	0.00000	149936-11	0.00000	-10789E+00	0.00000	.28400£+00°	0.00000	19364E-13	0.00000	~ .52489E-14	o`ooooo
27459E-13	0.00000	138128-11	0.00000	107d9E+00	0.00000	28400E+00	0.00000	15561E-13	_ 0.00000	-12403E-13	o'• oo'doō <u>_</u>
-+26446E-I3	0.00000	.15465£-11	0.00000	27426E+00	0.00000	.33926E-01	0.00000	87627E-14	0.00000	~86138E-13	0_0_0000
_+62073E-14	0.00000	.17649E-11	0.00000	.27426E+00	0.00000	3J926E-01	0.00000	24680E-14	0.00000	12957c-12	0.00000
T-16524E-14	0.00000	121106-11	0.00000	•69997€-01	.0.00000	27041E+00	0.00000	.94120E-14	0.00000	645776-13	_ 0 • 0 0 0 0 0 <u>.</u> .
-60665E-13	0.00000	101370-11	0.00000	699976-01	0.00000	.27041£+00	0.00000	•11530E-13	0.00000	.28337E-13	เ _ 0ั∙าดอดดี `
17931E-13	0.00000	.656198-13	0.00000	. 26724E-01	0.00000_	26724E-01	0.00000	10421E-13	0.00000	90932E-14	0.00000
20687E-14	0.00000	•92241E-14	0.60000	26724E-01	0.00000						
42529E-14	0.00000	. •525786-13	0.00000	26724E-01	0.00000	•					
31874E-13	0.00000	•12704E-13	0.00000	.267248-01	0.00000	.26724E-01	0.00000	.78484E-14	0.00000	11442E-13	0.00000
-138B3E-13	0.00000.	_10216b-11_	0.00000	699976-01	0.00000	270416+00	0.00000	149856-13	0.00000	.38805 <u>c</u> -13	0.00000
-,58711E-14	0.00000	. 89924E-12.	0.00000		0.00000	.2/041E+00	0.00000	,15968£-13	0.00000	56560E-13	0.000000
.719828-14	0.00000	7.147016-11	0.00000	. 27426E+00	0.00000	.33926E-01	_0.00000	,24005E-13	0.00000	- <u>.</u> 63486E-13	0,00000
					•	33926E_01					
21233E-13	0.00000	.132146-11	0.00000	107896+00	0.00000	.28400E+00	0.00000	61850E-14	0.00000	50866 <u>E</u> _13	_ 0.00000
-58050E-13	000000		ັຍ.0000ປຸ	10789E+00	_ 0.00000	20400E+90	0.00000	.64970E-14	0.00000	96d5 jè-1:	
179526-13	0,00000	51340E-12	0.50000	420238-01	0.00000	21887E-01	0.00000	.15331E-13	0.00000	.79219 <u>5</u> -14	. 0.00000
_+15053E-13	0.0000.	51872E-12_	_0.00000	-42023E-01	Ö.00000	•21887E-01	`0.00000	20663E-13	_ `0.00000]	-22104E-1	0.00000

NATURAL FREQUENCY= -175288E+U4

										-	
TX Real	XT Imag	ĨΥ ×ΕΑL	TY Imag	TZ REAL	TZ [HAG	KX KEAL	RX Imag	RY Real	RY Imag	KZ " KEAL	RZ IHAG
.81494E-13	0.00000	.26529E-11	0.00000	13115E+00	0.00000	11043E+00	0.00000	437176-15	0.00000	.69929E-13	0.00000
-33647E−13	0.00000	.26170E-11	0.00000	.13115E+00	0.00000	.11043E+00	0.00000	96037E-14	0.00000	50801Ë-13	o•090jo2
55177E-13	0.00000	602600-11	0.00000	.21182E+00	0.00000	153456+00	0.00000	535116-14	0.00000_	.11835E-13	ō•0000ō
14982E-13	0.00000	658170-11	0.00000	211826+00	0.00000	.153458+00	0.00000	.346966-13	0.00000	45347E-13	0.00000
55682E-13	0.00000	.74064E-11	0.0000	.33248E-01	0.00000	.34817E+00	0.00000	95754E-13	0.00100	99171E-13	
14305E-13	0.00000	.75123E-11	0.00000	33248E-01	0.00000	34817£+00	0.00000	88480E-13	0.00000	.55774E-13	0.00000
-,47152E-13	0.00000	464025-11	0.00000		0.00000	186618-01	0.00000	.37147E-13,	. 0.000'00		<u></u>
-11217E-12	0.00000	47918E-11	0.00000	.16437E+00	0.00000	.18661E-01	0.00000	•56153E-13	0.00000	37714E-13	ò•ooōo <u>ō</u>
".17398E-13	0.00000	11127E-12	0.00000		0.00000	.60716E-12	0.00000	18750E-13	_0.00000	. 22449 <u>6</u> —13	0.00000
.75111E-14	0.00000	135148-12	0.00000		0.00000						
-174833E-14	0.00000	11627E-12	0.0000	.504646-01	0.00000						
						60001E-12	0.0000	.23678E-13	. 0 . 000 00	.34924E-14	0.00000
				16439E±00_							
				.16439E.00							
				.33248E-01							
•				33248E-01				•13201E-1 <u>3</u>			
=				21182E+00			0.00000		0_000000	-16567E-12	0.00002_
.271176-13					0.00006	15345t+00	0.00000	.24458t-13	0.00000	14763E-12	0.00000
.95821E-13	0.00000		0.00000		0.00000	-11043E+00	0.00000	152028-13	0.00000	.3731d <u>u</u> —13	0.00000
904678-13	0.00.00	207408-11	0.00000	•13115E+00	0.00000	11043E+00	0.00000	206336-13	0.00000	14363¢-13	. 0.000000
				*							

MATURAL PREQUENCY = 182921E+04

TX TX TX	TY TY	TZ REAL	TŽ IHAG	R.K KEAL	KX I HAG	RY REAL	RY RZ RZ IMAG REAL IMAG
36719F=13 U.00000	.103171+00 0.00000	175935-01	0.00000	.55701E-01			0.00000 .2436dE-13 0.00000
119294F-11 0.00000	103176+00 0.00000	17593E-01	0.00006	55701E-01	0.00000	556698-14_	0.0000021194E-13 0.00000
.1644!E=13 0.00000	186338+00 0.00000	175566-01	0.00000	26026E+00	0.00000	34911E-13	0.00000 .3555AF-Ĭ3 0.00000 -
.3530}E-13 0.00000	~16833E+00 0.00000	17550E-01	0.00000	200266+00	0.00000	45818E-13	0.0000013905E-T3 0.00309
-11147F-14 U-00000	52531t +01 0.00000	.57659E-01	0.00000	73297E-01	0.00000	.59598E-14	0.00000 -19389F-73 0.00000
.55709E-14 0.00000		57659E-01	0.00000	73297E-01	0.00000	49590E-14	0.00000 19740E-13 0.00000
.529476-13 0.00900	.20139E+00 0.6000J	.442056-02		.2d1o4L+00	0.0000	95729E-15	0.00000 .79839==13 0.00000
.232256-13 0.00000	20147E+00 0.00000	.4420>E-02		.261842+00			0.0000081227E-14 0.00000
-13457E-L3 0.00000	].179456-12 [0.00000]	269308-01	0.00000	11403E-12	_0.00000	17946E-13	0.00000106d5E-13 0.00000
•	20465L-12 0.00000				,		•
.34983E-13 0.07000	.17954E-12 0.000G0	269305-01	0.00000				-
.98991E-14 0.00000	204651-12 _0.00000	26 <u>93</u> 0E-01	_0.00000	95334E-13_	0.00000	20051E-13	0.0000011016£-13 0.00000
.27512E-13 0.00000	20199E+00 0.00000						0.0000056601E-13 0.00000
.31941E-13 0.00000	.201996+00 0.00000	.442051-02	0.00000	28184E+00	0.00000		0.0000057290E-13 0.0000
+19905E-13 0.00900	.525316-01 _0.00000	5765 ) = -01	0.00000				0.00000 11149LL-12 0.00000
.16463E-13 0.00000	52531E-01 0.00000	57659E-01_	0.00000			13795E-14	0.0000062168E-13 0.00000
18246E-T3 0.00000	.1d333E+00 ,0.00000	175561-01	0.00000			_	0.00000 .13636E-11 0.00000
.152478-13 0.00000	108331+00, 0.00000	-,1755oE-01	_0.00000				0.0000037266t-13 0.00000
-26209E-13 0.00000	1031/6+00 0.00000	17593E-01	0.00000				0.00000 .33447E-13 0.00000
732931-13 0.00000	.163172+00 0.00000	175936-01	0.00000	55701E-01	0.00000	3531E-13	0.0000022963E-13 0.00000

## MATURAL FREGUENCY= .175361E+04

. TX REAL	TX IMAG ,	TY REAL	YY JAH1	TZ Real	TZ IHAG	RX KEAL	XX 1HAG	RY Real	KY .	REAL	
.14586E-13	0.00000	11401E+00	0.00000	297346-11	0.00000	26070E-11	0.00000	.328588-13	0.00000	24184E-14	
20325E-13	0.00000	11401L+00	0.00000	.2942JE-11	0.00000	.26583E-11	0.00000	.11557E~13	0.00000	.177275-13	
21844[-13	0.00000	.288680+00	0.00003	.515136-11	0.00000	290846-11	0.00000	.83654E-14	0.00000	23860c-13	
420191-14	0.00000	.28868F+00	0.00000	52362E-11	0.00000	.20425L-11	0.00000	.21873E-13	0.00000	2207st-14	
18394E-13	0.00000	32827£+00	0.00000	320736-13	0.00000	.75447E-11	0.00000			52263±-13	
160021-13	J-00000	328276+00	0.00000	.36890£-13	0.00000	81515E-11	0.00000			24131E-13	
-40531E-14	0.00000	.214268+00	0.00000	32675E-11	0.00000	115872-11	0.00000			.37373E-15	
-32221E-13	0.00000	.21426E+00	0.00000	.33406E-11	0.00000	.74230t-12	0.00000			10191E-13	
-30625E-13	0.00000	.312526-12	0.00000	.10283E-11	0.00000	30578E-13	0.00000	16350E-13	0.00000	36468E-14	0.00590
.19852E-13		.221966-12	0.00000	10179E-11	0.00000						
14771E-13	0.00000	29171E-12	0.00000	.47313E-12	0.00000		•	_			~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
21332E-14	0.00000	.21/44E-12	0.00000	96479E-12	0.00000	·13424E-13	0.00000	.25878E-13	0.00000	17154E-14	
=	0.000.00	21426E+00	0.0000	39608E-11	. 6*00009	10413E-11	0.00000	21382E-13	0.00000		0,00002_
- <del>-</del>		31/3/5+00	0.0000	38611E-11	0.00000	.70951E-12	`_0•0 <u>00</u> 00	1504¢E-1.₫	0•00000		
623058-13	0.00000	21426E+00	0.00000	-2,1084E-11	0.00000	755395-11	O.UOOOO	452516-43	0.00000	7.017754 45	
74713E-13	ŭ.00000	- 32827E+00	ó.0000ũ	21216E-11		.68719E-I1	. 0.00000	427616-13	0.00000	,	·
			0.0000	.39725E-11	0.00000	.40272t-11	0.00000	_ 78541E-13	. 0.00000	10043E-12	
739285-13	0.00000	23568E+00	0.00000	38727E-11	0.00000	441445-11	0.00000	.66498E-1.	0.00000	,	3 0-00000
			0.00000	30001E-11	0.00000	.22846£-11	0.0000	11032E-1.	3 0.0000	, ,,,,,,	
	J.00000	.11401E+00	0.0000	,302148-11	. 0.00000	21795E-11	0.00000	22661E-1.	າັ ດ•ດດລິດ <u>ໂ</u>	) - 4554 <u>je-1</u>	

•• ·		1490144	L FKŁGUIN	LY= .185000E	+04						
TX REAL	TX 1 mag	TY NEAL	TY 1 mag	T/ Rial	TZ Imag	KE AL KX	RX I MAG	RY Real	KY IMAG .	KAL	K&
~.13515E-		100921+00	0.03000	.177386-01	0.00000	543142-01	0.00000	.383918-14		37263E-14	
•32430E-	13 0.00300	.108922+00	0.00000	.17738E-01	0.00000	54314E-01	0.00000	155678-13		14736L-13	
.17871E-	13 0.00000	.21136L+00	0.00000	.106678-01	0.00000	.25825E+00	0.00000	19292E-13	•	247176-13	
326d5E-	14 0.00000	21136c+00	0.00000	.106678-01	0.00000	.25825E+00	0.00000	.141078-13		14104e-14	
	13 0.00090		0.00000	53255L-01	0.00000	.15730E-01	0.00000	24087E-13		34652E-13	
'	-13 0.00000			53255E-01	0.00000	.15730L-01	0.00000	130936-13		.15832t-13	
.662348		215126+00	0.00000	.28367E-02	0.00000	255256+00	0.00000	.346488-13		33720E-13	
36195E-				.28367E-02	0.00000	25525E+00	0.00000	.37385E-13	0.0000	11689E-13	0.00000
-18855E		.93383E-01		.47271E-02	0.00000	47271E-02	0.00000	.81766E-14	_0.0000	.14894c-13	0.00000
.22219E		933331-01		.472716-02	0.00060						
"14622E·	-13 0.00000	. *433836-01	0.00000	472716-02	0.00000						
-281168-	-13 0.00000	933835-01	0.00000	47271E-02	0,00000	47271L-02	0.00000	.42258E-14	0.00000	1 10635t-14	0.0000
		21512c+00	0.00000	28367E-02	0.00000	25525:+00	0.00000	94637Ē-14	0•00000	10487E-13	0.00000
	-13 0.00000	.21512L+00	0.00000	28307E-02	0.00000	25525£+00	0.00000	941748-14	u.0000	, •15@eof-13	0.000 <u>000</u>
		_			0.00000	.15730E-01	0.00000	26181E-14	0.0000	32907£-13	0.00000
,	-13 0.00000				0.00060	.15730E-01	0.00000	650098-14	0.0000	o ~ .34471E-13	. o.gooog
	-14 0.00300	211365+00	0.00000	10667E-01	0.0000	.25825£+00					3 `0 • 0 n 0 <u>0 0 </u>
		21136E+00		10667E-01	0.00000	.25825E+00	_ 6.00000	.74386E-14	_ 0.0000	0 <u> </u>	0.00000
21967£						54314E-01			0.0000	017486E-1	3 0.00000
-	-13 0.00000								0.0000	0 .354546-15	5 0.0000)

1854.39	
3	
ž Ž	
₹	
~	

NATURAL FREQUE					
TX TX TY TY TY THAG	TZ TZ KEAL IMAG	XX KEAL	RK IMAG	RY	RY RZ RZ
-10789E-13 0.00000 .88884L-01 0.00000	105836-01 0.00000	<b>44</b>			0.00000131364-13 0.00000
12058E-13 0.0000088984E-01 0.00000	105#30±0.00000				0.00000 .23d05E-13 0.00000
16753E-13 0.0000G24219E+00 0.00000					0.00000 65441E-14 0.00000
.323778-13 3.00000 242196+00 0.00000	<b>'</b>	152936+00	~o.000oo		0.00000 241686-15 0.00000
-21043E-13 0.00000 .28072E+00 0.00000			0.00000		0.00000140856-13 0.0000
77444E-14 0.0000028072E+00 0.00000		*1d141E+00			0.00000643675-12 0.0000
18314E-13 0.0000018345E+00 0.00000	16341E-01 0.00000	114688+00	0.00000	11580E-13	0.0000015495E-13 _0.00000
4241bE-1> 0.00000 -10345E+00 0.00000	16341E-01 0.00000	11468E+00	0.00000	77027E-14	0.00000725036-14 0.00000
22593C-13 0.0000031265L-12 0.00000		.294808-14	0.00000	.13489E-13	0.0000022995E-13 0.00000
57781E-1+ 0.00000 .31398E-12 0.00000	.10131E-01 0.00000				<del>_</del>
-22563E-13 0.0000031265L-12 0.00000	.101316-01 0.00000				
15608E-13 0.00000 .31398E-12 0.00000			_0.00000	<u>.1</u> 3972 <u>E</u> -13	0.00000 .85882e-14 0.00000
27858E-14 0.00000 .18345L+00 0.00000	16341E-01 0.000GC	11468£+00	0.00000	.55116E-14	0.0000062483E-13 0.00000
25481E-13 0.00000 -18345E+00 0.0000			0.00000		0.00000 .59446E-13 0.00000
-36749E-13 U.003U026972E+00 0.00000					0.00000 7.413916-13 0.00000
_40213E-13 U.00U0 .28072E+00 0.0000	3456/E-02 0.0000			3115dE,-13	<u> 0.00000270112-13 0.00000</u>
.40213E-13 u.00000 .28072E±00 0.0000	5 - 13337E-01 0.0000	152936+00	0.00000	32943E-13	0.00000 .46375E-13 0.00000
•				337266-13	
				177468-15	
	0 102838-01 0.0030				<u>-</u>
.30697E-14 0.00000 .80564E-01 0.0000	ŭ' -•*0>02¢-01 'Aidaa.		-	-	-

* NATURAL FREQUENCY= -201454E+04

TX Real	TX 1mag	TY KEAL	TY IHAG	T.Z REAL	TZ I MAG	KEAL KX	RX IMAG	RY Real	KY IHAG	RZ Real	RZ IMAG
20255E-13	0.00000	.79916E-01	0.00000	93145E-02	0.00000	.257458-01	0.00000	.16675E-13	U. 00000	76377E-14	0.00000
58994E-14	0.00000	79916:-01	0:00000	931456-02	0.00000	.2>745E-01	0.00000	-19045E-13	0.00000	73611E-14	0.00000
1893dE-13	0.00000	2/2774+00	0.00000	.12794E-01	0.00000	13502L+00	0.00000	577888-14	0.00000	.146895-13	0.00000
233248-13	0.00000	.22277L+00	0.00000	.12794E-01	0.00000	13502E+00	0.00000	172176-13	0.00000	15244E-13	0.00000
515975-15	0.00000	.276496+00	0.00000	.67816E-03	0.00000	.171996+00	0.00000	25981E-13	0.00000	30254E-13	0.00000
50050E-14	0.00000	2764JL+00	0.00000	.678165-03	0.00000	•17149L+00	0.00000	174878-13	0.00000	.233d3c-13	. <b>ว•ก</b> อบอง์
151708-13	0.00000	21065(+00	0.00000	143838-01	0.00000	128401+00	0.00000	23240114	0.00000	.28537 <u>e</u> -13	0.00000
-372645-13	J.00000	.216651+00	<b>0.</b> 00000	-1143838-01	0.00060	12840L+00	0.00000	·18225E-14	0.00000	600276-13	0.00000
.10441E-13	0.00000	-720451-01	0.00000	.725045-03	0.00000	725046-03	0.00000	.73977E-14	0.00000	.72d67E-14.	0.00000
•39336L-14	0.0000	720451-01	0.00000	./25042-03	0.00000						
19272E-14	0.00000	.72045E-01	0.00000	-1.125041-03	0.00000						
.60275E-14	0.00000	720456-01	0.00000	/2504E-03	0.00000	725041-03	0.00000	-81239E-14	0.00000	703636-15	.0.00001
320516-14	0.00000	216652+00	0.00000	.14363L-01	0.00000	128408+00	0.0000	21362E-13	0.00000	153936-13	, jō•goo <u>g</u> o, T
34924L-13	0.00000	.21605£+00	0.00000	.14363E-01	_0.00000	12840=+00	0.00000	209908-13	0.00000	219926-13	7.00000
107275-13	0.00000	.275432+00	0.00000	07810E-0J	0.00000	.17199±+00	0.00000	.372078-13	6.00000	150436-13	_0.00001
•13773E-13	0.00000	27648E+00	0.00000	678166-03	0.00000	.171991+00	0.00000	"".37271E-13	0.00000	.23861E-14	0.00030
.84652E-15	0.00000	222/76+00	0.53000	127948-01	0.00000	13502=+00	0.00000	133304-13	0.00.00	-27295e-13	0.00000
•10625E-13	0.00000	.222776+00	0.00000	12774E-01	0.00000	13502t+00	0.00000	12800E-13	0.00000	20d00ë-13	C00000.
,10748L-13	0.00000	.799166-01	0.00000	.931455-02	0.00000	.257452-01	0.00000	.15385E-14	0.00000	.544576-14	0.00000
1160/E-13	0.00030	799164-01	0.00000	.931452-02	0.00060	.25745L-01	6.00000	.21479E-14	0.00000	.134388-13	0.00000